



UNIVERSITI PUTRA MALAYSIA

***NUMERICAL AND EXPERIMENTAL STUDY OF LEADING EDGE
TUBERCLES WITH VORTEX GENERATORS ON NACA 4415 AIRFOIL***

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By

SYED MOHAMMED AMINUDDIN AFTAB

**Thesis Submitted to the School of Graduate Studies, Universiti Putra Malaysia,
in Fulfillment of the Requirement for the Degree of Doctor of Philosophy**

March 2017

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DEDICATION

This thesis is dedicated to my parents and inspiring teachers,

(Mr. S. M. M. Peerzada and Mrs. S. F. N. Sultana)



Abstract of thesis presented to the Senate of Universiti Putra Malaysia in fulfillment of the requirement for the Degree of Doctor of Philosophy

NUMERICAL AND EXPERIMENTAL STUDY OF LEADING EDGE TUBERCLES WITH VORTEX GENERATORS ON NACA 4415 AIRFOIL

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March 2017

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Low Reynolds number flows are associated with the problems of separation bubble. The presence of separation bubble reduces the performance of the airfoil. The most commonly used devices in order to increase the performance in these Reynolds number range are Vortex Generators (VG). Recently studies have shown that implementing humpback whale Tubercle Leading Edge (TLE), also enhance the performance of the airfoil. The objective of the current work is to combine TLE and VG thereby elimination of separation bubble and increase airfoil lift to drag ratio. Initially the flow over NACA 4415 at low Reynolds number (Re) of 120,000 using Computational Fluid Dynamics (CFD) is carried out, and proper methodology for selection of turbulence model for low Re flows is also reported. Five turbulence models, were tested and it was found that $\gamma-Re_\theta$ sst was the best suitable Reynolds Averaged Navier Stokes (RANS) model to capture the flow physics. The main mesh requirements for utilizing $\gamma-Re_\theta$ sst is to maintain the wall $y^+ < 1$. Throughout the thesis, structured meshing has been carried out using ICEM CFD. The established turbulence model was used to conduct CFD analysis on two Tubercle Leading Edge (TLE) designs. The designs tested are, 1. Spherical 2. Sinusoidal, the geometry is modeled using CATIA V5R21. A parametric study varying the amplitude of the tubercles is also carried out. The wavelength was kept constant at $0.25c$ three amplitude variations $0.025c$, $0.05c$ and $0.075c$, were modeled for both spherical and sinusoidal tubercles designs. The flow Re was set to 120,000. As the tip effects were neglected, the results are for $2.5D$, only the effect of span is taken into consideration. A 3D hex grid was generated around the rectangular domain with a span of $0.5c$. The results showed that spherical tubercle with $0.025c$ amplitude was efficient at 18° AoA, it increased the l/d ratio by 6.25%. Based on these CFD results, a modified NACA 4415 airfoil with spherical TLE was fabricated. Wind tunnel testing was carried out at Re 200,000. The results were compared with previous experimental work on NACA 4415 with straight leading edge. The results of spherical TLE showed an improvement in lift to drag ratio by 67.3% at 0° , 14% at 6° , 17.6% at 12° and the performance decrement at 18° by 3.23%. This proves that spherical TLE do improve the

performance but Re number effect is an important aspect which needs to be studied. Finally a CFD analysis combining spherical TLE and VG is studied. This is the novelty of the current research is the combination of TLE and VG. The results showed that the combination enhanced the performance of clean airfoil by 8.9%. TLE and VG combination improved performance by 50% at 12° AoA as compared to merely TLE airfoil. The breakthrough finding was the working mechanism of spherical TLE which appeared similar to sub boundary layer VG. Thus the combination of TLE and VG gives a major boost in enhancing the performance of airfoil working in low Re range.



Abstrak tesis yang dikemukakan kepada Senat Universiti Putra Malaysia sebagai memenuhi keperluan untuk Ijazah Doktor Falsafah

KAJIAN BERANGKA DAN EKSPERIMEN TUBERKEL PINGGIR DEPAN DENGAN PENGHASIL PUSARAN KE ATAS AEROFIL NACA 4415

Oleh

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Aliran pada nombor Reynolds rendah sering dikaitkan dengan masalah gelembung pemisah. Kehadiran gelembung pemisah mengurangkan prestasi aerofil. Peranti yang sering digunakan untuk meningkatkan prestasi pada julat nombor Reynolds ini ialah penghasil pusaran (VG). Kajian terkini menunjukkan penggunaan tuberkel pinggir depan (TLE) juga dapat meningkatkan kecekapan aerofil. Objektif kajian ini adalah untuk menggabungkan TLE dan VG seterusnya menghapuskan gelembung pemisah dan meningkatkan nisbah angkat kepada seretan aerofil. Pada mulanya, aliran ke atas aerofil NACA 4415 pada nombor Reynolds (Re) 120,000 menggunakan Pengkomputeran Dinamik Bendalir (CFD) dijalankan, dan pemilihan model gelora dilaporkan. Lima model gelora, di uji dan didapati $\gamma-Re_\theta$ SST adalah model Reynolds Purata Navier Stokes (RANS) yang terbaik untuk mengukur aliran fizik. Keperluan utama jejaring untuk menggunakan $\gamma-Re_\theta$ SST adalah dengan mengekalkan nilai dinding $y^+ < 1$. Dalam kajian ini, jejaring berstruktur telah dihasilkan menggunakan ICEM CFD. Model gelora yang ditubuhkan telah digunakan untuk menjalankan analisis CFD pada dua reka bentuk TLE. Reka bentuk yang diuji adalah, 1. Sfera 2. Sinus, geometri dimodelkan menggunakan CATIA V5R21. Satu kajian parametrik dijalankan dengan mengubah amplitud tuberkel. Panjang gelombang ditetapkan pada 0.25c. Tiga variasi amplitud 0.025c, 0.05c dan 0.075c, dimodelkan untuk reka bentuk tuberkel kedua-dua sfera dan sinus. Nombor Re bagi aliran ditetapkan pada 120,000. Disebabkan kesan hujung diabaikan, keputusan adalah untuk 2.5D, hanya kesan rentang diambil kira. Grid segi enam 3D telah dihasilkan sekitar domain segi empat tepat dengan rentang 0.5c. Hasil kajian menunjukkan bahawa tuberkel sfera dengan 0.025c amplitud menghasilkan kecekapan pada 18° AoA, telah meningkatkan nisbah L / D sebanyak 6.25%. Berdasarkan kepada keputusan CFD ini, aerofil NACA4415 yang diubahsuai dengan bentuk sfera TLE telah difabrikasi. Ujian terowong angin telah dijalankan pada Re 200,000. Keputusan ini dibandingkan dengan kerja eksperimen sebelum ini pada NACA 4415 dengan pinggir depan lurus. Keputusan bentuk sfera TLE menunjukkan peningkatan dalam nisbah lif kepada seret sebanyak 67.3% pada 0° , 14% pada 6° , 17.6% pada 12° dan susutan kecekapan pada 18°

sabanyak 3.23%. Ini membuktikan bahawa sfera TLE menghasilkan kecekapan prestasi tetapi kesan nombor Re merupakan aspek penting yang perlu dikaji. Akhirnya analisis CFD yang menggabungkan sfera TLE dan penghasil pusaran (VG) dikaji. Ini adalah sesuatu yang baru bagi penyelidikan semasa, setakat ini gabungan TLE dan VG masih belum pernah dilaporkan. Hasil kajian menunjukkan bahawa kombinasi ini meningkatkan prestasi aerofil bersih sebanyak 8.9%. Gabungan TLE dan VG meningkatkan prestasi sebanyak 50% pada 12° AoA berbanding dengan aerofil TLE. Penemuan utama adalah terhadap mekanisme kerja sfera TLE yang sama dengan sub VG lapisan sempadan. Oleh itu gabungan TLE dan VG memberikan rangsangan utama dalam meningkatkan prestasi aerofil pada Re rendah.



This thesis submitted to the Senate of Universiti Putra Malaysia has been accepted as fulfillment of the requirement for the degree of Doctor of Philosophy. The members of the Supervisory Committee were as follows:

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LIST OF ABBREVIATIONS

AGI	Airfoil Gust Interaction
AoA	AoA
BL	Boundary Layer
CAA	Computational Aero Acoustic
CFD	Computational Fluid Dynamics
CNC	Computer Numerical Controlled
CTRM	Composite Technology Research Malaysia
DAQ	Data Acquisition
DARC	Data Acquisition Reduction and Control
DDES	Delayed Detached Eddy Simulation
DDLE	Dynamically Deformed Leading Edge
DES	Direct Eddy Simulation
DSM	Dynamic Smagorinsky Model
Gmi	German Malaysian Institute
HAWT	Horizontal Axis Wind Tunnel
HPC	High Performance Computing
IBM	Immersed Boundary Method
ISVR	Institute of Sound and Vibration Research
LDV	Laser Doppler Velocimetry
LES	Large Eddy Simulation
LEV	Leading Edge Vortex
MAV	Micro Air Vehicle
MOGA	Multi Objective Generic Algorithm
NACA	National Advisory Committee for Aeronautics
NASA	National Aeronautics and Space Administration
Open FOAM	Open source Field Operation And Manipulation
PIV	Particle Image Velocimetry
PNLLT	Prandtl's Nonlinear Lifting Line Theory
RANS	Reynolds Averaged Navier Stokes
SA	Spalart Allmaras
SBVG	Sub Boundary Layer Vortex Generator
SIMPLE	Semi-Implicit Method for Pressure-Linked Equations
SLE	Straight Leading Edge
SMA	Shape Memory Alloys
SPIV	Stereo Particle Image Velocimetry

SST	Shear Stress Transport
SWFS	Solid Works Flow Simulation
TLE	Tubercle Leading Edge
T-S	Tollmien-Schlichting
UAV	Unmanned Aerial Vehicle
VAWT	Vertical Axis Wind Tunnel
VG	Vortex Generators



LIST OF SYMBOLS

2D	Two Dimensional	
3D	Three Dimensional	
A	Amplitude	m
c	Chord	m
C_d	Coefficient of Drag	
C_l	coefficient of Lift	
C_m	Coefficient of Moment	
C_p	Coefficient of Pressure	
d	Distance between VG	m
e	Thickness of the VG	m
G	Generation Term	N/m ³
h	Height of the VG	m
K	Turbulent Kinetic Energy	m ² /s ²
KL	Laminar Kinetic Energy	
L	Length of the VG	m
L/D	Lift to drag ratio	
Re	Reynolds Number	
Re_θ	Transition Reynolds Number	
S	Span	m
S	Source Term	N/m ³
x	Length of the airfoil	m
β	VG orientation angle	deg
γ	Intermittency	
δ	Boundary layer thickness	m
ε	Turbulence Dissipation Rate	m ² /s ³
λ/W	Wavelength	m
ω	Specific Dissipation Rate	1/s

CHAPTER 1

INTRODUCTION

The dream of flying has baffled humanity since earliest times. Greek mythology depicts the flight of Icarus, with wings made of wax, flying towards the sun. The Ancient Egyptian god Khensu had wings and was known as a traveler journeying through the skies. These stories have been a dream for man, inspiring him to achieve the goal of flying. Only at the beginning of the 20th century, this dream was possible. The first human photographed in airplane is Otto Lilienthal, with over 2000 successful glider flights and was the inspiration to the efforts of powered flight by Wright brothers Anderson, (2005). The current goal of the aerospace industry is to develop greener technologies. This can be achieved only by reducing the structural weight, using a highly efficient propulsion system, increasing the aerodynamic efficiency and decreasing the overall drag.

1.1 Flow control

The major areas where flow control is necessary are wings, rudders, fans and turbines. Flow on aerodynamic surfaces has to be attached at a high Angle of Attack (AoA), as this increases operational capability, efficiency, range and endurance Green, (2008). Aerodynamic flow control is classified into active, passive and hybrid. The active flow control technique is one where actuators and other mechanisms are used. Passive flow control mainly employs devices or modification without involving actuators and complex mechanisms. In hybrid control, both active and passive mechanisms are implemented. The main aim of these devices is to control separation. Figure 1.1 shows the interrelation of separation to lift, drag, transition and reattachment. A detailed description of the various flow separation control methods, both active and passive, has been elaborately covered by Gad-el-Hak, (2007).

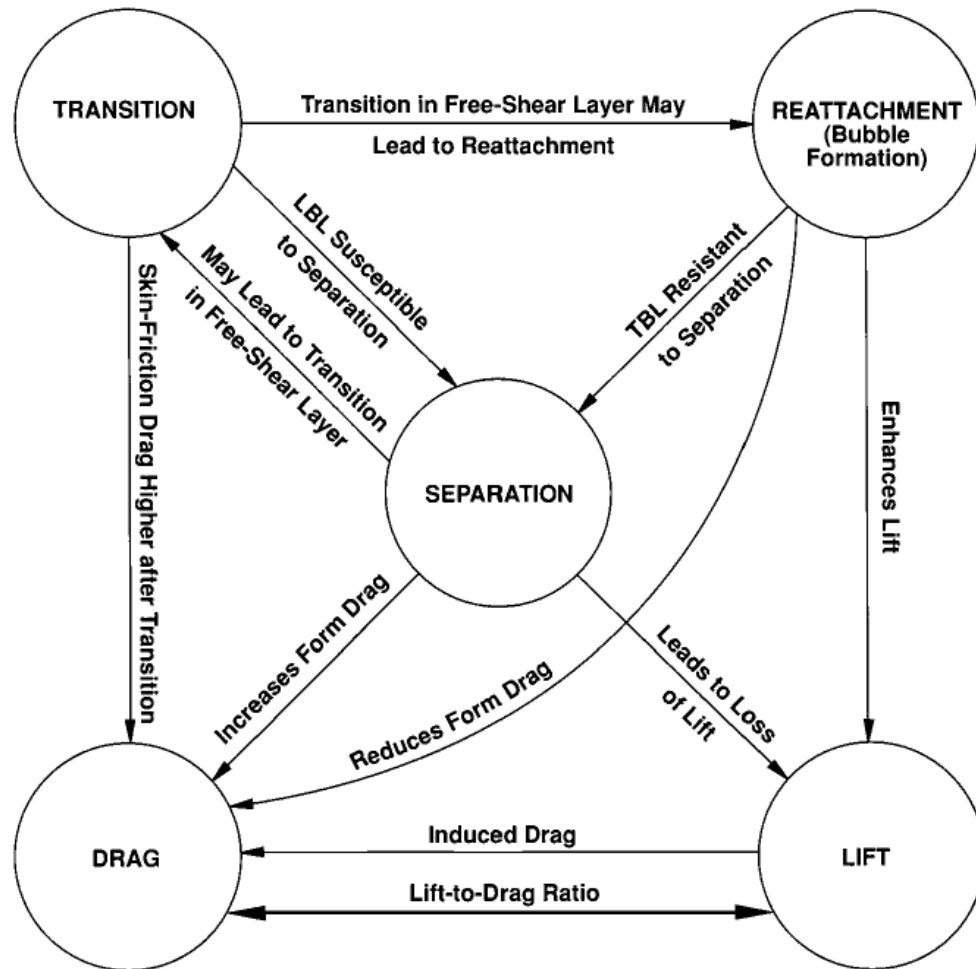


Figure 1.1: Effects of separation Gad-el-Hak, (2007)

1.2 Biomimetics

The study of the structures and functions of biological systems in the design of engineering systems is known as biomimetics. In general, this means imitating nature to solve engineering problems. A detailed review and the in-depth technological applications of various biological systems in relation to engineering has been compiled by Yoseph Bar- Cohen, (2005). Some of the most fascinating bio-mimicking studies, from the aerodynamic perspective, include the flight of owls and seagulls (Collins, 1981; Cranston et al., 2012; Hua et al., 2010; Ito, 2009; Klan et al., 2010; Lilley, 1998). Owls have the ability to approach their prey in total silence, and the flapping sound is damped by leading edge serrations, giving them the ability to control the flow (Collins, 1981; Klan et al., 2010; Lilley, 1998).

Aerodynamic engineers draw inspiration from marine animals. Designing an aircraft skin similar to that of sailfish and swordfish, or implementing riblets inspired by sharks, has been beneficial in overcoming the skin friction drag on aircraft. Bhushan, (2009) summarises various inspirations drawn from nature and their applications as shown in Figure 1.2.

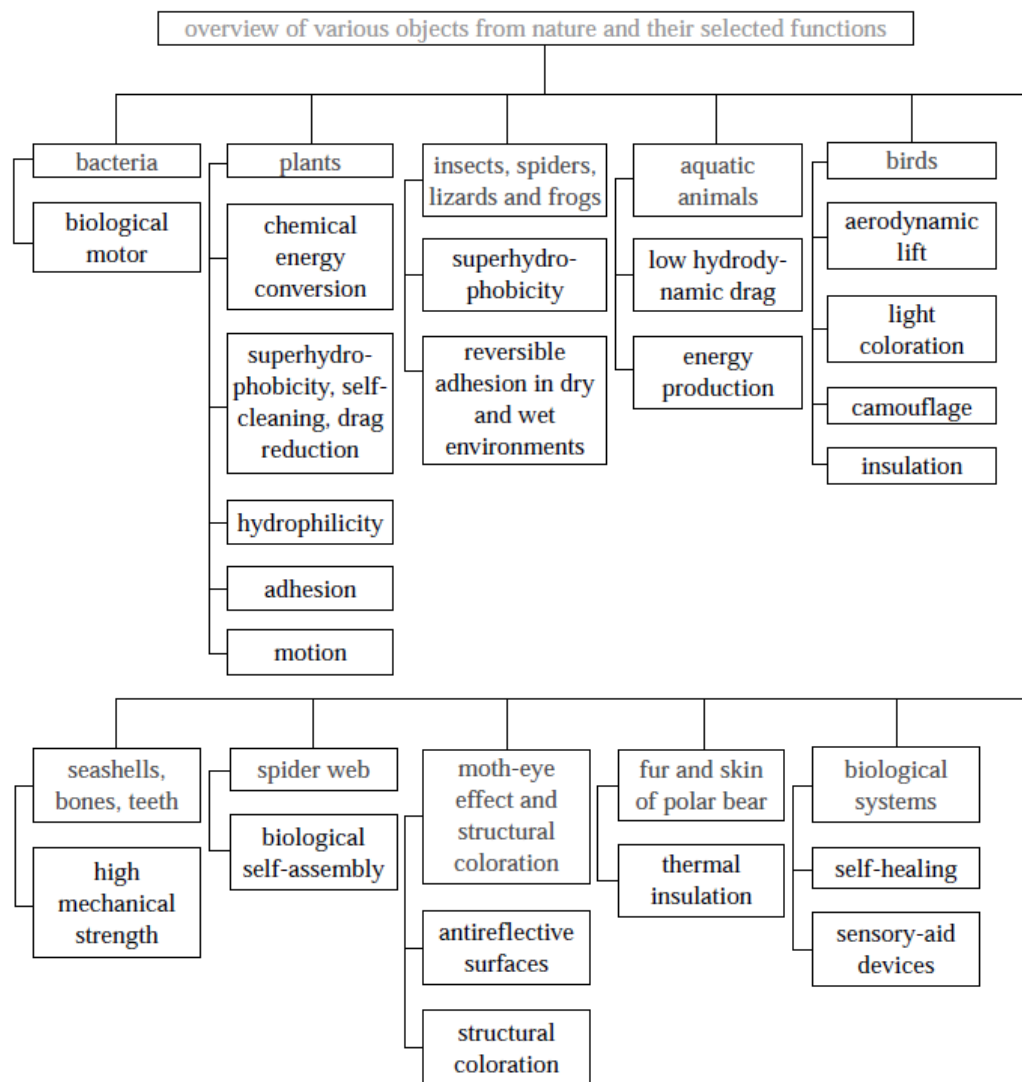


Figure 1.2: The various inspirations and applications of biomimetics Bhushan, (2009)

The successful integration of biomimetics into mechanical systems has been a challenge. Recent technological advancements in the field of material science and engineering have made the dream of mimicking nature a reality (Choi, 2009; Fish, 2008; Fish, 2006). Due to its huge importance, research in the field of biomimetics is gaining popularity.

1.3 Humpback Whale

The humpback whale (*Megaptera Novaeangliea*) is a species of baleen whale of the Balaenopteridae family. This mammal has existed for the past 55 million years and comes under the order of cetaceans, which includes dolphins, whales and porpoises Fish et al., (2011a). This whale has a huge size, measuring approximately 15.6 meters in length and weighing around 34 tons Johnson and Wolman, (1984). Humpback whales feed on plankton, and fish schools of euphausiids, herring, and capelin Fish et

al., (2008). The most amazing feature of the humpback is its acrobatic behaviour during feeding known as bubble netting, which involves creating a zone around the prey and then sudden lunging towards it, giving the whale an element of surprise Johnson and Wolman, (1984), Winn and Winn, (1985). Due to the presence of the tubercles on the flippers, the whale has a minimum turning diameter of 14.8m Figure 1.3 Summers and Wynne, (2004), Fish, (1999).

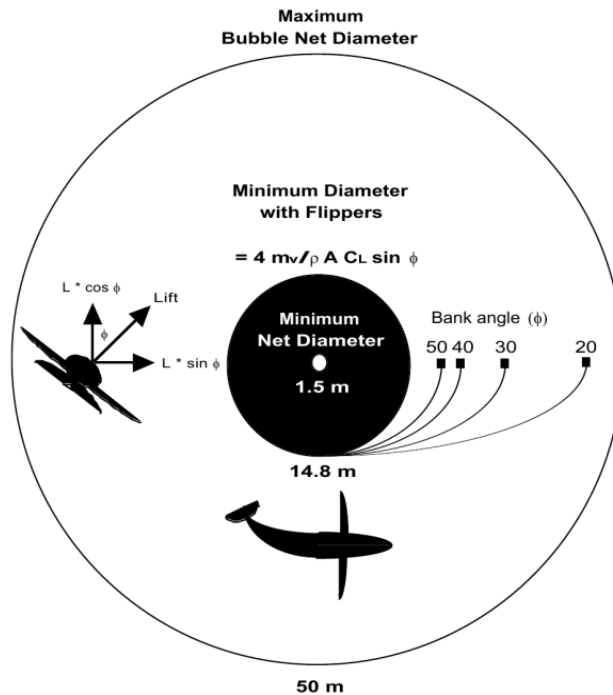


Figure 1.3: Bubble net formation and the turning radius of the humpback Fish, (1999)

Humpbacks can also perform acrobatic manoeuvres and underwater somersaults, (Summers and Wynne, (2004), Johari, et al., (2007). The flippers measure more than 9 meters in length, are elliptical in shape and have a high aspect ratio. The wavy leading edge consists typically of 10 or 11 rounded tubercles Figure 1.4 (Fish and Lauder, 2006; Fish et al., 2008; Fish, 1994; Van Nierop et al., 2008).

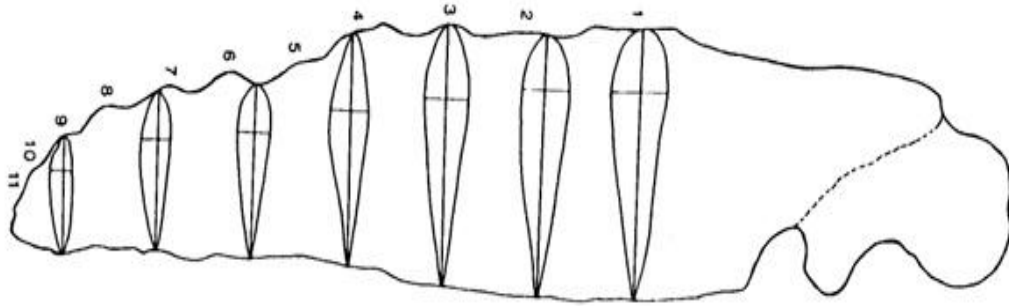


Figure 1.4: Humpback whale flipper with Tubercle locations profile Fish and Battle, (1995)

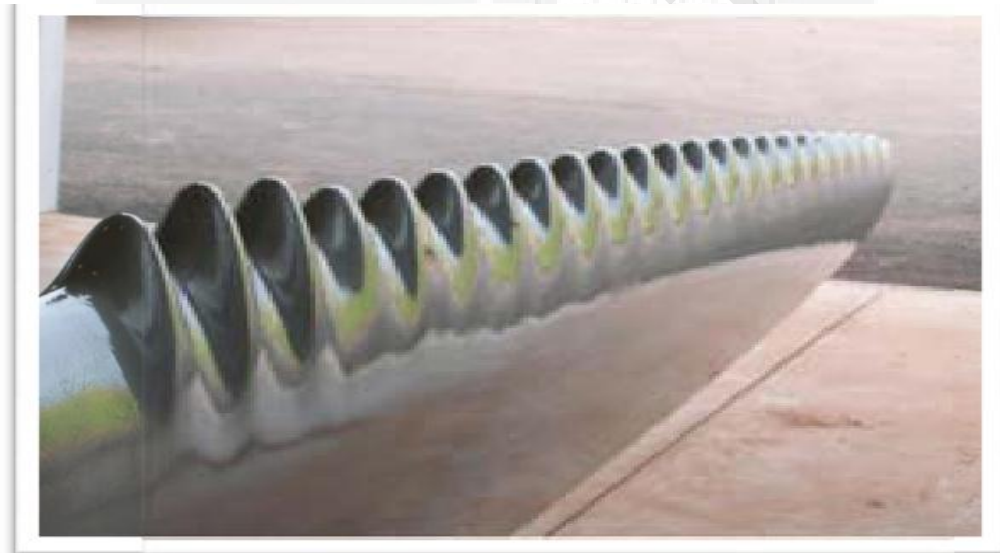


Figure 1.5: Blade developed by Whale Power Corp Wind Energy Institute of Canada, (2008)

Dr. Frank Fish (a marine biologist) who noticed bumps on the flipper, started the initial research, subsequently publishing numerous research articles on the topic (Fish et al., 2008; Fish and Lauder, 2006, Fish and Lauder, 2013; Fish et al., 2011a; Fish et al., 2011b; Fish, 1999; Fish, 2006; Fish, 1994; Fish and Battle, 1995; Watts and Fish, 2001; Watts and Fish, 2002). Watts and Fish patented this technology and started a company named 'Whale Power', which develops wind turbine blades. Figure 1.5 shows the blades incorporated with the tubercle design. The new design has 25% more airflow than conventional wind turbine blades and it produces 20% more energy Watts and Fish, (2002), Wind Energy Institute of Canada, (2008), Yurchenko, (2011).

Fish and Battle, (1995) studied flipper morphology in detail after obtaining a dead humpback whale. The flipper is elliptical and tapered, with a 19° swept angle w.r.t longitudinal axis. Tubercle location is as shown in Figure 1.4 the whale fin obtained consisted of 11 tubercles. The location of first tubercle is at 33% span and 11th tubercle at 99.1% Figure 1.4. The flipper profile has a cross-section that is constant, irrespective of the span-wise position, while the chord reduces moving outward. The profile is similar to NACA 634-021 airfoil. An analogy between leading edge strakes and tubercles working was drawn Fish and Battle, (1995).

1.4 Low Reynolds Number

Low Reynolds number flows pose a great challenge in the selection of a Turbulence model for simulation. Many of the UAV's and MAV's work in these Reynolds number ranges. Colossal interest is growing in the CFD study of static wing and flapping wing aerodynamics on flow in this regime Gad-el-Hak, (2007).

In the case of low Re airfoils, the resistance to separation of the boundary layer is very poor, thus resulting in a dominant adverse pressure gradient. As flow separates from the point of minimum pressure, due to the increase in adverse pressure at the leading edge, separation takes place. The separated flow is highly unstable, resulting in transition immediately downstream, causing the flow to become turbulent. Thereby turbulent shear stresses energize the flow to counteract the increased adverse pressure, helping the flow to reattach. Thus, a zone in between separation and reattachment is formed, known as the separation bubble (Mueller and Batil, 1982 and Carmichael, 1981). The separation bubble is dependent on the flow Re, the pressure distribution, the curvature of the airfoil, roughness and various other factors Gad-el-Hak, (2007). Two types of separation bubble exist, namely the short bubble and the long bubble Figure 1.6. A short bubble exists when the flow Re is below 10^5 and only extends to a couple of percent along the chord. The stability of this bubble is only for a short duration. Carmichael, (1981) has stated that below $Re\ 5 \times 10^4$, a short laminar separation bubble causes a drastic drop in lift. If the Reynolds number exceeds 10^5 , a long bubble is formed. This bubble extends to 20-30% along the chord and affects the flow drastically Lissaman, (1983).

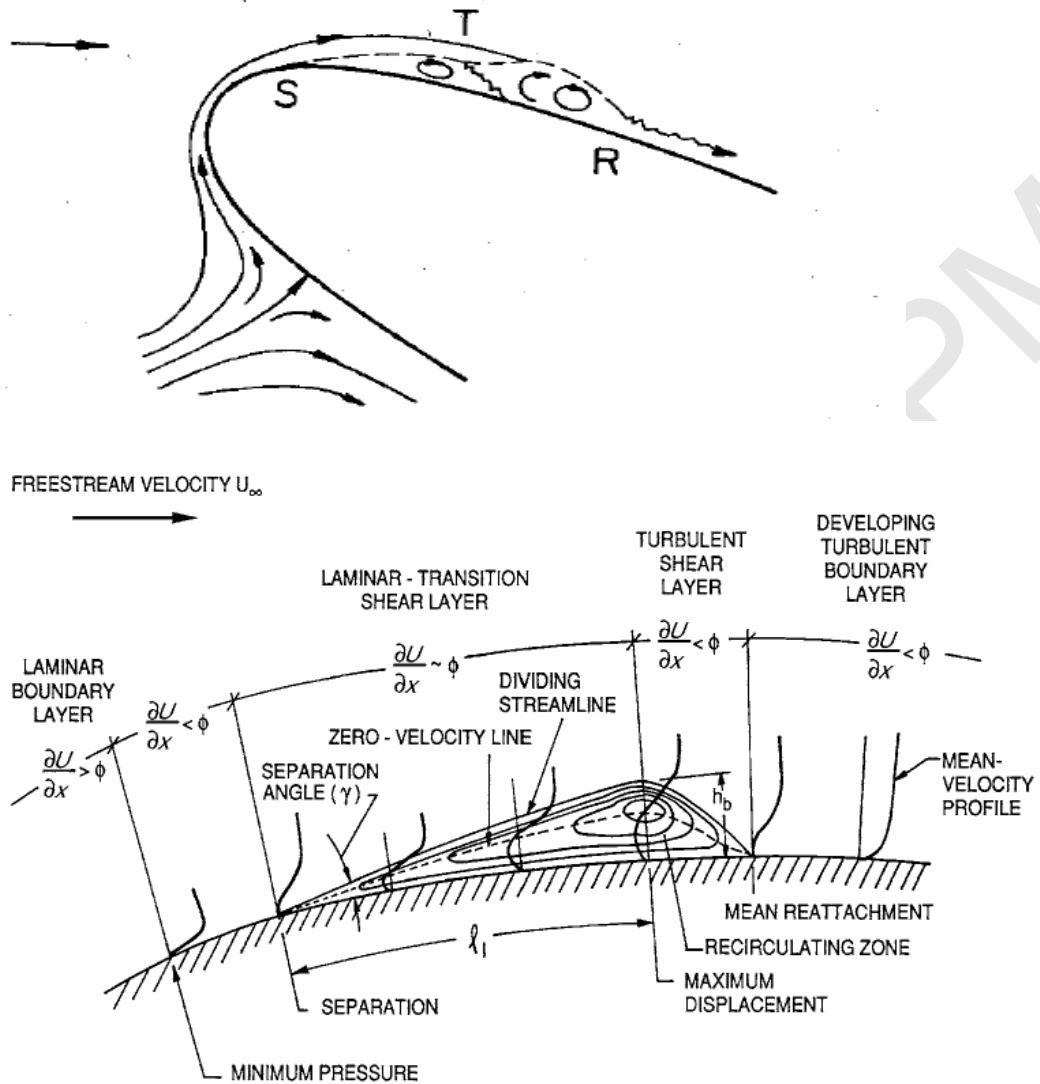


Figure 1.6: Flow separation bubble (Mueller and Batil, 1982; Carmichael, 1981)

For airfoils operating in the Re range of 10^6 , the adverse pressure gradient is eliminated by turbulent flow at transition thus preventing separation. An increase in Re induces turbulence in the boundary layer, imparting high energy to oppose separation.

1.5 Vortex Generators

Vortex generator (VG) is most commonly used flow control devices for, low Re flows and to control the formation of separation bubble. A detailed review on types of VG, working mechanism and application is reported by Lin, (2002)

Previous work by Zhen et al., (2011) showed that implementation of VG increased the airfoil performance. Serakawi and Ahmad, (2012) did PIV experimental work and

concluded that VG effectively reduce the separation in diffuser. Ahmad et al., (2008) showed the effect of oscillating Sub Boundary Layer Vortex Generator (SBVG) in reducing the separation, Halim and Ahmad, (2013) did simulation to find optimized configuration in order to reduce separation. Aftab and Murthy, (2012) showed that standard VG reduced separation on Onera M6 wing.

1.6 Problem Statement and Hypothesis

Wind turbine blades, trainer aircraft and UAV's operate at low Reynolds number. Thick airfoils are mainly used in these applications, due to its benefit at low speed in generating high lift. Airfoils operating at low speed fall under low Reynolds number range, 100,000 to 500,000 and are prone to the formation of laminar separation bubble. The separation bubble increases drag and reduces the performance of the airfoil. In order to prevent the formation of separation bubble passive and active flow control devices are used. Previous research has shown that installing passive flow control devices such as, VG on the airfoil drastically improves the performance. Recent discovery of tubercle technology has effectively, helped in performance improvement by hindering the formation of separation bubble. Turbulence models used in CFD studies of low Reynolds number flow experience uncertainties, which need to be properly captured. New turbulence models have been developed and are available to address this issue. In the current research the CFD simulations are carried out, on a NACA 4415 airfoil at low Reynolds number of 120,000. The newly developed RANS transition turbulence models are utilised. To check the accuracy and capability of the transition turbulence model to obtain a CFD solution is very essential, to understand the flow characteristics of NACA 4415 airfoil at low Reynolds number. The issue in regard with the effect of tubercles at the leading edge of NACA 4415 needs to be investigated. The author of the current research hypothesizes that favourable performance benefits will results, from the combination two passive flow control devices, tubercles and vortex generators on NACA 4415 airfoil in low Reynolds number range. The author intends to address the gap in knowledge, as well as bring forward a new dimension to low Reynolds number flow control research.

1.7 Aims and Objectives

Tubercles are currently being used to address the problem of separation bubble. Previously, VG's have been used to provide enhancement in airfoil performance. The main aim of the current work is to combine vortex generators with tubercle design, and study the effect on performance of the airfoil for low Reynolds number flows.

To achieve the above aim three objectives have to be achieved as described below

- To investigate and validate an optimal CFD turbulence modeling technique, suitable for low Reynolds number flows.
- To conduct a parametric study to determine the optimal shape for the tubercle and to determine the optimal amplitude and wavelength suitable for the tubercle.

- Implement Vortex Generators (VG) and the optimized tubercle design on the airfoil and determine the effect on performance.

1.8 Scope of work

This research work was carried out in collaboration with CTRM Sdn Bhd, Malaysia. The Aludra MK-I UAV is designed and built by CTRM and is operated by Royal Malaysian Air Force. The airfoil design in the current study is similar to the one on Aludra Mk-I UAV. Based on the TLE airfoil performance benefits, a new wing model will be designed and tested on the Aludra Mk-I UAV. The CFD parametric study on TLE shape and analysis will give a deeper insight into flow behaviour. No extensive research has been reported considering the TLE shape. The fabricated TLE airfoil on which the experimental work is reported in this thesis is first of a kind study. The combination of TLE and VG will result in a deeper understanding of combining two flow control devices.

1.9 Thesis Organization

Chapter 1 introduces to the background of biomimetics, flow control, low Reynolds number, and Vortex Generators (VG). It also highlights the motivation for the study, outlining the scope and objectives of the research.

Chapter 2 summarises the literature available on humpback whale flipper. A detailed in-depth review has been carried out and discussed in this chapter. The chapter deals with studies incorporation tubercle design on various airfoils. The contents of the chapter have been published as a review article in Journal Progress in Aerospace Sciences.

Chapter 3 deals with the numerical and experimental methodology used for conducting the validation study. It also includes the numerical methodology followed in order to carry out the parametric study of Sinusoidal and Spherical shaped tubercles, varying the amplitude and wavelength of the tubercles designs. The fabrication and Wind tunnel calibration methodology employed in open loop wind tunnel test facility at Universiti Putra Malaysia (UPM) has been described in detail in this chapter.

Chapter 4 reports the numerical, results. The validation and verification of the numerical results is reported. The results of the parametric study are also discussed.

Chapter 5 describes the experimental results, performance comparison of airfoil with spherical tubercle and airfoil with VG is reported.

Chapter 6 discusses the benefits of combining two flow control techniques. The results of this unique combination are discussed in detail.

Chapter 7 summarises the overall work along with conclusions and recommendations for future research.

REFERENCES

- Aftab, S. M. A. and Murthy, P. S. (2012). Comparative Study of Vortex Generator Orientation on Wing Surface Considering Delta Vortex Generators. *Applied Mechanics and Materials*, 225, 79–84.
- Ahmad, K., Abdullah, M. and Watterson, J. (2008). CFD Simulations of Oscillating Sub-Boundary Layer Vortex Generators for Diffuser Flow Separation Control. *International Journal of Engineering and Technology*, 5(1), 25–35.
- Anderson, J. D. (2005). *Introduction to Flight* (Vol. 199). McGraw-Hill Boston.
- Arai, H., Yasuaki, D., Takuji, N. and Hidemi, M. (2011). Numerical Simulation around Rectangular Wings with Wavy Leading Edge. *Journal of the Japan Society of Naval Architects and Ocean Engineers*, 12, 33–41.
- Asghar, A., Allan, W., LaViolette, M. and Woodason, R. (2014). Influence of a novel 3D leading edge geometry on the aerodynamic performance of low pressure turbine blade cascade vanes. In *ASME Turbo Expo 2014: Turbine Technical Conference and Exposition*, 2c (25899), 1-13.
- Bai, C. J., Lin, Y. Y., Lin, S. Y. and Wang, W. C. (2015). Computational fluid dynamics analysis of the vertical axis wind turbine blade with tubercle leading edge. *Journal of Renewable and Sustainable Energy*, 7(3), 33124–33139.
- Bar-Cohen, Y. (2005). *Biomimetics: Biologically Inspired Technologies*. CRC Press.
- Bhushan, B. (2009). Biomimetics: lessons from nature-an overview. *Philosophical Transactions of the Royal Society A: Mathematical, Physical and Engineering Sciences*, 367(1893), 1445–1486.
- Bolzon, M. D., Kelso, R. M. and Arjomandi, M. (2015). Tubercles and their applications. *Journal of Aerospace Engineering*, 29(1), 04015013.
- Borg, J. (2012). The effect of leading edge serrations on dynamic stall. *Master's Thesis, University of Southampton*.
- Bushnell, D. M. and Moore, K. (1991). Drag reduction in nature. *Annual Review of Fluid Mechanics*, 23(1), 65–79.
- Butler, R. J., Byerley, A. R., VanTreuren, K. and Baughn, J. W. (2001). The effect of turbulence intensity and length scale on low-pressure turbine blade aerodynamics. *International Journal of Heat and Fluid Flow*, 22(2), 123–133.
- Cai, C., Zuo, Z., Liu, S., Wu, Y. and Wang, F. (2013). Numerical evaluations of the effect of leading-edge protuberances on the static and dynamic stall characteristics of an airfoil. In *6 th IOP Conference Series: Materials Science and Engineering*, 52(1), 1-7.

- Câmara, J. and Sousa, J. (2013). Numerical Study on the Use of a Sinusoidal Leading Edge for Passive Stall Control at Low Reynolds Number. *51st AIAA Aerospace Sciences Meeting* (0062), 1-7.
- Cao, N. (2010). Effects of turbulence intensity and integral length scale on an asymmetric airfoil at low Reynolds numbers.
- Carmichael, B. (1981). Low Reynolds number airfoil survey. National Aeronautics and Space Administration, Langley Research Center (CR-165803).
- Chaitanya, P., Narayanan, S., Joseph, P., Vanderwel, C., Turner, J., Kim, J. and Ganapathisubramani, B. (2015). Broadband noise reduction through leading edge serrations on realistic aerofoils, *21st AIAA/CEAS Aeroacoustics Conference, AIAA*, (2202), 1-29
- Chandrasekhara, M., Wilder, M. and Carr, L. (1997). Control of flow separation using adaptive airfoils. *35th Aerospace Sciences Meeting and Exhibit, AIAA*, (0655), 1-12.
- Chandrasekhara, M., Wilder, M. and Carr, L. (1998). Unsteady stall control using dynamically deforming airfoils. *AIAA Journal*, 36(10), 1792-1800.
- Chen, H., Pan, C. and Wang, J. (2013). Effects of sinusoidal leading edge on delta wing performance and mechanism. *Science China Technological Sciences*, 56(3), 772-779.
- Chen, H. and Wang, J.-J. (2014). Vortex structures for flow over a delta wing with sinusoidal leading edge. *Experiments in Fluids*, 55(6), 1-9.
- Chen, J., Li, S. and Nguyen, V. (2012). The Effect of Leading Edge Protuberances On The Performance Of Small Aspect Ratio Foils. *15th International Symposium on Flow Visualization*, 1-6.
- Chen, W., Qiao, W., Wang, L., Tong, F. and Wang, X. (2015). Rod-Airfoil Interaction Noise Reduction Using Leading Edge Serrations. In *21st AIAA/CEAS Aeroacoustics Conference* (3264) 1-24.
- Choi, H. (2009). Bio-mimetic flow control. *Bulletin of the American Physical Society*, 54.
- Choi, H., Park, H., Sagong, W. (2012). Biomimetic flow control based on morphological features of living creatures. *Physics of Fluids*, 24(12), 121302.
- Chong, T. P., Vathylakis, A., McEwen, A., Kemsley, F., Muhammad, C. and Siddiqi, S. (2015). Aeroacoustic and aerodynamic performances of an aerofoil subjected to sinusoidal leading edges. *21st AIAA/CEAS Aeroacoustics Conference*, (2200), 1-19.

- Choudhry, A., Arjomandi, M. and Kelso, R. (2015). A study of long separation bubble on thick airfoils and its consequent effects. *International Journal of Heat and Fluid Flow*, 52, 84–96.
- Choudhry, A., Leknys, R., Arjomandi, M. and Kelso, R. (2014). An Insight into the dynamic stall lift characteristics. *Experimental Thermal and Fluid Science*. 58, 188-208.
- Clair, V., Polacsek, C., Le Garrec, T., Reboul, G., Gruber, M. and Joseph, P. (2013). Experimental and numerical investigation of turbulence-airfoil noise reduction using Wavy edges. *AIAA Journal*, 51(11), 2695–2713.
- Collins, F. G. (1981). Boundary-layer control on wings using sound and leading-edge serrations. *AIAA Journal*, 19(2), 129–130.
- Corsini, A., Delibra, G. and Sheard, A. G. (2013a). The application of sinusoidal blade-leading edges in a fan-design methodology to improve stall resistance. *Proceedings of the Institution of Mechanical Engineers, Part A: Journal of Power and Energy*, 1-18.
- Corsini, A., Delibra, G. and Sheard, A. G. (2013b). On the Role of Leading-Edge Bumps in the Control of Stall Onset in Axial Fan Blades. *Journal of Fluids Engineering*, 135(8), 081104-081104.
- Cranston, B., Laux, C. and Altman, A. (2012). Leading edge serrations on flat plates at low reynolds number. In *50th AIAA Aerospace Sciences Meeting Including the New Horizons Forum and Aerospace Exposition*. (0053), 1-14.
- Custodio, D., Henoch, C. and Johari, H. (2012). Aerodynamic characteristics of finite-span wings with leading edge protuberances. *50th AIAA Aerospace Sciences Meeting Including the New Horizons Forum and Aerospace Exposition*, (0054), 12.
- Custodio, D., Henoch, C. and Johari, H. (2015). Aerodynamic characteristics of Finite Span Wings with Leading-Edge Protuberances. *AIAA Journal*, 53(7), 1–16.
- Delgado, H., Esmaili, A. and Sousa, J. (2014). Stereo PIV measurements of low-aspect-ratio low-reynolds-number wings with sinusoidal leading edges for improved computational modeling. *52nd Aerospace Sciences Meeting, AIAA*, (1280), 1–7.
- Dropkin, A., Custodio, D., Henoch, C. and Johari, H. (2012). Computation of flow field around an airfoil with leading-edge protuberances. *Journal of Aircraft*, 49(5), 1345–1355.
- Guerreiro, J. E. and M. Sousa, J. (2012). Low-reynolds-number effects in passive stall control using sinusoidal leading edges. *AIAA Journal*, 50(2), 461–469.

- Favier, J., Pinelli, A. and Piomelli, U. (2012). Control of the separated flow around an airfoil using a wavy leading edge inspired by humpback whale flippers. *Comptes Rendus Mecanique*, 340(1), 107–114.
- Fernandes, I., Sapkota, Y., Mammen, T., Rasheed, A., Rebello, C. L. and Kim, Y. H. (2013). Theoretical and experimental investigation of the leading edge tubercles on the wing performance. *Aviation Technology, Integration, and Operations Conference*, AIAA, (4300), 1-41..
- Fish, F. (2006). Limits of nature and advances of technology: What does biomimetics have to offer to aquatic robots? *Applied Bionics and Biomechanics*, 3(1), 49–60.
- Fish, F. E. (1994). Influence of hydrodynamic-design and propulsive mode on mammalian swimming energetics. *Australian Journal of Zoology*, 42(1), 79–101.
- Fish, F. E. (1999). Performance constraints on the maneuverability of flexible and rigid biological systems. In *International Symposium On Unmanned Untethered Submersible Technology* (pp. 394–406)
- Fish, F. E. and Battle, J. M. (1995). Hydrodynamic design of the humpback whale flipper. *Journal of Morphology*, 225(1), 51–60.
- Fish, F. E. and Battle, J. M. (1995). Hydrodynamic design of the humpback whale flipper. *Journal of Morphology*, 225(1), 51–60.
- Fish, F. E., Howle, L. E. and Murray, M. M. (2008). Hydrodynamic flow control in marine mammals. *Integrative and Comparative Biology*, 48(6), 788–800.
- Fish, F. E. and Lauder, G. V. (2006). Passive and active flow control by swimming fishes and mammals. *Annu. Rev. Fluid Mech.*, 38, 193–224.
- Fish, F. E. and Lauder, G. V. (2013). Not just going with the flow. *Am Sci*, 101, 114–123.
- Fish, F. E., Weber, P. W., Murray, M. M. and Howle, L. E. (2011a). Marine Applications of the Biomimetic Humpback Whale Flipper. *Marine Technology Society Journal*, 45(4), 198–207.
- Fish, F. E., Weber, P. W., Murray, M. M. and Howle, L. E. (2011b). The tubercles on humpback whales flippers: application of bio-inspired technology. *Integrative and Comparative Biology*, 51(1), 203–213.
- Fish, F., Legac, P., Wei, T. and Williams, T. (2008). Vortex mechanics associated with propulsion and control in whales and dolphins. *Comparative Biochemistry and Physiology Part A: Molecular and Integrative Physiology*, 150(3), S65–S66.
- Fluent Ansys, (2015) Theory Guide Release 16.1, Ansys Inc.

Fluent Ansys, (2015) User's Guide Release 16.1, Ansys Inc..

Fouatih, O. M., Medale, M., Imine, O. and Imine, B. (2016). Design optimization of the aerodynamic passive flow control on NACA 4415 airfoil using vortex generators. *European Journal of Mechanics-B/Fluids*, 56, 82–96.

Gad-el-Hak, M. (2007). Flow control: passive, active, and reactive flow management. Cambridge University Press.

Gawad, A. F. A. (2012). Numerical simulation of the effect of leading-edge tubercles on the flow characteristics around an airfoil. *International Mechanical Engineering Congress and Exposition*. ASME 1-9.

Gawad, A. F. A. (2013). Utilization of whale-inspired tubercles as a control technique to improve airfoil performance. *Transaction on Control and Mechanical Systems*, 2(5), 212-218.

Gorunev, T. and Rockwell, D. (2009). Flow past a delta wing with a sinusoidal leading edge: near-surface topology and flow structure. *Experiments in Fluids*, 47(2), 321–331.

Green, J. E. (2008). Laminar flow control-back to the future? *8th Fluid dynamics conference and exhibit*. AIAA, 3738, 1-23.

Gross, A. and Fasel, H. (2013). Numerical Investigation of Passive separation control for an airfoil at low-reynolds-number conditions. *AIAA Journal*, 51(7), 1553–1565.

Gupta, A., Alsultan, A. and Ryo S. Amano. (2013). Numerical and experimental performance analysis of wind turbine blades. *AIAA Journal*, (3675), 1–12.

Halim, M. F. and Ahmad, K. A. (2013). CFD simulation of passive vortex generator on separated flow diffuser. Proceedings of Malaysian Technical Universities Conference on Engineering and Technology (MUCET) (pp. 1–6).

Hansen, K., Kelso, R. and Dally, B. (2010). An investigation of three-dimensional effects on the performance of tubercles at low reynolds numbers. *17th Australasian Fluid Mechanics Conference*, 5–9.

Hansen, K. L. (2012). Effect of leading edge tubercles on airfoil performance. *PhD dissertation, University of Adelaide*.

Hansen, K. L., Kelso, R. M. and Dally, B. B. (2009). The effect of leading edge tubercle geometry on the performance of different airfoils. *7th World Conference on Experimental Heat Transfer, Fluid Mechanics and Thermodynamics*. 599-608..

- Hansen, K. L., Kelso, R. M. and Dally, B. B. (2011). Performance variations of leading-edge tubercles for distinct airfoil profiles. *AIAA Journal*, 49(1), 185–194.
- Hansen, K. L., Kelso, R. M., Dally, B. B. and Hassan, E. R. (2011). Analysis of the streamwise vortices generated between leading edge tubercles. *6th Australian Conference on Laser Diagnostics in Fluid Mechanics and Combustion*, 99–102.
- Hansen, K. L., Kelso, R. M. and Doolan, C. J. (2010). Reduction of flow induced tonal noise through leading edge tubercle modifications. *16th AIAA/CEAS Aeroacoustics Conference*, AIAA. 1-10.
- Hansen, K. L., Kelso, R. M. and Doolan, C. J. (2012). Reduction of flow induced airfoil tonal noise using leading edge sinusoidal modifications. *Acoustics Australia*, 40(3), 172–177.
- Hua, X., Gu, R., Jin, J., Liu, Y., Ma, Y., Cong, Q. and Zheng, Y. (2010). Numerical simulation and aerodynamic performance comparison between seagull aerofoil and NACA 4412 aerofoil under low-Reynolds. *Advances in Natural Science*, 3(2), 244–250.
- Huang, G. Y., Shiah, Y. C., Bai, C. J. and Chong, W. T. (2015). Experimental study of the protuberance effect on the blade performance of a small horizontal axis wind turbine. *Journal of Wind Engineering and Industrial Aerodynamics*, 147, 202–211.
- Ibrahim, I. and New, T. (2015). A numerical study on the effects of leading-edge modifications upon propeller flow characteristics. *Ninth International Symposium on Turbulence and Shear Flow Phenomena (TSFP-9)*. 1-6.
- Ito, S. (2009). Aerodynamic influence of leading-edge serrations on an airfoil in a low Reynolds number. *Journal of Biomechanical Science and Engineering*, 4(1), 117–123.
- Johari, H., Henoch, C. W., Custodio, D. and Levshin, A. (2007). Effects of leading-edge protuberances on airfoil performance. *AIAA Journal*, 45(11), 2634–2642.
- Johnson, J. S. H. and Wolman, A. A. (1984). The humpback whale, *Megaptera novaeangliae*. *Marine Fisheries Review*, 46(4), 30–37.
- Karthikeyan, N., Sudhakar, S. and Suriyanarayanan, P. (2014). Experimental studies on the effect of leading edge tubercles on laminar separation bubble. In *52nd Aerospace Science Meeting*, AIAA, (1279), 1-16.
- Kim, J., Haeri, S. and Joseph, P. (2015). On the mechanisms of noise reduction in aerofoil-turbulence interaction by using wavy leading edges. *21st AIAA/CEAS Aeroacoustics Conference*, AIAA, (3269), 1-18

- Kim, M. J., Yoon, H. S., Jung, J. H., Chun, H. H. and Park, D. W. (2012). Hydrodynamic characteristics for flow around wavy wings with different wave lengths. *International Journal of Naval Architecture and Ocean Engineering*, 4(4), 447–459.
- Klan, S., Klaas, M. and Schroder, W. (2010). The Influence of Leading-Edge Serrations on the flow field of an artificial owl wing. *AIAA Journal*, (4942), 1–9.
- Kouh, J.-S., Lin, H.-T., Lin, T.-Y., Yang, C.-Y. and Bryan-Steven Nelson. (2011). Numerical study of Aerodynamic characteristic of protuberances wing in low reynolds number. *11th International Conference on Fluid Control Measurements and Visualization, FLUCOME 2011*. 1–6).
- Kumar, S. and Amano, R. (2012). Wind turbine blade design and analysis with tubercle technology. In ASME 2012 International Design Engineering Technical Conferences and Computers and Information in Engineering Conference, 5(70688), 859–872.
- Langtry, R. B. and Menter, F. R. (2009). Correlation-based transition modeling for unstructured parallelized computational fluid dynamics codes. *AIAA Journal*, 47(12), 2894–2906.
- Lau, A. H. S. and Kim, J. (2013). The effect of wavy leading edges on aerofoil-turbulence interaction noise. *Journal of Sound and Vibration*, 332(24), 6234–6253.
- Lau, A. S. H. (2012). High-order computations on aerofoil-gust interaction noise and the effects of wavy leading edges. *PhD Thesis, University of Southampton*.
- Lilley, G. M. (1998). A study of the silent flight of the owl. in 4th AIAA/CEAS Aeroacoustics Conference, 2340(1998), 1–6.
- Lin, J. C. (2002). Review of research on low-profile vortex generators to control boundary-layer separation. *Progress in Aerospace Sciences*, 38(4), 389–420.
- Lissaman, P. (1983). Low-Reynolds-number airfoils. *Annual Review of Fluid Mechanics*, 15(1), 223–239.
- Lohry, M. W., Clifton, D. and Martinelli, L. (2012). Characterization and design of tubercle leading-edge wings. *ICCFD7*, 1–11..
- Lohry, M. W., Martinelli, L. and Kollasch, J. S. (2013). Genetic algorithm optimization of periodic wing protuberances for stall mitigation. *31st AIAA Applied Aerodynamics Conference, AIAA*, 1–13.
- Mai, H., Dietz, G., Geißler, W., Richter, K., Bosbach, J., Richard, H. and de Groot, K. (2008). Dynamic stall control by leading edge vortex generators. *Journal of the American Helicopter Society*, 53(1), 26–36.

- Malipeddi, A. K., Mahmoudnejad, N. and Hoffmann, K. A. (2012). Numerical analysis of effects of leading-edge protuberances on aircraft wing performance. *Journal of Aircraft*, 49(5), 1336–1344.
- Mathews, J. and Peake, N. (2015). Noise generation by turbulence interacting with an aerofoil with a serrated leading edge. In *21st AIAA/CEAS Aeroacoustics Conference* (2204), 1-21.
- Menter, F. R. (1994). Two-equation eddy-viscosity turbulence models for engineering applications. *AIAA Journal*, 32(8), 1598–1605.
- Menter, F. R., Langtry, R., Likki, S., Suzen, Y., Huang, P. and Völker, S. (2006). A correlation-based transition model using local variables—Part I: model formulation. *Journal of Turbomachinery*, 128(3), 413–422.
- Miklosovic, D., Murray, M., Howle, L. and Fish, F. (2004). Leading-edge tubercles delay stall on humpback whale (*Megaptera novaeangliae*) flippers. *Physics of Fluids*, 16(5), L39-L42.
- Miklosovic, D. S., Murray, M. M. and Howle, L. E. (2007). Experimental evaluation of sinusoidal leading edges. *Journal of Aircraft*, 44(4), 1404–1408.
- Mueller, T. J. and Batil, S. M. (1982). Experimental studies of separation on a two-dimensional airfoil at low Reynolds numbers. *AIAA Journal*, 20(4), 457–463.
- Ozen, C. and Rockwell, D. (2010). Control of vortical structures on a flapping wing via a sinusoidal leading-edge. *Physics of Fluids*, 22(6), 021701-021704.
- Pechlivanoglou, G. (2012). Passive and active flow control solutions for wind turbine blades. *Phd dissertation, Universitätsbibliothek der Technischen University*.
- Pedro, H. T. and Kobayashi, M. H. (2008). Numerical study of stall delay on humpback whale flippers. *46th AIAA Aerospace Sciences Meeting and Exhibit*, (0584), 1-8.
- Polacsek, C., Reboul, G., Clair, V., Le Garrec, T. and Deniau, H. (2011). Turbulence-airfoil interaction noise reduction using wavy leading edge: An experimental and numerical study. In *INTER-NOISE and NOISE-CON Congress and Conference.*, 4464–4474.
- Reuster, J. G. and Baeder, J. D. (2000). A computational investigation of dynamic stall alleviation using leading edge deformation. In *18th Applied Aerodynamics Conference, AIAA Journal*, (4121), 247–257.
- Roger, M., Schram, C. and De Santana, L. (2013). Reduction of airfoil turbulence-impingement noise by means of leading-edge serrations and/or porous materials. *19th AIAA/CEAS Aeroacoustics Conference*, 1-20.

- Rostamzadeh, N., Kelso, R., Dally, B. and Kl Hansen. (2012). The Effect of Wavy Leading Edge Modification on NACA 0021 Airfoil characteristics. *18th Australian Fluid Mechanics conference*, 1-4.
- Rostamzadeh, N., Kelso, R. M., Dally, B. B. and Hansen, K. L. (2013). The Effect of Undulating Leading-edge Modification on NACA 0021 airfoil characteristics. *Physics of Fluids*, 25(117101), 1-20.
- Sahin, M., Sankar, L. N., Chandrasekhara, M. and Tung, C. (2003). Dynamic stall alleviation using a deformable leading edge concept-a numerical study. *Journal of Aircraft*, 40(1), 77–85.
- Selig, M. S., Deters, R. W. and Williamson, G. A. (2011). Wind tunnel testing airfoils at low reynolds numbers. *49th AIAA Aerospace, Sciences Meeting, AIAA*, 875, 4–7.
- Serakawi, A. R. and Ahmad, K. A. (2012). Experimental Study of Half-Delta Wing Vortex Generator for Flow Separation Control. *Journal of Aircraft*, 49(1), 76–81.
- Shi, W., Atlar, M., Norman, R., Aktas, B. and Turkmen, S. (2015). Biomimetic improvement for a tidal turbine blade. *11th European Wave and Tidal Energy Conference*, 1-6.
- Skillen A, Revell A, Favier J, Pinelli A, and Piomelli U. (2013). Investigation of wing stall delay effect due to an undulating leading edge: An LES study. *International Symposium On Turbulence and Shear Flow Phenomena*. 7, 1-6.
- Skillen, A., Revell, A., Pinelli, A., Piomelli, U. and Favier, J. (2014). Flow over a Wing with Leading-Edge Undulations. *AIAA Journal*, 53(2), 464–472.
- Spalart, P. R. and Allmaras, S. R. (1992). A one-equation turbulence model for aerodynamic flows. *AIAA Journal*, 092(0439).
- Stanway, M. J. (2008). Hydrodynamic effects of leading-edge tubercles on control surfaces and in flapping foil propulsion. *Master's Thesis, Massachusetts Institute of Technology*.
- Summers, A. and Wynne, P. J. (2004). As the Whale turns: The shape of the humpback's flippers might hold the secret to more maneuverable submarines. *Natural History*, 113(5), 24–25.
- Swanson, T. and Isaac, K. (2011). Biologically Inspired Wing Leading Edge for Enhanced Wind Turbine and Aircraft Performance *6th AIAA Theoretical Fluid Mechanics Conference*,. AIAA , (3533), 1-10.
- Van Nierop, E. A. (2009). *Flows in Films and Over Flippers*. PhD dissertation, Harvard University Cambridge, Massachusetts

- Van Nierop, E. A., Alben, S. and Brenner, M. P. (2008). How bumps on whale flippers delay stall: an aerodynamic model. *Physical review letters*, 100(5), 054502.
- Versteeg, H. K. and Malalasekera, W. (2007). An Introduction to Computational Fluid Dynamics: The Finite Volume Method. Pearson Education.
- Walters, D. K. and Cokljat, D. (2008). A three-equation eddy-viscosity model for Reynolds-averaged Navier-Stokes simulations of transitional flow. *Journal of Fluids Engineering*, 130(12), 121401.
- Wang, Y., Hu, W. and Zhang, S. (2015). Performance of the bio-inspired leading edge protuberances on a static wing and a pitching wing. *Journal of Hydrodynamics, Ser. B*, 26(6), 912–920.
- Watts, P. and Fish, F. (2001). The influence of passive, leading edge tubercles on wing performance. In *Proc. Twelfth Intl. Symp. Unmanned Untethered Submer. Technol.*
- Watts, P. and Fish, F. E. (2002). Scalloped wing leading edge. *US Patent 6,431,498*.
- Weber, P. W., Howle, L. E. and Murray, M. M. (2010). Lift, drag, and cavitation onset on rudders with leading-edge tubercles. *Marine Technology*, 47(1), 27–36.
- Weber, P. W., Howle, L. E., Murray, M. M. and Miklosovic, D. S. (2011). Computational Evaluation of the Performance of Lifting Surfaces with Leading-Edge Protuberances. *Journal of Aircraft*, 48(2), 591–600.
- Wei, Z., New, T. and Cui, Y. (2015). An experimental study on flow separation control of hydrofoils with leading-edge tubercles at low Reynolds number. *Ocean Engineering*, 108, 336–349.
- Downer, L and Dockrill, P, (2008), Wind Energy Institute of Canada. (2008). *Whalepower Tubercle Blade Power Performance Test Report*.
- Winn, L. K. and Winn, H. E. (1985). *Wings in the sea: the humpback whale*. University Press of New England.
- Wisuda. (2012). UPM External Balance Specification.
- Yoon, H., Hung, P., Jung, J. and Kim, M. (2011). Effect of the wavy leading edge on hydrodynamic characteristics for flow around low aspect ratio wing. *Computers and Fluids*, 49(1), 276–289.
- Yurchenko, N. (2011). From Marine Animals to Plasma Aerodynamics. In 49th AIAA Aerospace Sciences Meeting Including the New Horizons Forum and Aerospace Exposition (1341), 1–14.

- Zhang, L. H., Li, W. J. and Yin, J. X. (2013). Numerical Simulation of Bionic Wing for Drag Reduction. *Advanced Materials Research*, 602, 1761–1764.
- Zhang, M., Wang, G. and Xu, J. (2013). Aerodynamic control of low-Reynolds-number airfoil with leading-edge protuberances. *AIAA Journal*, 51(8), 1960–1971.
- Zhang, M., Wang, G. and Xu, J. (2014a). Effect of Humpback Whale-like Leading-Edge Protuberances on the Low Reynolds Number Airfoil Aerodynamics. In *Fluid-Structure-Sound Interactions and Control* (pp. 107–113).
- Zhang, M., Wang, G. and Xu, J. (2014b). Experimental study of flow separation control on a low-Re airfoil using leading-edge protuberance method. *Experiments in Fluids*, 55(4), 1–13.
- Zhang, X., Zhou, C., Zhang, T. and Ji, W. (2013). Numerical study on effect of leading-edge tubercles. *Aircraft Engineering and Aerospace Technology*, 85(4), 247-257
- Zhen, T. K., Zubair, M. and Ahmad, K. A. (2011). Experimental and numerical investigation of the effects of passive vortex generators on Aludra UAV performance. *Chinese Journal of Aeronautics*, 24(5), 577–583.
- Zhu, G.-H. (2008). Comment on ‘‘How Bumps on Whale Flippers Delay Stall: An Aerodynamic Model’’. *Physical Review Letters*, 101(10), 109401.
- Zverkov, I., Zanin, B. and Kozlov, V. (2008). Disturbances Growth in Boundary Layers on Classical and Wavy Surface Wings. *AIAA Journal*, 46(12), 3149–3158.