



**UNIVERSITI PUTRA MALAYSIA**

***EFFECT OF SURFACE ROUGHNESS ON HELICOPTER MAIN ROTOR  
BLADE***

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**EFFECT OF SURFACE ROUGHNESS ON HELICOPTER MAIN ROTOR  
BLADE**

By

**WAN NORHAFIZAN BIN WAN ROHIZAN**

**Thesis Submitted to the School of Graduate Studies, Universiti Putra  
Malaysia, in Fulfilment of the Requirements for the Degree of  
Master of Science**

**April 2017**

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Abstract of thesis presented to the Senate of Universiti Putra Malaysia in  
fulfilment of the requirement for the Degree of Master of Science

## **EFFECT OF SURFACE ROUGHNESS ON HELICOPTER MAIN ROTOR BLADE**

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**April 2017**

**Chair: Assoc. Prof. Azmin Shakrine bin Mohd Rafie, PhD**  
**Faculty: Engineering**

This study describes the effect of surface roughness when applied on helicopter main rotor blade. The study was performed in wind tunnel using scaled helicopter model to study the aerodynamic characteristic in vertical flight condition. This is to show the feasibility of surface roughness for rotary wing applications. The requirement for helicopter main rotor blades are high thrust and low power requirement. Smooth profile of main rotor blade is modified by applying surface roughness on the upper and lower camber in transition and turbulent boundary layer region; starting from 25% of chord length and gradually extended to trailing edge (TE). The analysis following the research shows that with right application of roughness will result in lower power requirement. The aerodynamic efficiency is enhanced at lower and upper pitch level between 7% to 69%. However, this came at the expense of reduced thrust at middle collective pitch level between 11% to 45%. Surface roughness found to have insignificant effect on rotor power requirement (only 2% to 5% difference). At upper range of collective pitch level, surface roughness is seen to delay the stall angle as well as increasing the lift in the stall region. Meanwhile for aerodynamic efficiency, thrust-to-power ratio shows less steep graph and peak ratio were pushed to higher pitch level. This indicates wider operating envelope and more predictable flight profile. All these results may provide foundation for further research to further optimisation of surface roughness effect for rotary wing aircraft.

Abstrak tesis yang dipersembahkan kepada Senat Universiti Putra Malaysia  
sebagai memenuhi keperluan untuk ijazah Master Sains

## KESAN KEKASARAN PERMUKAAN PADA BILAH ROTOR UTAMA HELIKOPTER

Oleh

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April 2017

**Pengerusi: Prof. Madya Azmin Shakrine bin Mohd Rafie, PhD**  
**Fakulti: Kejuruteraan**

Kajian ini menerangkan kesan kekasaran permukaan apabila diaplikasikan pada bilah rotor utama helikopter. Kajian dijalankan dalam terowong angin menggunakan model skala helikopter bagi mengkaji ciri-ciri aerodinamik dalam keadaan penerbangan menegak. Ini bagi membuktikan kesesuaian kekasaran permukaan bagi aplikasi sayap putar. Profil asal bilah rotor diubah dengan meletakkan permukaan kasar di bahagian atas dan bawah, mulai daripada 25% *chord length* dan beransur-ansur ditambah sehingga ke *Trailing Edge* (TE). Analisis daripada eksperimen tersebut menunjukkan: Dengan aplikasi yang betul akan memberikan keperluan kuasa yang lebih rendah; Keberkesanan aerodinamik lebih baik dapat dicapai pada julat dongakan bawah dan tinggi dengan penambahbaikan antara 7% hingga 69%. Namun, pemnambahbaikan ini datang dengan pengurangan tujuh di julat pertengahan antara 11% hingga 45%. Kekasaran permukaan didapati mempunyai kesan yang tidak signifikan kepada keperluan kuasa rotor (hanya perbezaan antara 2% hingga 5%). Di julat atas, kekasaran permukaan diperhatikan meningkatkan sudut pegun di samping meningkatkan tujuh di zon pegun. Manakala bagi keberkesanan aerodinamik, nisbah tujuh-kepada-kuasa menunjukkan graf yang kurang curam dan nisbah maksimum berada di sudut dongakan yang lebih tinggi. Keadaan ini menunjukkan julat operasi yang lebih lebar dan profil penerbangan yang lebih mudah dijangka. Semua hasil kajian ini boleh menjadi asas untuk kajian seterusnya bagi lebih optimisasi kesan kekasaran permukaan untuk pesawat sayap putar.

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This is to confirm that:

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## TABLE OF CONTENTS

	Page
<b>ABSTRACT</b>	i
<b>ABSTRAK</b>	ii
<b>ACKNOWLEDGEMENTS</b>	iii
<b>APPROVAL</b>	iv
<b>DECLARATION</b>	vi
<b>LIST OF TABLES</b>	x
<b>LIST OF FIGURES</b>	xi
<b>LIST OF NOMENCLATURE</b>	xiii
 <b>CHAPTER</b>	
<b>1</b>	
<b>INTRODUCTION</b>	<b>1</b>
1.1 Background	1
1.2 Helicopter Rotor Blade	8
1.3 Problem Statement	8
1.4 Objective	9
1.5 Scope	9
1.6 Thesis Layout	10
 <b>2</b>	
<b>LITERATURE REVIEW</b>	<b>11</b>
2.1 Flow Control Method	11
2.2 Coanda Effect	12
2.3 Experimental Work	14
2.4 Computational Work	22
2.5 Helicopter Aerodynamic Theory	26
2.5.1 Blade Element Theory	26
2.5.2 Rotor Solidity	28
2.6 Summary	28
 <b>3</b>	
<b>METHODOLOGY</b>	<b>29</b>
3.1 Research Flow Chart	29
3.2 Model Selection	30
3.3 Experimental Apparatus	31
3.3.1 The Wind Tunnel	31
3.3.2 Six Component Balance	32
3.3.3 Multi Range Tachometer	33
3.3.4 Power Supply	34
3.3.5 Helicopter Mounting	34
3.3.6 Roughness Paper	35
3.4 Experimental Setup	36
3.4.1 Surface Roughness Arrangement	36
3.4.2 Model Setup	37
3.5 Experimental Procedures	38
3.5.1 Error Analysis	40
3.6 Similitude Study	41
3.6.1 Kinematic Similarity	42
3.6.2 Dynamic Similarity	43

3.7	Data Collection	44
<b>4</b>	<b>RESULTS AND DISCUSSION</b>	46
4.1	Baseline Model	46
4.1.1	Thrust for Baseline Model	46
4.1.2	Power for Baseline Model	47
4.1.3	Thrust-to-Power Ratio for Baseline Model	48
4.2	Roughness Model	49
4.2.1	Thrust for Roughness Model	49
4.2.2	Power for Roughness Model	50
4.2.3	Thrust to Power Ratio for Roughness Model	51
4.3	Comparison Baseline Vs. Roughness Model	52
4.4	Summary	56
<b>5</b>	<b>CONCLUSION</b>	57
5.1	Recommendations	58
5.2	Research Contributions	58
	<b>REFERENCES</b>	59
	<b>APPENDICES</b>	63
	<b>BIODATA OF STUDENT</b>	67

## LIST OF TABLES

Table		Page
2.1	Optimisation Results	22
2.2	Applied LE Roughness	25
3.1	Scaled Helicopter vs Real Helicopter Specification and Scaling Factor	30
3.2	Sand Paper Roughness Details	36
3.3	Main Rotor Blade Rotational Speed	39
3.4	Helicopter Model Operating Parameter	40
3.5	Error Analysis for Baseline Readings	40
3.6	Error Analysis for 25% - 50% Roughness Readings	40
3.7	Error Analysis for 25% - 75% Roughness Readings	41
3.8	Error Analysis for 25% - TE Roughness Readings	41
3.9	Comparison Between Scaled Model and Real Helicopter Rotor Blade	42

## LIST OF FIGURES

Figure		Page
1.1	Chinese Bamboo-copter	1
1.2	Leonardo da Vinci's "Helicopter"	2
1.3	Sir George Cayley's "Aerial Carriage"	3
1.4	Paul Cornu's "Cornu Helicopter"	4
1.5	Boeing CH-47 Chinook	5
1.6	Airbus Helicopters' X3	5
1.7	Bell-Boeing V-22 Osprey	6
1.8	Kamov Ka-27 "Helix"	6
1.9	Turboshaft Gas Turbine Schematics	7
2.1	Henri Coanda's Coanda-1910	12
2.2	Deflection of jet stream using Coanda Effect	13
2.3	Illustration of Coanda Effect	13
2.4	Application of triangular roughness on upper and lower camber of an airfoil	14
2.5	$C_L$ vs $\alpha$ for Lower Triangular Roughness	15
2.6	$C_D$ vs $\alpha$ for Lower Triangular Roughness	15
2.7	Aerodynamic Efficiency ( $C_L/C_D$ Ratio) vs $\alpha$ for Lower Triangular Roughness	16
2.8	Cross-section of model and definition of flap perimeters	16
2.9	The airfoil-flap model with VG (left) and cylinder (right)	17
2.10	Baseline Lift Polar and Flap Deflection Angle	17
2.11	VG Geometry and Construction Method	18
2.12	VG Lift Polar and Position of VG on the Airfoil	19
2.13	Definition of Cylinder Position	20
2.14	Cylinder Geometrical Definitions	20
2.15	Cylinder Lift Polar and Position of Cylinder on the Airfoil	21
2.16	Optimisation results of NACA 0012 Airfoil	23
2.17	Blade profile at the final set of optimisation cycle	24
2.18	Pressure contours at the upper surface	24
2.19	Microscopy measurements of different roughness tapes. Left: Roughness Level 1, Centre: Roughness Level 2, Right: Roughness Level 3	25
2.20	RFOIL vs Experimental Result	25
2.21	ANSYS CFX vs Experimental Result	26
2.22	Blade Section Aerodynamics	26
2.23	Blade Section Nomenclature	27
3.1	Experimental Flow Chart	29
3.2	ROBAN AS350 470 Model	30
3.3	OWLT-1000 Wind Tunnel	31
3.4	Six Component Balance	32
3.5	Computer	32
3.6	Multi-range Tachometer	33
3.7	Reflective Sticker on Main Rotor Blade	33
3.8	Power Converter	34
3.9	Helicopter Mounting	35
3.10	Sand Paper	35

3.11	Region covered by roughness on the upper and lower surface	36
3.12	Surface Roughness Applied on the Upper Surface of Main Rotor Blade (covering 25% of airfoil and located 25% from LE)	37
3.13	Surface Roughness Applied on the Lower Surface of Main Rotor Blade (covering 25% of airfoil and located 25% from LE)	37
3.14	Helicopter Model Mounted on Six-component Balance	38
3.15	Rotational Speed Measurement	39
4.1	$C_T/s$ vs. Collective Pitch Level for Baseline Model	47
4.2	$C_P/s$ vs. Collective Pitch Level for Baseline Model	48
4.3	$C_T/C_P$ Ratio vs. Collective Pitch Level for Baseline Model	49
4.4	$C_T/s$ vs. Collective Pitch Level for Roughness Model	50
4.5	$C_P/s$ vs. Collective Pitch Level for Roughness Model	51
4.6	$C_T/C_P$ Ratio vs. Collective Pitch Level for Roughness Model	52
4.7	$C_T/s$ vs. Collective Pitch Level for Baseline, 25% Roughness, 50% Roughness and 75% Roughness Models	53
4.8	$C_P/s$ vs. Collective Pitch Level for Baseline, 25% Roughness, 50% Roughness and 75% Roughness Models	53
4.9	$C_T/C_P$ Ratio vs. Collective Pitch Level for Baseline, 25% Roughness, 50% Roughness and 75% Roughness Models	55

## LIST OF NOMENCLATURE

Re	Reynolds Number
CFD	Computational Fluid Dynamics
TE	Trailing Edge
VG	Vortex Generator
LE	Leading Edge
$\alpha$	Angle of Attack
$U$	Relative Wind
$\theta$	Pitch Angle
$\rho$	Air Density
$A$	Rotor Disc Area
$C_T$	Coefficient of Thrust
$C_P$	Coefficient of Power
$V_T$	Tip Speed of Rotor Blade
$s$	Rotor Solidity
$N$	Number of Blades
$c$	Chord Length
$R$	Rotor Swept Radius
$I$	Current
$V$	Voltage
$P$	Power
$C_L$	Coefficient of Lift
$C_D$	Coefficient of Drag
$\omega$	Angular Speed
$\mu$	Dynamic Viscosity

## CHAPTER 1

### INTRODUCTION

The advent of helicopter is considered one of the most important milestones in aviation. Even though the development started later and not much publicised compared to the development of fixed wing aircraft, the versatility of helicopter makes it a choice among civilian and military operators. It is also observed that aerodynamics of helicopter is largely influenced by rotor blade aerodynamics, and aerodynamic design of its airframe has lesser influence on flight performance compared to fixed wing aircraft. Therefore, this study is focused on helicopter rotor blades in order to enhance flight performance.

#### 1.1 Background

Helicopter is a type of rotorcraft (also known as rotary wing aircraft) that uses rotating wings (known as blades) to fly. As mentioned by Johnson (2013), the rotor blades rotate depicting a disk in horizontal (or almost horizontal) plane. A helicopter with its rotating blades can generate aerodynamic forces via its motion relative to the air. Given this feature (which is unique to a rotorcraft), these forces can be produced even though the velocity of the airframe is zero, in contradiction of fixed-wing aircraft in which the airframe needs translational velocity to sustain flight (Johnson, 2013).

According to Seddon and Newman (2011), the history of rotary-winged flight can be traced from 400 B.C. with a toy known as Chinese top or bamboo-copter (Figure 1.1). It was constructed with a shaft attached to wings inclined to the rotation plane normal to the shaft. When spun between the hands and released, it generated thrust which allow it to fly for a short time. Even though simple, it provided inspiration for invention of helicopters.

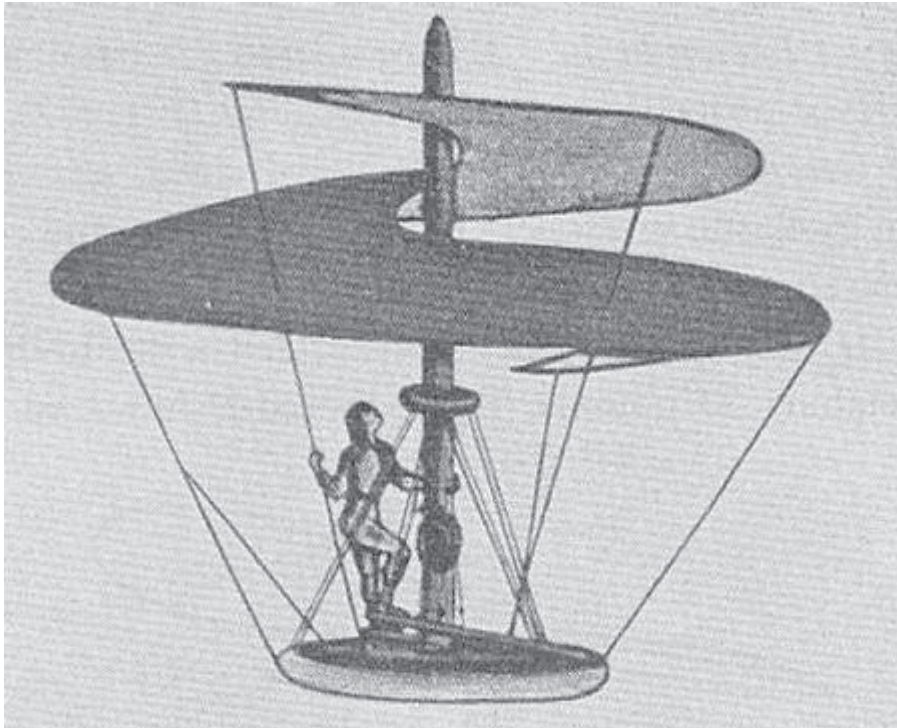


**Figure 1.1: Chinese Bamboo-copter**

(Source: [kaleidoscope.cultural-china.com/en/144Kaleidoscope1053.html](http://kaleidoscope.cultural-china.com/en/144Kaleidoscope1053.html))



A famous artist and inventor Leonardo da Vinci conceived his design of a helicopter (Figure 1.2). Similar to many of his ideas, the design never left the drawing board, but the drawings and notes charted exactly how a helicopter would operate. With the purpose of compressing air to obtain flight, the helical screw on his design formed a basis on how a helicopter rotor blade would be.

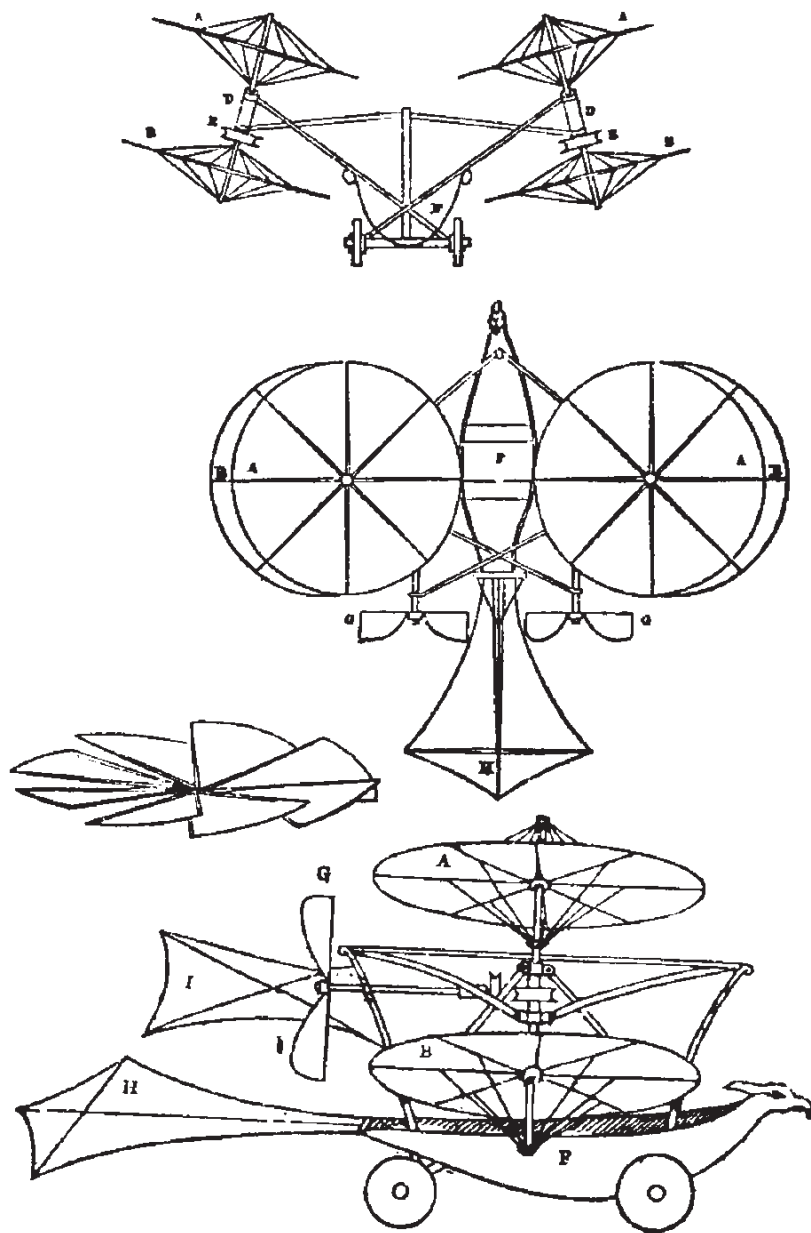


**Figure 1.2: Leonardo da Vinci's "Helicopter"**

(Source: <http://www.aerospaceweb.org/design/helicopter/history.shtml>)

Meanwhile, Sir George Cayley wrote an aeronautical paper which laid the foundation for future helicopter development (Seddon and Newman, 2011). He envisioned an air vehicle consisting of two pairs of contra-rotating rotors arranged coaxially to generate lifting thrust. The forward propulsion of this so-called "aerial carriage" was provided by two propellers mounted at the rear. This design was the sign of many features of modern rotary-winged craft. This awkward design (Figure 1.3) was an improvement compared to other contemporary projects; however due to unavailability of suitable propulsion, the project never materialised.



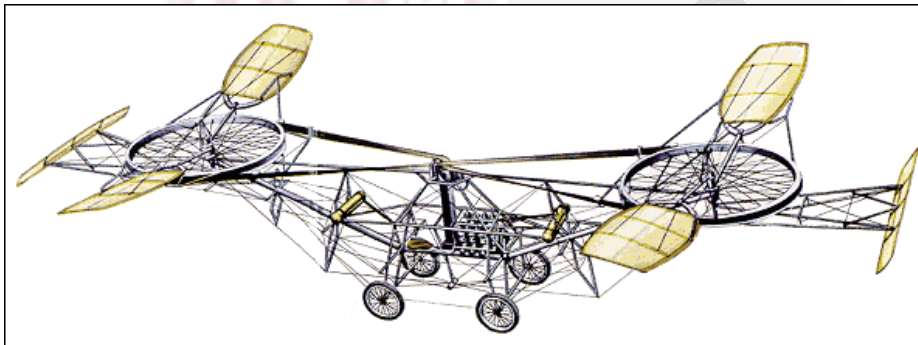


**Figure 1.3: Sir George Cayley's "Aerial Carriage"**  
 (Source: [http://www.aviastar.org/helicopters\\_eng/cayley.php](http://www.aviastar.org/helicopters_eng/cayley.php))

American inventor, Thomas Alva Edison was facing the same problem that Cayley and other aircraft experimenters had; which was lack of suitable propulsion ([www.aviastar.org/history](http://www.aviastar.org/history)). In 1880, he examined the thrust vs. power performance. He tested on various designs of rotor blades in order to find out those with the best lifting power. With only electric motor at his disposal (since internal combustion engines did not yet exist), he found it as unsuitable for the

purpose. With this in mind, he shifted his focus to the engine instead. He was thinking of one with small weight with a good amount of horsepower. In a notable attempt, he used gun cotton in the cylinder of an engine fired with a spark. He attained good results, but at the expense of near-fatal injury to him and one of his colleagues.

This incident forced him to abandon his helicopter experiments and focused on more pressing work. Nevertheless, his work provided estimation of the required power-to-weight ratio for a workable helicopter to be achieved (Seddon and Newman, 2011). He concluded, no helicopter would be able to fly until engines with power to weight ratio of 3 to 4 lb/hp were available (Johnson, 2013). In parallel with this finding, he also confirmed that the most suitable propulsion means for helicopter is the one with high power-to-weight ratio.



**Figure 1.4: Paul Cornu's "Cornu Helicopter"**

(Source: [http://www.aviastar.org/helicopters\\_eng/cornu.php](http://www.aviastar.org/helicopters_eng/cornu.php))

Meanwhile in 1906, a Frenchman, Paul Cornu pioneered first free flight of helicopter. His twin-rotored helicopter (Figure 1.4) rose to between 1 and 5 feet of altitude for a period of 20 seconds. This is considered a significant milestone, since the flight controls entirely achieved from the aircraft without any interference or attachment from the ground, hence giving the distinction of first free flight of helicopter. Since then progressive developments have been made until the birth of Focke-Wulf 61 as first operational helicopter in 1936. This is later followed by Sikorsky's R-4 helicopter which became the first mass-produced helicopter in 1942. Since then helicopter has evolved into multiple type of configurations; from its earlier designs of more than one main rotor, to single main rotor with anti-torque tail rotor arrangement, tandem rotors (Figure 1.5), compound helicopter (Figure 1.6), tiltrotor (Figure 1.7) and coaxial helicopter (Figure 1.8).



**Figure 1.5: Boeing CH-47 Chinook**  
(Source: [http://www.militaryfactory.com/aircraft/detail.asp?aircraft\\_id=56](http://www.militaryfactory.com/aircraft/detail.asp?aircraft_id=56))



**Figure 1.6: Airbus Helicopters' X3**  
(Source: [http://www.militaryfactory.com/aircraft/detail.asp?aircraft\\_id=880](http://www.militaryfactory.com/aircraft/detail.asp?aircraft_id=880))



**Figure 1.7: Bell-Boeing V-22 Osprey**  
(Source: US Navy)

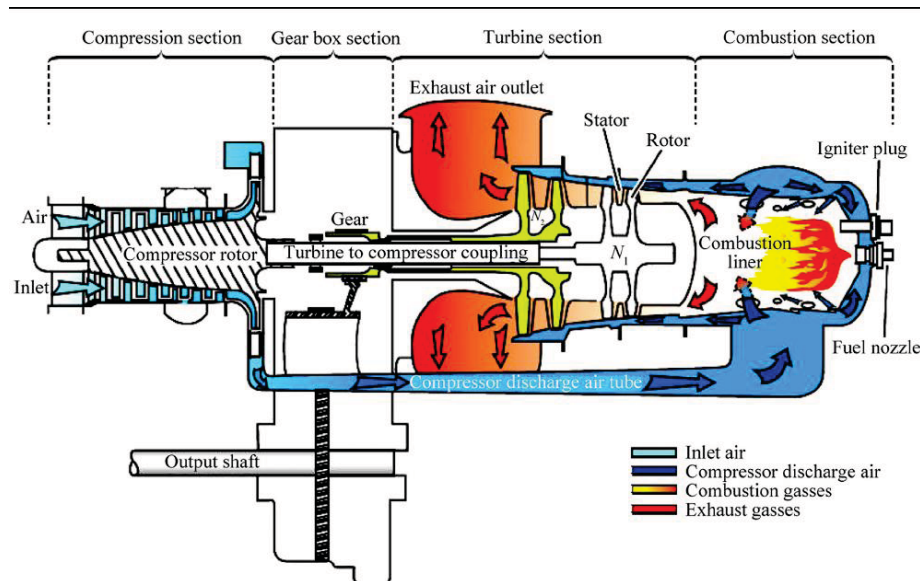


**Figure 1.8: Kamov Ka-27 "Helix"**  
(Source: US Navy)

The first true turboshaft engines developed for helicopter was built by French firm Turbomeca in 1948, with the creation of a turboshaft engine code-named



“782”. Originally developed as auxiliary power unit, it was soon adopted to aircraft propulsion, and settled down as a niche power plant for turboshaft driven helicopters back in the 1950s. However, in 1951, Charles Kaman with his K-225 synchropter modified to receive newly-developed Boeing T50 turboshaft engine became the first ever turboshaft-powered helicopter to fly ([www.faa.gov](http://www.faa.gov)).



**Figure 1.9: Turboshaft Gas Turbine Schematics**  
(Source: Nkoi et al, 2013)

Turboshaft engines (Figure 1.9) is considered an important leap in helicopter development. With high power-to-weight ratio, turboshaft engines allowing helicopter to have lighter weight while at the same time having significant higher lift capability. This also translates into the benefit of higher payload.

Because helicopters use rotating blades to generate thrust required for flight, this allows helicopter to hover and have vertical flight (including vertical take-off and landing) capability, in addition to forward and lateral flight. Due to this unique feature, it can operate at areas with limited runway or at isolated or congested areas. Therefore, despite having significantly slower speed than fixed wing aircraft, it is regarded as more versatile than fixed-wing aircrafts; and often tasked to perform missions that other types of aircraft were incapable, or for tasks which require close contact with ground such as medical transport, vertical replenishment or aerial firefighting.

For military use, the function of helicopter evolved significantly for 40 years ago. Not only restricted to troop or logistical transport like before, it evolved into a formidable combat platform and able to perform its own offensive manoeuvre or

assisting friendly forces such as anti-tank fire support or in case of shipborne helicopters; assisting in identifying hostile contacts and providing guidance for missile fired from a friendly platform to a target located beyond the horizon, a capability known as Over-The-Horizon-Targeting (OTHT).

## 1.2 Helicopter Rotor Blade

As mentioned by Leishman (2000), a helicopter rotor provides three basic functions; to generate vertical thrust for vertical flight, to generate propulsive force for forward flight, and generating forces and moments for attitude and position control of a helicopter. Unlike fixed wing aircraft where these functions are split, the helicopter rotor must provide all three within single control on the pilot.

The aerodynamics often regarded as more complex than fixed wing, largely due to wakes trailed from each blade. As for fixed wing aircraft, tip vortices will stream away from the aircraft. However, for a helicopter in forward flight, the tip vortices can remain near to the rotor and following rotor blades for several rotor revolutions. These tip vortices can cause fluctuating airloads which can cause excessive rotor vibrations and noise.

During early days of helicopter development, blade airfoil profile was not given priority because of other many technical issues to solve. Although National Advisory Committee on Aeronautics (NACA; precursor to National Aeronautics and Space Administration (NASA)) developed some airfoils dedicated for helicopter in the 1940s, it was only in the middle of 1960s that specially tailored type of airfoil sections for helicopter were widely used by manufacturers (Leishman, 2006).

With regard to rotor blade design, the selection of airfoil type is proven to be more complex than fixed wing because the angle of attack and Mach number vary continuously throughout the spanwise of rotor blade and one airfoil profile cannot satisfy the different aerodynamic requirements. In addition, the complexity of rotor control mechanism makes it difficult to embed any moving-type high lifting device (such as adjustable slot and flap) on the rotor blade as opposed to fixed wing. Given the intricacy of the system, it is obvious that any active based flow control method is impossible to be devised. This causes the design of rotor blade remain basically solid, something unchanged for the past century since the early development of helicopter.

While most airfoil designs are built around 2-D flow, the complex flow at the rotor tip requires 3-D flow consideration as well. Given this, plus severe operating conditions and typically unsteady flow environment on helicopter meaning that rotor blade must be tested in wind tunnel to fully and accurately appraise the aerodynamic performance.

### 1.3 Problem Statement

Due to complexity of the helicopter main rotor mechanism, there is little or no advancement in active flow control method and currently it is impractical to implement such approach. Therefore, passive control flow is seen more viable to be applied. While previous research has been done on the application of surface roughness as passive control flow method, those researches were focused on fixed wing applications and in two-dimensional flow conditions. Given this, there is an opportunity to explore the applications of surface roughness for rotary wing applications. Generally, main criteria for helicopter rotor blade is high thrust with low power requirement.

### 1.4 Objective

The research goals are to come up with improvised surface roughness on helicopter rotor blades, which will enhance the flight performance and power consumption. Specifically, the objectives are as follow:

- a. To perform wind tunnel experiment on helicopter main rotor blade using scaled helicopter model to study and find the aerodynamic characteristic in vertical flight condition.
- b. To evaluate the effect of surface roughness on helicopter main rotor blade and observe the thrust and power characteristics when surface roughness is applied.

### 1.5 Scope

The report will cover the result of applied surface roughness on helicopter main rotor blade. For rotary wing aerodynamics, the areas of interest are the thrust and power which correspond to lift and drag for fixed wing. This experiment will focus entirely on vertical flight condition, since it is a most complex flight regime for a helicopter. It involves constant correction input which takes toll on power provided, therefore vertical flight (particularly hover condition) is considered as high power consuming flight regime. Therefore, any improvement in vertical flight will subsequently enhance flight performance in other flight conditions.

The limitation of the research is the restricted power supply to the rotor, with maximum power supplied between 44W – 49W. This restricts rotational speed output between 600rpm – 900rpm, equal to linear speed between 20m/s – 40m/s at the rotor tip. Due to this nature, the Reynolds Number ( $Re$ ) due to flow through the rotor blade will be between  $3.7 \times 10^4$  and  $5.4 \times 10^4$ . This region is considered

as transitional flow region as mentioned by McArthur (2008). The limitation is also on blades' collective control mechanism, since the rotational speed varies with pitch level. In addition, no frontal airflow will be used in this research.

## **1.6 Thesis Layout**

The layout will be as follows: introduction is provided in Chapter 1 which includes a background in helicopter development and also issues regarding helicopter main rotor blade.

Chapter 2 will cover the literature review for this thesis, which consists of previous research work in related area, as well as theories relevant to the study.

In Chapter 3, the methodology of the study is described and the setup of the experiment will be discussed. This also covers an overview of the wind tunnel, apparatus and the model. Furthermore, the measurement techniques will also be described.

Chapter 4 will give the results and analysis from the experiment. Finally, the conclusion and recommendation will be covered in Chapter 5.



## REFERENCES

- Abuaf, N., Bunker, R. S., Lee, C. P. (1997), *Effects of Surface Roughness on Heat Transfer and Aerodynamic Performance of Turbine Airfoils*, International Gas Turbine & Aeroengine Congress & Exhibition, Orlando, Florida.
- Anderson, J. D. (2011), *Fundamentals of Aerodynamics (Fifth Edition in SI Units)*, United States McGraw-Hill.
- Bai, T. et al (2014), *Effect of Surface Roughness on the Aerodynamic Performance of Turbine Blade Cascade*, Propulsion and Power Research 2014; 3(2): 82–89.
- Bierle, M. T. (1998). *Investigation of Effects of Surface Roughness on Symmetric Airfoil Lift and Lift-To-Drag Ratio*, PhD Thesis, University of Maryland, United States.
- Boyle, R. J. (2003), *Measurements and Predictions of Surface Roughness Effects on Turbine Vane Aerodynamics*, ASME Turbo Expo 2003, Atlanta, United States.
- Bragg, M. B., Gregorek, G. M. (1987), *Experimental Study of Airfoil Performance with Vortex Generators*, Journal of Aircraft, Vol. 24, 5: 305-309.
- Bragg, M. B., Kerho, M. F. (1997), *Airfoil Boundary-Layer Development and Transition with Large Leading-Edge Roughness*, AIAA Journal, Vol. 35, 1: 75-84.
- Bramwell, A. R.S., Done, G., Balmford, D. (2001), *Bramwell's Helicopter Dynamics*, United Kingdom, Butterworth-Heinemann.
- Brocklehurst, A., Barakos, G.N. (2012), *A Review of Helicopter Rotor Blade Tip Shapes*, Progress in Aerospace Sciences (2013): 35-74.
- Brown, R. E. et al (2002), *Blade Twist Effects on Rotor Behaviour in the Vortex Ring State*, European Rotorcraft Forum, Bristol, England.
- Buchholz, T. T., Gretarsson, D., (2009), *Construction of a Four Rotor Helicopter Control System*, Technical University of Denmark, Ørsted.
- Chakroun, W., Al-Mesri, I. and Al-Fahad S. (2004), *Effect of Surface Roughness on The Aerodynamic Characteristics of a Symmetrical Airfoil*, Wind Engineering Vol. 28, No. 5.
- Conlisk, A.T. (2001), *Modern Helicopter Rotor Aerodynamics*, Progress in Aerospace Sciences 37 (2001) 419–476.
- Dhiliban, A. et al (2013), *Aerodynamic Performance of Rear Roughness Airfoils*, The Eighth Asia-Pacific Conference on Wind Engineering, Chennai, India.

- Farrokhfal, H., Pishavar, A. R. (2012), *Aerodynamic Shape Optimization of Hovering Rotor Blades Using a Coupled Free Wake–CFD and Adjoin Method*, Aerospace Science and Technology, <http://dx.doi.org/10.1016/j.ast.2012.09.004>.
- Glaz, B., (2008), *Active/Passive Optimization of Helicopter Rotor Blades for Improved Vibration, Noise, and Performance Characteristics*, PhD Thesis, University of Michigan, MI.
- Gregory, N., O'Reilly, C. L. (1973), *Low-Speed Aerodynamic Characteristics of NACA 0012 Aerofoil Section, including the Effects of Upper-Surface Roughness Simulating Hoar Frost*. Aeronautical Research Council. London: Her Majesty's Stationery Office.
- Guglieri, G. (2012), *Using of Particle Swarm for Performance Optimization of Helicopter Rotor Blades*, Applied Mathematics, 2012, 3: 1403-1408.
- Harun, Z. et al (2016), *Ordered Roughness on NACA 0026 Airfoil*, Aerotech VI - Innovation in Aerospace Engineering and Technology, Kuala Lumpur, Malaysia.
- Hicken, J. E., (2013), *Aerodynamic Design Optimization Workshop: Twist Optimization Case*, Department of Mechanical, Aerospace and Nuclear Engineering, Rensselaer Polytechnic Institute, United States.
- Hummel, F. et al (2005), *Surface Roughness Effects on Turbine Blade Aerodynamics*, Journal of Turbomachinery, Vol. 127: 453-461.
- Jansen, D. P., (2012), *Passive Flow Separation Control on an Airfoil-Flap Model (The Effect of Cylinders and Vortex Generators)*, Faculty of Aerospace Engineering, Delft University of Technology, Netherlands.
- Johnson, W. (2013), *Rotorcraft Aeromechanics*, United States, Cambridge University Press.
- Kurz, H. B. E., Kloker, M. J. (2014), *Effects of a Discrete Medium-Sized Roughness in a Laminar Swept-Wing Boundary Layer*, Notes on Numerical Fluid Mechanics and Multidisciplinary Design 124, Springer International Publishing Switzerland 2014.
- Leishman, G. (2006). *Principles of Helicopter Aerodynamics*, United States, Cambridge University Press.
- Li, J. et al (2015), *Large-Eddy Simulation for Golf Ball Aerodynamics: The Effect of Surface Roughness on The Drag Crisis and the Magnus Effect*, International Symposium on Turbulence and Shear Flow Phenomena (TSFP-9), Melbourne, Australia.

- Marzabadi, F. R., Soltani, M. R., (2012), *Effect of Leading-Edge Roughness on Boundary Layer Transition of an Oscillating Airfoil*, Scientia Iranica B (2013) 20 (3), 508–515.
- Matheis, B., D., Huebsch .W.W., Rothmayer .A.P., (2004), *Separation and Unsteady Vortex Shedding from Leading Edge Surface Roughness*, Enhancement of NATO Military Flight Vehicle Performance by Management of Interacting Boundary Layer Transition and Separation, RTO-MP-AVT-111, Prague, Czech Republic.
- Maier, T. H., Bousman, W. G., (1993), *An Examination of the Aerodynamic Moment on Rotor Blade Tips Using Flight Test Data and Analysis*, Aeroflightdynamics Directorate, U.S. Army Aviation and Troop Command, Ames Research Center, California, United States.
- McArthur, J. (2008). *Aerodynamics of Wings at Low Reynolds Numbers: Boundary Layer Separation and Reattachment*, PhD Thesis, University of Southern California, United States.
- McCroskey W.J., (1986) *Special Opportunities in Helicopter Aerodynamics*. In: Krothapalli A., Smith C.A. (eds) Recent Advances in Aerodynamics. Springer, New York, NY.
- Michael, J. E., Sharif, M. A. R., (2005), *Effect of Surface Roughness On Turbulent Transonic Flow Around A RAE-2822 Airfoil*, International Conference on Mechanical Engineering 2005, Dhaka, Bangladesh.
- Nkoi, B., Pilidis, P., and Nikolaidis, T. (2013). *Performance Assessment of Simple and Modified Cycle Turboshift Gas Turbines* [Electronic version]. Propulsion and Power Research 2013, 2(2): 96-106.
- Noonan, K. W., Yeager, W. T. and Singleton, J. D., (2001), *Wind Tunnel Evaluation of a Model Helicopter Main-Rotor Blade with Slotted Airfoils at the Tip*, National Aeronautics and Space Administration, Langley Research Center, Hampton, VA.
- Pedersen, A. H., (2006), *Test and Modelling of Four Rotor Helicopter Rotors*, Technical University of Denmark, Ørsted.
- Philips, W. F., (2003), *Minimizing Induced Drag with Geometric and Aerodynamic Twist on a Wing of Arbitrary Planform*, Department of Mechanical and Aerospace Engineering, Utah State University, United States.
- Pulla, D. P., (2006), *A Study of Helicopter Aerodynamics In Ground Effect*, The Ohio State University, United States.
- Reuss, R. L., Hoffmann M. J. and Gregorek G.M. (1995), *Effects of Surface Roughness and Vortex Generators on the NACA 4415 Airfoil*, NREL/TP-442-6472.

- Rohizan, W. N. W. et al (2016), *Effect of Surface Roughness on Helicopter Main Rotor Blade*, Aerotech VI - Innovation in Aerospace Engineering and Technology, Kuala Lumpur, Malaysia.
- Seddon, J., Newman, S., (2011), *Basic Helicopter Aerodynamics (Third Edition)*, United Kingdom, John Wiley & Sons Ltd.
- Srivastav, D. (2012), *Flow Control Over Airfoils Using Different Shaped Dimples*, International Conference on Fluid Dynamics and Thermodynamics Technologies (FDTT 2012) IPCSIT Vol. 33, IACSIT Press, Singapore.
- Standish, K. et al (2010), *Computational Prediction of Airfoil Roughness Sensitivity*, 48<sup>th</sup> AIAA Aerospace Sciences Meeting Including the New Horizons Forum and Aerospace Exhibition, Orlando, Florida.
- Straathof, M. H. et al, *Aerodynamic Shape Parameterisation and Optimisation of Novel Configurations*, Delft University of Technology, The Netherlands.
- Timmer, W. A., Schaffarczyk, A. P., (2004), *The Effect of Roughness at High Reynolds Numbers On the Performance of DU 97-W-300Mod*, Delft University Wind Energy Institute, The Netherlands.
- Vu, N. A., Jae, W. L., Jung, I. S., (2011), *Aerodynamic Design Optimization of Helicopter Rotor Blades Including Airfoil Shape for Hover Performance*, Chinese Journal of Aeronautics 2013, 26(1): 1-8.
- Walsh, J. L., LaMarsh, II, W. J., Adelman, H. M., (1993), *Fully Integrated Aerodynamic/Dynamic Optimization on Helicopter Rotor Blades*, Mathl. Comput. Modelling Vol. 18, No. 3/4: 53-72.
- Zhang, L. et al (2016), *Effects of Vortex Generators on Aerodynamic Performance of Thick Wind Turbine Airfoils*, Journal of Wind Engineering and Industrial Aerodynamics, 156(2016): 84–92.