



UNIVERSITI PUTRA MALAYSIA

***NUMERICAL ANALYSIS OF FREQUENCY AND ELECTRICAL
RESPONSE IN PIEZOELECTRIC-COVERED COMPONENTS FOR
ENERGY HARVESTING***

ERFAN SHAMSADDINI LORI

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By

ERFAN SHAMSADDINI LORI

**Thesis Submitted to the School of Graduate Studies, Universiti Putra Malaysia,
in Fulfilment of the Requirements for the Degree of Doctor of Philosophy**

September 2020

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Abstract of thesis presented to the Senate of Universiti Putra Malaysia in fulfilment of the requirement for the degree of Doctor of Philosophy

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September 2020

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In recent years there has been an increased interest in scavenging energy using alternative sources. One of these sources is vibration which can be harvested and converted to electrical energy. Piezoelectric materials can be used to capture vibration, motion or acoustic noise, to be converted into electrical output. Due to the never-ending human attitude towards technology for improving the mechanical properties and operation of the structures, GPL reinforcements gain the attention of scientists for providing an enthusiastic enhancement in the design of the existing composite structures. This study presents the electrical response of piezoelectric for two different components (microdisk and cantilever beam). In the first part of this research, the frequency analysis of a Graphene Nanoplatelets Reinforced Composite (GPLRC) microdisk is investigated for three different boundary conditions (simply-simply, simply-clamped and clamped-clamped). The issue rises since at nanoscale no experimental work has been done before. To overcome this problem, nonlocal strain gradient theory (NSGT) is employed which introduces two size-dependent length scale (l) and nonlocal (μ). The present study is done in the framework of numerical based generalized differential quadrature method (GDQM). The stresses and strains are obtained using the higher-order shear deformable theory (HOSDT). The rule of the mixture is employed to obtain varying mass density and Poisson's ratio, while the module of elasticity is computed by a modified Halpin-Tsai model. Governing equations and boundary conditions of the GPLRC microdisk covered with the piezoelectric layer are obtained by implementing Hamilton's principle. Regarding perfect bonding between the piezoelectric layer and core, the compatibility conditions are derived. Also, due to the existence of the piezoelectric layer, Maxwell's equation is derived. MATLAB software is used and results show that the ratio of the outer to the inner radius (R_o/R_i), ratios of length scale and nonlocal to thickness (l/h and μ/h), the ratio of piezoelectric to core thickness (h_p/h), applied voltage, and GPL weight fraction (g_{GPL}) have a significant influence

on the frequency characteristics of the GPLRC micro-disk. Another important consequence is that as well as the nonlinear indirect effects of applied voltage on the natural frequency of the GPLRC micro-disk covered with piezoelectric for each specific value of R_o/R_i , the impact of the R_o/R_i on the natural frequency is indirect. In addition, four different patterns of GPL distribution in the microdisk are investigated. For all patterns, the relation between g_{GPL} parameter and critical voltage is linear. It was also found that when the boundary conditions of S–S is considered, patterns 4 and 1 have not shown any significant effect on the critical voltage of the structure. A useful suggestion of this research is that, for designing the GPLRC circular microplate at the low value of the R_o/R_i , more attention should be given to the g_{GPL} and R_o/R_i , simultaneously.

For the second component, a cantilever beam with one fixed end which is covered with a piezoelectric layer is studied under two different vibrational sources. The effect of thickness ratio of the piezoelectric layer, different geometric shapes (trapezoidal, rectangular and triangular) of the beam and a tip mass on output voltage in both sources of vibration is carried using COMSOL Multiphysics. For the case of vibration under body load, a swept sine excitation source of 200 mV which creates a harmonic body load is investigated. The simulation is carried on in a frequency range of 0-800 Hz. The highest voltage output has been achieved by the triangular shape (14.4 V) of the beam and the lowest value belongs to the trapezium (3.3 V). For the effect of the thickness ratio of the piezoelectric layer to the base (R_p/R_b), the best result is achieved when the piezoelectric layer and the base layer have the same thickness. The simulation is continued with the second source of vibration which is coming from rain droplets and acts as a point load on the surface of the beam. Different rain droplets with various range of radius size, speed and impact force are used in the study. Besides, three different impact point along the beam was selected and the findings reveal that the closer the impact point to the free end of the beam the higher the output voltage generated. The highest voltage output occurs for the triangular beam where the droplet has a diameter of 5 mm and a terminal velocity of 9 m/s. It was found that by changing the shape of the beam from rectangular to triangular the voltage output had been more than doubled (increased from 5.7 V to 14.4 V). Attaching a tip mass on the cantilever beam results in decreasing the voltage output but it increases the duration of oscillation. In conclusion, the piezoelectric specimen which is cut into a triangular shape results in a significant increase in the output voltage compared to other geometrical shapes upon the impact of rain droplets. However, to utilize this more effectively in real applications there must be arrays of these specimens to cover a larger surface area; therefore, resulting in great power.

Abstrak tesis yang dikemukakan kepada Senat Universiti Putra Malaysia sebagai memenuhi keperluan untuk ijazah Doktor Falsafah

**ANALISIS BERANGKA FREKUENSI DAN TINDAKBALAS ELEKTRIK
DALAM KOMPONEN BERLAPIS PIEZOELEKTRIK UNTUK PENUAIAN
TENAGA**

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Dalam tahun-tahun kebelakangan ini, ada peningkatan minat untuk mengumpul tenaga menggunakan sumber alternatif. Salah satu sumbernya ialah getaran yang dapat diambil dan ditukarkan menjadi tenaga elektrik. Bahan piezoelektrik dapat digunakan untuk menangkap getaran, gerakan atau suara akustik, untuk diubah menjadi output elektrik oleh kerana sikap mausia terhadap teknologi yang tidak pernah putus-putus untuk meningkatkan sifat mekanik dan operasi struktur. Pengukuhan GPL mendapat perhatian para saintis kerana memberikan peningkatan yang memberasangkan dalam reka bentuk struktur komposit yang sedia ada. Kajian ini menunjukkan tindak balas elektrik piezoelektrik untuk dua komponen yang berbeza (cakera mikro dan rasuk kantilever). Pada bahagian pertama penyelidikan ini, analisis frekuensi mikrodisk Graphene Nanoplatelets Reinforced Composite (GPLRC) disiasat untuk tiga keadaan sempadan yang berbeza (sederhana-sederhana, hanya diapit dan diapit-diapit). Masalahnya adalah, kerana ini dilakukan pada skala nano belum ada kerja eksperimen yang dilakukan sebelumnya. Untuk mengatasi masalah ini, teori kecerunan regangan nonlokal (NSGT) digunakan yang memperkenalkan dua skala panjang bergantung pada ukuran (l) dan nonlokal (μ). Kajian ini dilakukan dalam rangka kaedah kuadratur pembezaan generalisasi berdasarkan berangka (GDQM). Tekanan dan ketegangan diperoleh menggunakan teori ubah bentuk ricih tertib tinggi (HOSDT). Peraturan campuran digunakan untuk memperoleh kepadatan jisim dan nisbah Poisson yang berbeza-beza, sedangkan modul keanjalan dihitung dengan model Halpin-Tsai yang diubahsuai. Persamaan dan keadaan sempadan mikrodisk GPLRC yang ditutup dengan lapisan piezoelektrik diperoleh dengan menerapkan prinsip Hamilton. Mengenai ikatan sempurna antara lapisan dan teras piezoelektrik, syarat keserasian diperoleh. Juga, kerana wujudnya lapisan piezoelektrik, persamaan Maxwell diturunkan. Perisian MATLAB digunakan dan hasilnya menunjukkan bahawa nisbah jejari luaran ke dalam (R_o/R_i), nisbah skala panjang dan ketebalan tidak lokal ke (l/h and μ/h) nisbah ketebalan

piezoelektrik ke teras (h_p/h), voltan gunaan, dan pecahan berat GPL (g_{GPL}) mempunyai pengaruh yang signifikan terhadap ciri frekuensi cakera mikro GPLRC. Satu akibat penting lain adalah bahawa selain kesan tidak langsung voltan gunaan pada frekuensi semula jadi cakera mikro GPLRC yang ditutup dengan piezoelektrik untuk setiap nilai tertentu R_o/R_i , kesan R_o/R_i pada frekuensi semula jadi tidak langsung. Sebagai tambahan, empat corak taburan GPL yang berbeza dalam cakera mikro disiasat. Untuk semua corak, hubungan antara parameter g_{GPL} dan voltan kritikal adalah linear. Ia juga didapati bahawa apabila keadaan batas S-S dipertimbangkan, corak 4 dan 1 tidak menunjukkan kesan yang signifikan terhadap voltan kritikal struktur. Cadangan berguna dari penyelidikan ini adalah bahawa, untuk merancang plat mikro pekeliling GPLRC pada nilai rendah R_o/R_i , perhatian lebih harus diberikan kepada g_{GPL} dan R_o/R_i , secara serentak.

Untuk komponen kedua, rasuk kantilever dengan satu hujung tetap yang ditutup dengan lapisan piezoelektrik dikaji di bawah dua sumber getaran yang berbeza. Kesan nisbah ketebalan lapisan piezoelektrik, bentuk geometri yang berbeza (trapezoid, segi empat tepat dan segitiga) rasuk dan jisim hujung pada voltan keluaran di kedua-dua sumber getaran dibawa menggunakan COMSOL Multiphysics. Untuk kes getaran di bawah beban badan, sumber pengujian sinus menyapu 200 mV yang membuat beban badan harmonik disiasat. Simulasi dijalankan dalam julat frekuensi 0-800 Hz. Output voltan tertinggi telah dicapai dengan bentuk segitiga (14.4 V) rasuk dan nilai terendah tergolong dalam trapezium (3.3 V). Untuk kesan nisbah ketebalan lapisan piezoelektrik ke dasar (R_p/R_b), hasil terbaik dicapai apabila lapisan piezoelektrik dan lapisan dasar mempunyai ketebalan yang sama. Simulasi diteruskan dengan sumber getaran kedua yang berasal dari titisan hujan dan bertindak sebagai muatan titik pada permukaan rasuk. Titisan hujan yang berbeza dengan pelbagai ukuran, kelajuan dan kekuatan hentaman digunakan dalam kajian ini. Di samping itu, tiga titik hentaman yang berbeza di sepanjang rasuk dipilih dan penemuan menunjukkan bahawa, semakin dekat titik hentaman ke hujung rasuk bebas, semakin tinggi voltan keluaran yang dihasilkan. Output voltan tertinggi berlaku untuk rasuk segitiga di mana titisan mempunyai diameter 5 mm dan halaju terminal 9 m/s. Didapati bahawa dengan mengubah bentuk rasuk dari segi empat tepat menjadi segitiga output voltan telah meningkat dua kali ganda (meningkat dari 5.7 V menjadi 14.4 V). Melampirkan jisim hujung pada rasuk kantilever akan menurunkan output voltan tetapi meningkatkan jangka masa ayunan. Kesimpulannya, spesimen piezoelektrik yang dipotong menjadi bentuk segitiga menghasilkan peningkatan voltan keluaran yang ketara dibandingkan dengan bentuk geometri lain pada kesan titisan hujan. Walau bagaimanapun, untuk menggunakan ini dengan lebih berkesan dalam aplikasi sebenar mesti ada susunan spesimen ini untuk menutup luas permukaan yang lebih besar; oleh itu, menghasilkan kuasa yang besar.

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LIST OF SYMBOLS

R_o	Outer radius
R_i	Inner radius
h	Core thickness
h_p	Piezoelectric thickness
l	Length scale
μ	Nonlocal scale
g_{GPL}	GPL weight fraction
V_{GPL}	GPL volume fraction
V_M	Matrix volume fraction
ρ_{GPL}	Mass densities of the GPL
ρ_M	Mass densities of polymer matrix
E_M	Young's modulus of polymer matrix
E_{GPL}	Young's modulus of GPL
L_{GPL}	Average length of GPL
t_{GPL}	Average thickness of GPL
w_{GPL}	Average width of GPL
ρ_c	Mass density of GPL/polymer nanocomposite
ν_c	Poisson's ratio of GPL/polymer nanocomposite
u^c	Displacement in core plate along x
v^c	Displacement in core plate along θ
w^c	Displacement in core plate along z
u^p	Displacement in piezoelectric layer along x
v^p	Displacement in piezoelectric layer along θ
w^p	Displacement in piezoelectric layer along z
Q_{ij}	Elasticity matrix
e_{mij}	Piezoelectric constant
ϵ_{im}	Dielectric constant
D_i	Electric displacement of the piezoelectric
E_m	Electric fields strength of the piezoelectric

E_R	Electric fields strength along R
E_θ	Electric fields strength along θ
E_z	Electric fields strength along z
U^i	Strain energy of the microdisk
T^i	Kinetic energy of the microdisk
W^i	External work on the microdisk
N_i^P	External electric load
t_{ij}	Nonlocal strain gradient stress tensor
ε_{ck}	Strain tensor
C_{ijck}	Elasticity tensor
V	Volt
R	Load resistance
W1	fix end's width of the beam
W2	free end's width of the beam
r	Droplet radius
ρ_w	Density of water
v	Droplet velocity
L	Length of the beam

LIST OF ABBREVIATIONS

2D	Two dimensional
AC	Alternative current
CNT	Carbon nanotube
CWCVD	Cockcroft Walton Cascade Voltage Doubler
DC	Direct current
DQ	Differential quadrature
DWCNT	Double-walled carbon nanotube
EH	Energy harvesting
FG	Functionally graded
FGM	Functionally graded material
FSD	First-order shear deformation
FSDT	First-order shear deformation theory
GDQ	General differential quadrature
GDQM	Generalized differential quadrature method
GNPRC	Graphene nanoplatelet reinforced composite
GPL	Graphene nanoplatelet
GPLRC	Graphene nanoplatelets reinforced composite
HOSDT	Higher order shear deformable theory
KFCVD	Karthus Fisher Cascade Voltage Doubler
MCS	Modified couple stress
MWCNT	Multi-walled carbon nanotube
NSGT	Nonlocal strain gradient theory
PEH	Piezoelectric energy harvesting
PIAC	Piezoelectric actuator
PMN- PT	Lead Magnesium Niobate-Lead Titanate
PVDF	Zinc Oxide and Polyvinylidene Difluoride
PZN- PT	Lead Zinc Niobate-Lead Titanate
PZT	Lead Zirconated Titanate
SWCNT	Single-walled carbon nanotube

CHAPTER 1

INTRODUCTION

1.1 Background

Over the past few years, the demand for renewable energy sources has significantly increased. Renewable energy sources are extensively used due to some of the disadvantages of fossil fuels such as, environmental damage, territorial imbalances and fossil fuel depletion which caused this global shift towards clean energy (Afsharzade et al., 2016; Candela et al., 2007; Di Dio et al., 2007; Shamsadini Lori & Leman, 2016). One of the potential sources of renewable energy that draws the researcher's attention is rain. Rain is a natural phenomenon that exists and occurs in day-to-day life. The potential energy that the raindrops carry out at high altitude is converted to kinetic energy upon impact on any surface which creates vibration. This vibration, even though might be weak but at large volume, can be harvested and can be used efficiently (Vatansever et al., 2011). There are of course some limitations to this idea since this method of harvesting relies strongly on frequency and volume of rainfall. Those regions, which have heavy rainy seasons, are suitable for this method. Malaysia is one of the countries which is located in equatorial and because of that it receives massive rainfall throughout the year (Mohtar et al., 2015). This makes it suitable to apply this technology especially in remote areas where the accessibility to electricity is difficult. It is seen that the demand has increased rapidly in self-powered electronic devices such as wireless sensors, industrial automation, and electronic devices.

Currently, three methods are being used to convert the mechanical energy from vibration into electrical energy namely as electromagnetic induction (Sari et al., 2007), electrostatic induction (Asanuma et al., 2013; Richards et al., 2004) and piezoelectric effect (Jackson et al., 2014; Lanbo et al., 2014). The studies on piezoelectric materials have been most widely investigated since they provide higher density and can be readily integrated into a system (Steven R Anton & Sodano, 2007; Li et al., 2014; S Roundy & Wright, 2004).

Reinforced laminated composites are increasingly used in various applications due to its outstanding features, namely high tensile strength, high modulus, and lightweight (Habibi et al., 2018; Habibi et al., 2016; Habibi, Hashemi et al., 2018). Sun & Zhao (2018) compared the fracture behavior of the functionally graded (FG) cemented carbide reinforced with and without the graphene nanoplatelet (GPL). They claimed that the property of GPLs in the nanocomposites is worked as a stopper for micro cracks. Besides, with the aid of an experimental study, Rafiee et al. (2009) reported that the composite structures which are reinforced with GPL agree with much stronger than the reinforced structures with single-walled carbon nanotube (SWCNT), double-walled carbon nanotube (DWCNT), and multi-walled carbon nanotube (MWCN). In their result presented the effect of different kinds of reinforcement to improving the vibrational behavior of the micro circular shell.

Gholami et al. (2018) focused on the modeling and instability analysis of the FG circular micro-shell based on a more applicable gradient elasticity theory which it can consider the size effect and high order parameters and that was a novelty in this field. They showed that the size effect and radius to thickness parameters could play an important role in the nonlinear instability of the microstructure. Mohammadimehr et al. (2018) presented static and dynamic stability of the circular composite plate which they solved this problem with the aid of first-order shear deformation (FSD) theory and general differential quadrature (GDQ) method.

Therefore, this study was conducted to investigate the frequency characteristics of a graphene nanoplatelet composite (GPLRC) as well as the critical voltage for circular micro-disk. Also, the effect of covering graphene with a layer of piezoelectric and its electrical properties are analyzed. These results are used in a bigger scale for the application of harvesting energy from raindrops. It is shown by simulation that how by varying design configurations an optimum output can be obtained.

1.2 Problem Statements

Due to the never-ending need of technology for improving the mechanical properties (Habibi et al., 2018; Habibi et al., 2016) and operation of the structures (Habibi et al., 2017), GPL reinforcements gain the attention of scientists for providing an enthusiastic enhancement in design of the applicable composite structures (Ebrahimi et al., 2018; Esmailpoor Hajilak et al., 2019a; Habibi et al., 2019b; Pourjabari et al., 2019a).

In the field of the vibrational and buckling characteristics of the piezoelectric circular micro/nanoplate, Wang et al. (2017) focused on the nonlinear dynamic responses of the size-dependent circular plate which is actuated with piezoelectric part and considered a thermal environment. They showed that nonlinear geometric effects on the dynamic responses are more significant. Mahinzare et al. (2019) presented a vibration response of an effected size functionally graded material (FGM) circular plate with the aid of nonlocal strain gradient theory (NSGT), first-order shear deformation theory (FSDT), Hamilton's principle, and the differential quadrature (DQ) method. They considered rotation, thermal, and electro-elastic impact in their mathematical modeling. They found that rotational speed plays an important role in the vibration characteristics of the nanostructure. In another work, Mahinzare et al. (2018) played the attention on the vibrational behaviors of the rotating two-directional FG piezoelectric size-dependent circular plate based on the FSDT, DQM, and Hamilton's principle. They showed that the dynamic behavior of the plate is depended on the externally applied voltage and rotating loads. Shojaeefard et al. (2018) illustrated the natural frequency of a rotating tapered size-dependent circular plate based on the DQM, and Hamilton's principle. They modeled the material of the structure as 2D-FGM. They found out the critical angular velocity for the structure in diffract conditions. To the best of authors' knowledge, frequency analysis of a GPLRC microdisk covered with a piezoelectric layer based on NSGT has not been issued in the published literature. In this study, modified Halpin-Tsai

micromechanics is employed to approximate effective elastic properties. A numerical solution to differential governing equations is presented in the case of various boundary conditions. Special attentions are given to explore the effects of the R_o/R_i , l/h , μ/h , h/h_p , applied voltage and g_{GPL} on the frequency characteristics of a GPLRC micro-disk covered with piezoelectric layer.

In terms of harvesting energy from potential energy possessed in rain droplets, many types of research have been over the past decade. In a study done in Italy made a comparison between the two most commonly used piezoelectric material (PZT and PVDF) with a simple cantilever beam with one fix end. Various droplets have been used and it was concluded that PZT material generates a higher amount of output voltage compared to PVDF (Vatansever et al., 2011). In another research, they (Viola et al., 2014) used a rectangular membrane made of PVDF which was clamped at four edges and a droplet was released on the center. Their findings show that a membrane is not a suitable design for harvesting energy from rain droplets compared to cantilever since the output power was extremely low. Wong et al. (2014) used a cantilever beam with fixing the two ends (cantilever bridge) while using two different materials (PVDF, PZT). Their findings were in parallel with previous literature and proved that PZT provides a higher output. However, a cantilever beam with one fix end gives a more promising result compared to cantilever bridge. An experiment conducted by Wu et al. (2014) tried to achieve the best efficiency by varying the thickness of the cantilever and they have the best thickness for cantilever but not the ratio to the base beam.

Many of these researchers limited their study on mainly three basic designs (cantilever, cantilever bridge, and membrane) for two different widely used piezoelectric material (PVDF, PZT) until recently were new designs are suggested and investigated. An investigation by Viola (2018) on implementing a floating disk was a new approach. Three sets of the experiment (single cantilever, disk supported by two cantilevers, disk supported by four cantilevers) were conducted and the results were compared. It was found that in the case of one single droplet the single cantilever without the disk generates a higher output voltage. In another research, the cantilever has been modified to the spoon shape cantilever (Doria et al., 2019). This design achieved a slightly higher output. They investigated further the effect of wetness on the efficiency of the system and according to their finding a wet surface can produce an output voltage up to three times more than a dry surface.

In this research, a new way of harvesting energy from raindrops by employing piezoelectric material is modeled and simulated. This new approach not only brings more durability to the system because of implementing copper as the base material but also generates higher voltage output due to the truncated shape of the beam.

1.3 Research Objective

This research aims to investigate and evaluate the effects of using piezoelectric material combined with graphene Nanoplatelets reinforced composite (GPLRC).

Also, one practical application of it which is harvesting energy using raindrop is analyzed and a new design is proposed. Towards achieving the main objective, the related aims associated are identified as follows:

1. To investigate frequency characteristics of a GPL reinforced composite microdisk covered with piezoelectric layer;
2. To find the critical voltage for different patterns of GPL reinforced composite microdisk covered with a piezoelectric layer;
3. To obtain the optimal piezoelectric cantilever beam harvester under body load vibration;
4. To enhance the current method of harvesting energy from raindrop by implementing a new shape configuration.

1.4 Significance of the Study

The main objective of this project is to develop the potential of the smart material application using PZT incorporated with GPLRC from the impact of the raindrop that enables to harvest energy-based numerical model.

The significant of the study are briefly explained as follows:

1. This research works on the frequency analysis of a graphene nanoplatelets composite (GPLRC) microdisk which is integrated with a piezoelectric layer in the framework of numerical approach;
2. The findings of this research give a useful suggestion for designing of the GPLRC circular microplate;
3. The modified cantilever beam with a layer of piezoelectric is simulated under two types of excitation from different sources to find the optimum design;
4. This research exposes the potentials of using piezoelectric material as a self-powered sensor in remote areas of Malaysia by proposing a new design configuration.

1.5 Scope and Limitations of the Study

The scope of this study is focused on two main topics:

1. A numerical approach for finding the electrical characteristics (voltage and frequency) based on the generalized differential quadrature method (GDQM) is presented. To derive the equations related to motion, nonlocal strain gradient theory is used. In deriving some of the equations as well as designing the shape of the circular micro-disk layered with piezoelectric MATLAB and ABAQUS software's are used respectively. One of the limitations could be

regarding a perfect bonding between the piezoelectric layer and core which the compatibility conditions for that are derived.

2. A complete and detailed review is done on studying the possible factors which may have any effect on harvesting raindrop using a piezoelectric material. The focus is narrowed down to the impact of a raindrop on the surface of the material. The most well-known piezoelectric material, which is widely used, is PZT (Lead Zirconate Titanate) is used but due to its nature which is extremely brittleness, it causes some limitations. To overcome this copper is used as the base material and the simulation is done with the aid of COMSOL Multi-Physics software.

1.6 Structure of the Thesis

This thesis is structured into 5 chapters by the thesis format of Universiti Putra Malaysia. The details of the thesis structure are presented as follows:

Chapter 1

Problem statements and objectives are presented in this chapter. The significance of the research work and the scope of research are also presented in this chapter.

Chapter 2

This chapter presents a comprehensive literature review on the areas related to the topic of this research. Besides, the research gaps obtained from the review were also clarified within the chapter.

Chapter 3

The methodology used in this research for the preparation of materials, modeling and simulation procedures is presented in this chapter.

Chapter 4

This chapter starts with showing the validations and making a comparison with previous literature. After that, the data analysis is done and discussed in three sections. In the first section the effect of parameters such as ratio of the outer to the inner radius (R_o/R_i), ratios of length scale and nonlocal to thickness (l/h and μ/h), the ratio of piezoelectric to core thickness (h_p/h), microdisk pattern, and GPL weight fraction (g_{GPL}) on critical voltage is shown and discussed. In the second section, the effect of various geometry and tip mass on the voltage output of a cantilever beam supported at one end under body load excitation is presented. In the last part of this

chapter, the impact force of various rain droplets is calculated and the corresponding output voltage for each one is presented.

Chapter 5

This chapter presents the overall conclusions from the whole study as well as future recommendations for further improvement of this study.



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APPENDIX

The governing equations of the GPLRC microdisk are given as follows:

$$\begin{aligned}
 & \delta u_0^i : \\
 & (1-l^2\nabla^2) \left[\begin{array}{l} \frac{\partial}{\partial R} \left[\left[A_{11}^i \frac{\partial u_0^i}{\partial R^i} + B_{11}^i \frac{\partial u_1^i}{\partial R^i} - D_{11}^i c_1 \left(\frac{\partial u_1^i}{\partial R^i} + \frac{\partial^2 w_0^i}{\partial R^{i2}} \right) \right] + \right. \\ \left. \left[A_{12}^i \frac{u_0^i}{R^i} + B_{12}^i \frac{u_1^i}{R} - D_{12}^i c_1 \left(\frac{u_1^i}{R^i} + \frac{\partial w_0^i}{R^i \partial R^i} \right) \right] - X_{31} \phi \right. \\ \left. - \frac{1}{R} \left[\left[A_{12}^i \frac{\partial u_0^i}{\partial R^i} + B_{12}^i \frac{\partial u_1^i}{\partial R^i} - D_{12}^i c_1 \left(\frac{\partial u_1^i}{\partial R^i} + \frac{\partial^2 w_0^i}{\partial R^{i2}} \right) \right] \right. \right. \\ \left. \left. + Q_{22}^i \left[A_{22}^i \frac{u_0^i}{R^i} + B_{22}^i \frac{u_1^i}{R^i} - D_{22}^i c_1 \left(\frac{u_1^i}{R^i} + \frac{\partial w_0^i}{R^i \partial R^i} \right) \right] \right] \right] \\
 & = (1-\mu^2\nabla^2) \left[I_0^i \frac{\partial^2 u_0^i}{\partial t^2} + I_1^i \frac{\partial^2 u_1^i}{\partial t^2} - I_3^i c_1 \left(\frac{\partial^2 u_1^i}{\partial t^2} + \frac{\partial^3 w_0^i}{\partial t^2 \partial R^i} \right) \right] \\
 & ; i = c, p
 \end{aligned} \tag{P-1}$$

δw_0^i :

$$\begin{aligned}
 & \left[c_1 \frac{\partial^2}{\partial R^{i2}} \left[\begin{aligned} & \left[D_{11}^i \frac{\partial u_0^i}{\partial R^i} + E_{11}^i \frac{\partial u_1^i}{\partial R^i} - G_{11}^i c_1 \left(\frac{\partial u_1^i}{\partial R^i} + \frac{\partial^2 w_0^i}{\partial R^{i2}} \right) \right] + \\ & \left[D_{12}^i \frac{u_0^i}{R^i} + E_{12}^i \frac{u_1^i}{R^i} - G_{12}^i c_1 \left(\frac{u_1^i}{R^i} + \frac{\partial w_0^i}{R^i \partial R^i} \right) \right] - X_{33} \phi \end{aligned} \right] \right. \\
 (1-l^2 \nabla^2) & \left. - c_1 \frac{\partial}{R^i \partial R^i} \left[\begin{aligned} & \left[D_{12}^i \frac{\partial u_0^i}{\partial R^i} + E_{12}^i \frac{\partial u_1^i}{\partial R^i} - G_{12}^i c_1 \left(\frac{\partial u_1^i}{\partial R^i} + \frac{\partial^2 w_0^i}{\partial R^{i2}} \right) \right] + \\ & Q_{22}^i \left[D_{22}^i \frac{u_0^i}{R^i} + E_{22}^i \frac{u_1^i}{R^i} - G_{22}^i c_1 \left(\frac{u_1^i}{R^i} + \frac{\partial w_0^i}{R^i \partial R^i} \right) \right] \right] \right. \\
 & \left. + \frac{\partial}{\partial R^i} \left((A_{55}^i - 3C_{55}^i c_1) \left(u_1^i + \frac{\partial w_0^i}{\partial R^i} \right) + X_{11} \partial \phi / \partial R \right) \right. \\
 & \left. - 3c_1 \frac{\partial}{\partial R^i} \left((C_{55}^i - 3E_{55}^i c_1) \left(u_1^i + \frac{\partial w_0^i}{\partial R^i} \right) + X_{12} \partial \phi / \partial R^i \right) - N_1^p w_{0,x^2}^i \right] \\
 & = (1 - \mu^2 \nabla^2) \left[c_1 I_3^i \frac{\partial^3 u_0^i}{\partial R^i \partial t^2} + c_1 I_4^i \frac{\partial^3 u_1^i}{\partial R^i \partial t^2} - I_6^i c_1^2 \left(\frac{\partial^3 u_1^i}{\partial R^i \partial t^2} + \frac{\partial^4 w_0^i}{\partial t^2 \partial R^2} \right) + \left(I_0^i \frac{\partial^2 w_0^i}{\partial t^2} \right) \right] \\
 & ; i = c, p
 \end{aligned} \tag{P-2}$$

δu_1^i :

$$\begin{aligned}
& \left[\begin{aligned} & \frac{\partial}{\partial R^i} \left[\begin{aligned} & \left[B_{11}^i \frac{\partial u_0^i}{\partial R^i} + C_{11}^i \frac{\partial u_1^i}{\partial R^i} - E_{11}^i c_1 \left(\frac{\partial u_1^i}{\partial R^i} + \frac{\partial^2 w_0^i}{\partial R^{i2}} \right) \right] + \\ & \left[B_{12}^i \frac{u_0^i}{R^i} + C_{12}^i \frac{u_1^i}{R^i} - E_{12}^i c_1 \left(\frac{u_1^i}{R^i} + \frac{\partial w_0^i}{R^i \partial R^i} \right) \right] - X_{32} \phi \end{aligned} \right] \\ & - \frac{c_1 \partial}{\partial R^i} \left[\begin{aligned} & \left[D_{11}^i \frac{\partial u_0^i}{\partial R^i} + E_{11}^i \frac{\partial u_1^i}{\partial R^i} - G_{11}^i c_1 \left(\frac{\partial u_1^i}{\partial R^i} + \frac{\partial^2 w_0^i}{\partial R^{i2}} \right) \right] + \\ & \left[D_{12}^i \frac{u_0^i}{R^i} + E_{12}^i \frac{u_1^i}{R^i} - G_{12}^i c_1 \left(\frac{u_1^i}{R^i} + \frac{\partial w_0^i}{R^i \partial R^i} \right) \right] - X_{33} \phi \end{aligned} \right] \\ & - \frac{1}{R^i} \left[\begin{aligned} & \left[B_{12}^i \frac{\partial u_0^i}{\partial R^i} + C_{12}^i \frac{\partial u_1^i}{\partial R^i} - E_{12}^i c_1 \left(\frac{\partial u_1^i}{\partial R^i} + \frac{\partial^2 w_0^i}{\partial R^{i2}} \right) \right] + \\ & Q_{22}^i \left[B_{22}^i \frac{u_0^i}{R^i} + C_{22}^i \frac{u_1^i}{R^i} - E_{22}^i c_1 \left(\frac{u_1^i}{R^i} + \frac{\partial w_0^i}{R^i \partial R^i} \right) \right] \end{aligned} \right] \\ & + \frac{c_1}{R^i} \left[\begin{aligned} & \left[D_{12}^i \frac{\partial u_0^i}{\partial R^i} + E_{12}^i \frac{\partial u_1^i}{\partial R^i} - G_{12}^i c_1 \left(\frac{\partial u_1^i}{\partial R^i} + \frac{\partial^2 w_0^i}{\partial R^{i2}} \right) \right] \\ & + Q_{22}^i \left[D_{22}^i \frac{u_0^i}{R^i} + E_{22}^i \frac{u_1^i}{R^i} - G_{22}^i c_1 \left(\frac{u_1^i}{R^i} + \frac{\partial w_0^i}{R^i \partial R^i} \right) \right] \end{aligned} \right] \\ & - \left[(A_{55}^i - 3C_{55}^i c_1) \left(u_1^i + \frac{\partial w_0^i}{\partial R^i} \right) + X_{11} \partial \phi / \partial R^i \right] \\ & + 3c_1 \left[S_{Rz}^i = (C_{55}^i - 3E_{55}^i c_1) \left(u_1^i + \frac{\partial w_0^i}{\partial R^i} \right) + X_{12} \partial \phi / \partial R^i \right] \end{aligned} \right] \quad (P-3) \\
& = (1 - \mu^2 \nabla^2) \left[\begin{aligned} & I_1^i \frac{\partial^2 u_0^i}{\partial t^2} + I_2^i \frac{\partial^2 u_1^i}{\partial t^2} - I_4^i c_1 \left(\frac{\partial^2 u_1^i}{\partial t^2} + \frac{\partial^3 w_0^i}{\partial t^2 \partial R^i} \right) - c_1 I_3^i \frac{\partial^2 u_0^i}{\partial t^2} \\ & - c_1 I_4^i \frac{\partial^2 u_1^i}{\partial t^2} + I_6^i c_1^2 \left(\frac{\partial^2 u_1^i}{\partial t^2} + \frac{\partial^3 w_0^i}{\partial t^2 \partial R^i} \right) \end{aligned} \right] \\
& ; i = c, p
\end{aligned}$$

$\delta \phi$;

$$\begin{aligned}
& \left(\begin{aligned} & + X_{31} \frac{\partial u_0^p}{\partial R^p} + (X_{11} - 3X_{12}) \frac{\partial^2 w_0^p}{\partial R^{p2}} - X_{33} \frac{\partial^2 w_0^p}{\partial R^{p2}} \\ & - (-X_{11} + 3X_{12}) \frac{\partial u_1^p}{\partial R^p} + X_{32} \frac{\partial u_1^p}{\partial R^p} - X_{33} \frac{\partial u_1^p}{\partial R^p} \\ & - X_{41} \frac{\partial^2 \phi}{\partial R^{p2}} + X_{42} \phi \end{aligned} \right) = 0 \quad (P-4)
\end{aligned}$$

The GDQ form of the governing equations of the GPLRC microdisk are given as below:

$$\begin{aligned}
 & \delta u_0^i : \\
 & (1-l^2 \left(\sum_{v=1}^{N_n} C_{n,v}^{(2)} + \sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{1}{R^i} \right)) \left[\left(\left[\begin{aligned} & A_{11}^i \sum_{v=1}^{N_n} C_{n,v}^{(2)} u_0^i + B_{11}^i \sum_{v=1}^{N_n} C_{n,v}^{(2)} u_1^i \\ & - D_{11}^i c_1 \left(\sum_{v=1}^{N_n} C_{n,v}^{(2)} u_1^i + \sum_{v=1}^{N_n} C_{n,v}^{(2)} w_0^i \right) \end{aligned} \right] + \left[\begin{aligned} & A_{12}^i \sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{u_0^i}{R_n^i} + B_{12}^i \sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{u_1^i}{R_n^i} \\ & - D_{12}^i c_1 \left(\sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{u_1^i}{R_n^i} + \sum_{v=1}^{N_n} C_{n,v}^{(2)} \frac{w_0^i}{R_n^i} \right) \end{aligned} \right] - X_{31} \sum_{v=1}^{N_n} C_{n,v}^{(1)} \phi_n \right) \right. \\
 & \left. - \frac{1}{R} \left[\begin{aligned} & A_{12}^i \sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{u_0^i}{R_n^i} + B_{12}^i \sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{u_1^i}{R_n^i} - \\ & D_{12}^i c_1 \left(\sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{u_1^i}{R_n^i} + \sum_{v=1}^{N_n} C_{n,v}^{(2)} \frac{w_0^i}{R_n^i} \right) \end{aligned} \right] \right. \\
 & \left. + Q_{22}^i \left[\begin{aligned} & A_{22}^i \sum_{v=1}^{N_n} \frac{u_0^i}{R_n^2} + B_{22}^i \sum_{v=1}^{N_n} \frac{u_1^i}{R_n^2} - \\ & D_{22}^i c_1 \left(\sum_{v=1}^{N_n} \frac{u_1^i}{R_n^2} + \sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{w_0^i}{R_n^2} \right) \end{aligned} \right] \right) \right] \\
 & = (1-\mu^2 \left(\sum_{v=1}^{N_n} C_{n,v}^{(2)} + \sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{1}{R^i} \right)) \left[I_0^i \sum_{v=1}^{N_n} \omega^2 u_0^i I_v + I_1^i \sum_{v=1}^{N_n} \omega^2 u_1^i I_v - I_3^i c_1 \left(\sum_{v=1}^{N_n} \omega^2 u_1^i I_v + \sum_{v=1}^{N_n} C_{n,v}^{(1)} \omega^2 w_0^i I_v \right) \right] \\
 & ; i = c, p
 \end{aligned} \tag{P-5}$$

δw_0^i :

$$\begin{aligned}
 & \left((1-l^2) \begin{pmatrix} \sum_{v=1}^{N_n} C_{n,v}^{(2)} + \\ \sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{1}{R^i} \end{pmatrix} \right) \left[\begin{aligned}
 & c_1 \left[\begin{aligned}
 & \left(\begin{aligned}
 & D_{11}^i \sum_{v=1}^{N_n} C_{n,v}^{(3)} u_0^i + E_{11}^i \sum_{v=1}^{N_n} C_{n,v}^{(3)} u_1^i \\
 & -G_{11}^i c_1 \left(\sum_{v=1}^{N_n} C_{n,v}^{(3)} u_1^i + \sum_{v=1}^{N_n} C_{n,v}^{(4)} w_0^i \right)
 \end{aligned} \right) + \\
 & \left[\begin{aligned}
 & D_{12}^i \sum_{v=1}^{N_n} C_{n,v}^{(2)} \frac{u_0^i}{R_n^i} + E_{12}^i \sum_{v=1}^{N_n} C_{n,v}^{(2)} \frac{u_1^i}{R_n^i} \\
 & -G_{12}^i c_1 \left(\sum_{v=1}^{N_n} C_{n,v}^{(2)} \frac{u_1^i}{R_n^i} + \sum_{v=1}^{N_n} C_{n,v}^{(3)} \frac{w_0^i}{R_n^i} \right)
 \end{aligned} \right] - X_{33} \sum_{v=1}^{N_n} C_{n,v}^{(2)} \phi
 \end{aligned} \right] \\
 & -c_1 \left[\begin{aligned}
 & \left(\begin{aligned}
 & D_{12}^i \sum_{v=1}^{N_n} C_{n,v}^{(2)} \frac{u_0^i}{R_n^i} + E_{12}^i \sum_{v=1}^{N_n} C_{n,v}^{(2)} \frac{u_1^i}{R_n^i} \\
 & -G_{12}^i c_1 \left(\sum_{v=1}^{N_n} C_{n,v}^{(2)} \frac{u_1^i}{R_n^i} + \sum_{v=1}^{N_n} C_{n,v}^{(3)} \frac{w_0^i}{R_n^i} \right)
 \end{aligned} \right) + \\
 & \left[\begin{aligned}
 & D_{22}^i \sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{u_0^i}{R_n^{2i}} + E_{22}^i \sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{u_1^i}{R_n^{2i}} \\
 & -G_{22}^i c_1 \left(\sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{u_1^i}{R_n^{2i}} + \sum_{v=1}^{N_n} C_{n,v}^{(2)} \frac{w_0^i}{R_n^{2i}} \right)
 \end{aligned} \right]
 \end{aligned} \right] \\
 & + \left(A_{55}^i - 3C_{55}^i c_1 \right) \left(\sum_{v=1}^{N_n} C_{n,v}^{(1)} u_1^i + \sum_{v=1}^{N_n} C_{n,v}^{(2)} w_0^i \right) + X_{11} \sum_{v=1}^{N_n} C_{n,v}^{(2)} \phi \\
 & -3c_1 \left(\begin{aligned}
 & \left(C_{55}^i - 3E_{55}^i c_1 \right) \left(\sum_{v=1}^{N_n} C_{n,v}^{(1)} u_1^i + \sum_{v=1}^{N_n} C_{n,v}^{(1)} w_0^i \right) \\
 & + X_{12} \sum_{v=1}^{N_n} C_{n,v}^{(2)} \phi
 \end{aligned} \right) - N_1^P \sum_{v=1}^{N_n} C_{n,v}^{(2)} w_0^i
 \end{aligned} \right] \\
 & = (1-\mu^2) \begin{pmatrix} \sum_{v=1}^{N_n} C_{n,v}^{(2)} + \\ \sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{1}{R^i} \end{pmatrix} \left[\begin{aligned}
 & c_1 I_3^i \sum_{v=1}^{N_n} C_{n,v}^{(1)} \omega^2 u_0^i I_v + c_1 I_4^i \sum_{v=1}^{N_n} C_{n,v}^{(1)} \omega^2 u_1^i I_v \\
 & -I_6^i c_1^2 \left(\sum_{v=1}^{N_n} C_{n,v}^{(1)} \omega^2 u_1^i I_v + \sum_{v=1}^{N_n} C_{n,v}^{(2)} \omega^2 w_0^i I_v \right) + \left(I_0^i \sum_{v=1}^{N_n} \omega^2 w_0^i I_v \right)
 \end{aligned} \right]
 \end{aligned}
 \tag{P-6}$$

$; i = c, p$

δu_1^i :

$$\begin{aligned}
& \left(\begin{array}{l} \sum_{v=1}^{N_n} C^{(2)}_{n,v} + \\ \sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{1}{R^i} \end{array} \right) \left[\begin{array}{l} \left[\begin{array}{l} B_{11}^i \sum_{v=1}^{N_n} C^{(2)}_{n,v} u_0^i + C_{11}^i \sum_{v=1}^{N_n} C^{(2)}_{n,v} u_1^i - E_{11}^i c_1 \left(\sum_{v=1}^{N_n} C^{(2)}_{n,v} u_1^i + \sum_{v=1}^{N_n} C^{(3)}_{n,v} w_0^i \right) + \\ \left[\begin{array}{l} B_{12}^i \sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{u_0^i}{R_n^i} + C_{12}^i \sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{u_1^i}{R_n^i} - \\ E_{12}^i c_1 \left(\sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{u_1^i}{R_n^i} + \sum_{v=1}^{N_n} C^{(2)}_{n,v} \frac{w_0^i}{R_n^i} \right) \end{array} \right] - X_{32} \sum_{v=1}^{N_n} C^{(1)}_{n,v} \phi \\ \left[\begin{array}{l} D_{11}^i \sum_{v=1}^{N_n} C^{(2)}_{n,v} u_0^i + E_{11}^i \sum_{v=1}^{N_n} C^{(2)}_{n,v} u_1^i - G_{11}^i c_1 \left(\sum_{v=1}^{N_n} C^{(2)}_{n,v} u_1^i + \sum_{v=1}^{N_n} C^{(3)}_{n,v} w_0^i \right) + \\ \left[\begin{array}{l} D_{12}^i \sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{u_0^i}{R_n^i} + E_{12}^i \sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{u_1^i}{R_n^i} - \\ G_{12}^i c_1 \left(\sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{u_1^i}{R_n^i} + \sum_{v=1}^{N_n} C^{(2)}_{n,v} \frac{w_0^i}{R_n^i} \right) \end{array} \right] - X_{33} \sum_{v=1}^{N_n} C^{(1)}_{n,v} \phi \end{array} \right] + \\ \left[\begin{array}{l} B_{12}^i \sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{u_0^i}{R_n^i} + C_{12}^i \sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{u_1^i}{R_n^i} \\ -E_{12}^i c_1 \left(\sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{u_1^i}{R_n^i} + \sum_{v=1}^{N_n} C^{(2)}_{n,v} \frac{w_0^i}{R_n^i} \right) \end{array} \right] + \\ Q_{22}^i \left[\begin{array}{l} B_{22}^i \sum_{v=1}^{N_n} \frac{u_0^i}{R_n^{2i}} + C_{22}^i \sum_{v=1}^{N_n} \frac{u_1^i}{R_n^{2i}} - E_{22}^i c_1 \left(\sum_{v=1}^{N_n} \frac{u_1^i}{R_n^{2i}} + \sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{w_0^i}{R_n^{2i}} \right) \\ \left[\begin{array}{l} D_{12}^i \sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{u_0^i}{R_n^i} + E_{12}^i \sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{u_1^i}{R_n^i} \\ -G_{12}^i c_1 \left(\sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{u_1^i}{R_n^i} + \sum_{v=1}^{N_n} C^{(2)}_{n,v} \frac{w_0^i}{R_n^i} \right) \end{array} \right] \\ + Q_{22}^i \left[\begin{array}{l} D_{22}^i \sum_{v=1}^{N_n} \frac{u_0^i}{R_n^{2i}} + E_{22}^i \sum_{v=1}^{N_n} \frac{u_1^i}{R_n^{2i}} - G_{22}^i c_1 \left(\sum_{v=1}^{N_n} \frac{u_1^i}{R_n^{2i}} + \sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{w_0^i}{R_n^{2i}} \right) \end{array} \right] \\ - \left[\begin{array}{l} (A_{55}^i - 3C_{55}^i c_1) \left(\sum_{v=1}^{N_n} u_0^i I_v + \sum_{v=1}^{N_n} C^{(1)}_{n,v} w_0^i \right) + X_{11} \sum_{v=1}^{N_n} C^{(1)}_{n,v} \phi \\ + 3c_1 \left((C_{55}^i - 3E_{55}^i c_1) \left(\sum_{v=1}^{N_n} u_1^i I_v + \sum_{v=1}^{N_n} C^{(1)}_{n,v} w_0^i \right) + X_{12} \sum_{v=1}^{N_n} C^{(1)}_{n,v} \phi \right) \end{array} \right] \\ \left[\begin{array}{l} I_1^i \sum_{v=1}^{N_n} \omega^2 u_0^i I_v + I_2^i \sum_{v=1}^{N_n} \omega^2 u_1^i I_v - I_4^i c_1 \left(\sum_{v=1}^{N_n} \omega^2 u_1^i I_v + \sum_{v=1}^{N_n} C^{(1)}_{n,v} \omega^2 w_0^i I_v \right) \\ - c_1 I_3^i \sum_{v=1}^{N_n} \omega^2 u_0^i I_v - c_1 I_4^i \sum_{v=1}^{N_n} \omega^2 u_1^i I_v \\ + I_6^i c_1^2 \left(\sum_{v=1}^{N_n} \omega^2 u_1^i I_v + \sum_{v=1}^{N_n} C^{(1)}_{n,v} \omega^2 w_0^i I_v \right) \end{array} \right] \end{array} \right] + \\ \left. \begin{array}{l} \left(\begin{array}{l} \sum_{v=1}^{N_n} C^{(2)}_{n,v} + \\ \sum_{v=1}^{N_n} C^{(1)}_{n,v} \frac{1}{R^i} \end{array} \right) \left[\begin{array}{l} I_1^i \sum_{v=1}^{N_n} \omega^2 u_0^i I_v + I_2^i \sum_{v=1}^{N_n} \omega^2 u_1^i I_v - I_4^i c_1 \left(\sum_{v=1}^{N_n} \omega^2 u_1^i I_v + \sum_{v=1}^{N_n} C^{(1)}_{n,v} \omega^2 w_0^i I_v \right) \\ - c_1 I_3^i \sum_{v=1}^{N_n} \omega^2 u_0^i I_v - c_1 I_4^i \sum_{v=1}^{N_n} \omega^2 u_1^i I_v \\ + I_6^i c_1^2 \left(\sum_{v=1}^{N_n} \omega^2 u_1^i I_v + \sum_{v=1}^{N_n} C^{(1)}_{n,v} \omega^2 w_0^i I_v \right) \end{array} \right] \end{array} \right] ; i = c, p \end{aligned} \tag{P-7}$$

$\delta\phi$:

$$(1-l^2 \left(\begin{array}{c} \sum_{v=1}^{N_n} C_{n,v}^{(2)} + \\ \sum_{v=1}^{N_n} C_{n,v}^{(1)} \frac{1}{R^i} \end{array} \right) \left(\begin{array}{c} +X_{31} \sum_{v=1}^{N_n} C_{n,v}^{(1)} u^p_0 + (X_{11} - 3X_{12} - X_{33}) \sum_{v=1}^{N_n} C_{n,v}^{(2)} w^p_0 \\ -(-X_{11} + 3X_{12} - X_{32} + X_{33}) \sum_{v=1}^{N_n} C_{n,v}^{(1)} u^p_1 \\ -X_{41} \sum_{v=1}^{N_n} C_{n,v}^{(2)} \phi + X_{42} \sum_{v=1}^{N_n} \phi I_v \end{array} \right) = 0 \quad (\text{P-8})$$



BIODATA OF STUDENT



The student Erfan Shamsaddini Lori was born on the 9th September 1989 in Bandarabbas, Iran. He received his early primary education at Abu Ali Sina School, Kerman from 1996 to 2000. Then he completed his secondary school at ImamAli School and Olum Pezeshki School, Kerman from 2001 to 2006. Then, proceeded to pursue his foundation in Engineering in 2006 at Multimedia University, Melaka Campus (MMU), Melaka, Malaysia. Then proceeded to pursue his Bachelor's Degree in Mechanical Engineering in 2008 at Multimedia University (MMU). Upon completing his BSc (Hons) in 2013, he continued his learning journey by undertaking a Master degree in the field of manufacturing systems at Universiti Putra Malaysia (UPM). Immediately after his graduation on 2016 he became a PhD candidate in the field of Mechanical Engineering at Universiti Putra Malaysia (UPM). His main research interests are: (1) material engineering (polymer composites, smart materials, piezoelectric) and (2) sustainable energy. He has authored and published more than 6 citation indexed journals on piezoelectric materials with new approach of harvesting energy.

LIST OF PUBLICATIONS

Journal Articles

Erfan Shamsaddini Lori, Ebrahimi, F., Supeni, E. E. B., Habibi, M., & Safarpour, H. (2020). Frequency characteristics of a GPL-reinforced composite microdisk coupled with a piezoelectric layer. *The European Physical Journal Plus*, 135(2), 144. (Published) [Q2, Impact factor: 2.24]

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