



UNIVERSITI PUTRA MALAYSIA

***DESIGN AND MODELING OF POWER TRANSISTOR-ASSISTED
SEN TRANSFORMERS FOR TRANSMISSION GRID
POWER FLOW CONTROL***

SALAH ELDEEN GASIM MOHAMED HASSAN

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SALAH ELDEEN GASIM MOHAMED HASSAN

**Thesis Submitted to the School of Graduate Studies, Universiti Putra Malaysia
in Fulfillment of the Requirements for the Degree of Doctor of Philosophy**

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DEDICATION

To the sole of my father, to my mother, wife, and brothers and sisters

with sincere and exceptional love



Abstract of thesis presented to the Senate of Universiti Putra Malaysia in fulfillment of the requirement for the degree of Doctor of Philosophy

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July 2017

Chair: Associate Professor Jasronita Jasni, PhD
Faculty: Engineering

Many arising factors endanger the secure and stable operation of transmission grids. Those are deregulation that opens transmission grid, increasing dynamics in consequence of wide integration of variable renewable energy sources, unwillingness to install new transmission lines, electric power demand increase, resulting stress that causes frequent components outage, uneven distribution of power in transmission lines, and resulting low utilization of existing transmission grid infrastructure. In consequence, the need to widely use transmission grid power flow controllers is escalating. However, these power flow controllers need to be reasonably costing as well as technically competent. Three main families of existing power flow controllers are conventional power flow controllers, flexible AC transmission systems controllers, and hybrid power flow controllers, which all have their pros and cons. Conventional power flow controllers are cost-effective, however, have technical shortcomings. Flexible AC transmission systems controllers are technically competent but their cost is high. Hybrid power flow controllers combine some advantages of the other two families, however, have their own limitations, and their cost is still high. Combination of most technical advantages of existing power flow controllers in a single power flow controller at a reasonable cost is promising. Based on a comprehensive review, a family of power transistor-assisted Sen Transformers that bridges the gap between unified power flow controller and Sen Transformer is proposed. Power transistor-assisted Sen Transformers are designed and their comprehensive Simulink model is developed and tested in *MATLAB/SIMULINK*. Ratings of components of a power transistor-assisted Sen Transformer are determined and its cost is analyzed and compared to that of a similar unified power flow controller. Operation principle of power transistor-assisted Sen Transformers, operational characteristics, and control strategies are revealed. Also, a simplified Simulink model and a comprehensive Newton-Raphson model of power transistor-assisted Sen Transformers are developed and validated. Performance of power transistor-assisted Sen Transformers for enhancement of optimal power flow and also for maintaining grid security is assessed and compared to that of Sen Transformer and unified power flow controller.

Methods used include simulation using *MATLAB/SIMULINK*, analytical Newton-Raphson based load flow analysis, optimal power flow, and simple power flow equations, besides voltage vector analysis. Among the significant findings, operational characteristics of power transistor-assisted Sen Transformers are found closely comparable to those of the unified power flow controller. Power transistor-assisted Sen Transformers operate continuously and provide repeatable control action, error-free, and ensure precise control action. They have non-limited operating points within their control area and ensures increased flexibility, improved response rate that enables mitigating transient stability problems, extended control range, and far lower cost as compared to an analogous unified power flow controller. As compared to an analogous conventional Sen Transformer, performance of power transistor-assisted Sen Transformer in enhancement of optimal power flow is found to be techno-economically feasible. Also, as compared to an analogous unified power flow controller, power transistor-assisted Sen Transformer is able to maintain grid security and found closely similar with a far lower installation cost. In conclusion, power transistor-assisted Sen Transformers are timely proposed competent and cost-effective power flow controllers those provide tremendous technical and economic benefits to the current days' and the future's smart grids.

Abstrak tesis yang dikemukakan kepada Senat Universiti Putra Malaysia sebagai memenuhi keperluan untuk ijazah Doktor Falsafah

**REKA BENTUK DAN PERMODELAN KUASA-TRANSISTOR
DIBANTU ALATUBAH SEN UNTUK KAWALAN
PENGHANTARAN ALIRAN KUASA GRID**

Oleh

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Terdapat pelbagai faktor yang timbul memberi ancaman khususnya pada operasi penghantaran grid yang selamat dan stabil. Antara faktor yang membahayakan operasi penghantaran grid termasuklah penyahkawalseliaan yang membuka penyaluran grid, peningkatan dinamik disebabkan oleh integrasi pelbagai sumber tenaga yang boleh diperbaharui yang meluas, keengganan untuk memasang talian penghantaran baru, permintaan kuasa elektrik yang meningkat, dan pengagihan talian kuasa yang tidak sekata, tekanan yang terhasil akibat komponen yang kerap terganggu meskipun penggunaan infrastruktur penghantaran grid yang kurang. Kesannya, keperluan penggunaan penghantaran aliran kuasa grid yang luas semakin meningkat. Namun begitu, untuk membolehkan penggunaan pengawal aliran kuasa yang luas, ianya memerlukan kos yang berpatutan dan cekap dari segi teknikal. Terdapat tiga kelompok utama pengawal aliran kuasa yang sedia ada iaitu pengawal aliran kuasa konvensional, pengawal sistem penghantaran arus ulang alik fleksibel, dan pengawal aliran kuasa hybrid, yang mempunyai kebaikan dan keburukan masing-masing. Pengawal aliran kuasa konvensional mempunyai kos yang efektif, walaubagaimanapun, ia mempunyai kelemahan dari segi teknikal. Pengawal sistem penghantaran arus ulang alik yang fleksibel pula cekap dari segi teknikal, namun ia memerlukan kos yang tinggi. Pengawal aliran kuasa hybrid menggabungkan beberapa kelebihan dari dua kelompok yang lain, namun begitu, pengawal aliran kuasa hybrid ini mempunyai had dan kos ia tetap tinggi. Gabungan pada kebanyakan kelebihan teknikal pengawal aliran kuasa yang sedia ada dalam pengawal aliran kuasa tunggal pada kos yang berpatutan adalah menarik. Berdasarkan pada keseluruhan kajian, kelompok transistor kuasa dibantu pengubah Sen menggabungkan jurang antara pengawal aliran kuasa bersatu dan pengubah Sen dicadangkan. Pengubah sen dibantu transistor kuasa direka dan Model *SIMULINK* komprehensif dibina dan diuji menggunakan *MATLAB/SIMULINK*. Penilaian untuk setiap komponen ditentukan dan kos pengubah sen dibantu transistor kuasa dianalisis

dan dibandingkan dengan analogi pengawal aliran kuasa bersatu. Prinsip operasi pengubah sen dibantu transistor kuasa, ciri-ciri operasi, strategi kawalan turut didedahkan. Selain itu, Model *SIMULINK* yang dipermudahkan dan Model Newton-Raphson Komprehensif daripada pengubah sen dibantu transistor kuasa turut dibina dan disahkan. Prestasi pengubah sen dibantu transistor kuasa dalam merealisasikan aliran kuasa optimum dan mengekalkan keselamatan grid telah dinilai dan dibandingkan dengan pengubah sen konvensional dan pengawal aliran kuasa bersatu. Kaedah yang digunakan juga termasuklah simulasi menggunakan *MATLAB/SIMULINK*, analisis Newton-Raphson berdasarkan aliran beban, aliran kuasa optimum dan penggunaan persamaan aliran kuasa yang mudah selain daripada analisis vektor voltan. Antara penemuan yang penting, ciri-ciri operasi pengubah sen dibantu transistor kuasa ditemui setanding dengan pengawal aliran kuasa bersatu. Pengubah sen dibantu transistor kuasa beroperasi secara berterusan dan menyediakan kawalan aksi yang berulang-ulang, tiada ralat dan memastikan tindakan kawalan yang tepat. Ia mempunyai titik operasi yang tidak terhad dalam kawasan kawalan serta memastikan peningkatan fleksibiliti, kadar tindakbalas yang bertambah baik yang membolehkan pengurangan masalah kestabilan sementara, pelbagai kawalan lanjutan dan kos yang jauh lebih rendah berbanding dengan analogi pengawal aliran kuasa bersatu. Jika dibandingkan dengan pengubah sen konvensional, pelaksanaan pengubah sen dibantu transistor kuasa dalam merealisasikan aliran kuasa optimum didapati tekno-ekonomi mampu dilaksanakan, dan jika di bandingkan dengan analogi pengawal aliran kuasa bersatu, pengubah sen dibantu transistor kuasa mampu mengekalkan grid keselamatan dan didapati hamper sama dengan kos pemasangan yang jauh lebih rendah. Kesimpulannya, pengubah sen dibantu transistor kuasa ini dicadangkan pada masa yang tepat dan kos efektif pengawal aliran kuasa yang menyediakan banyak kelebihan dari segi teknikal dan ekonomi pada penghantaran pintar pada masa kini dan akan datang.

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I certify that a Thesis Examination Committee has met on 27 July 2017 to conduct the final examination of Salah Eldeen Gasim Mohamed Hassan on his thesis entitled "Design and Modeling of Power Transistor-Assisted Sen Transformers for Transmission Grid Power Flow Control" in accordance with the Universities and University Colleges Act 1971 and the Constitution of the Universiti Putra Malaysia [P.U.(A) 106] 15 March 1998. The Committee recommends that the student be awarded the Doctor of Philosophy.

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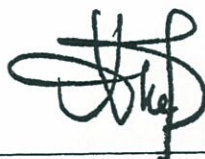
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Voltages are 1.03 pu, 1.02 pu)

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LIST OF ABBREVIATIONS

AC	Alternative Current
ACOPF	Alternative Current Optimal Power Flow
ASW	Active Smart Wires
ATC	Available Transfer Capability
AVR	Automatic Voltage Regulator
BES	Battery-based Energy Storage
BEST	Battery-based Energy Storage Transportation
BJT	Bipolar Junction Transistor
BTB	Back-To-Back
CB	Circuit Breaker
CD-PAR	Compact Dynamic Phase Angle Regulator
CM	Congestion Management
CMI	Cascade Multilevel Inverter
CNRM	Comprehensive Newton-Raphson Model
CNT	Controllable Network Transformer
CPFC	Conventional Power Flow Controller
CSM	Comprehensive Simulink Model
D	Duty Cycle
DC	Direct Current
DCOPF	Direct Current Optimal Power Flow
D-FACTS	Distributed Flexible AC Transmission Systems
DFC	Dynamic Flow Controller
DG	Distributed Generation
DPFC	Distributed Power Flow Controller
DR	Demand Response
DSSC	Distributed Static Series Compensator
DSI	Distributed Series Impedance
DVQS	Dual Virtual Quadrature Source
EGAT	Electricity Generating Authority of Thailand
ES	Energy Storage
ESC	Energy Storage Component
EST	Energy Storage Technology
EV	Electric Vehicle

FACTS	Flexible AC Transmission Systems
FC-TCR	Fixed Capacitor Thyristor Controlled Reactor
FR-BTB-PR	Fractionally Rated Back-To-Back Power Router
FRC	Fractionally Rated Converter
GIPFC	Generalized Interline Power Flow Controller
GR	Generation Rescheduling
GTO	Gate Turn-Off Thyristor
GUPFC	Generalized Unified Power Flow Controller
HE-UPFC	Hybrid Electromagnetic Unified Power Flow Controller
HFC	Hybrid Flow Controller
HVAC	High Voltage Alternating Current
HVDC	High Voltage Direct Current
HPFC	Hybrid Power Flow Controller
HPS	Hybrid Phase Shifter
IGBT	Insulated Gate Bipolar Transistor
IGCT	Integrated Gate Commutated Thyristor
IOOC	Integral On-Off Control
IPFC	Interline Power Flow Controller
ISO	Independent System Operator
IST	Improved Sen Transformer
LA-ST	Limited Angle Sen Transformer
LA-TAST	Limited Angle Power Transistor-Assisted Sen Transformer
LF	Load Flow
LS	Load Shedding
MC	Matrix Converter
MOSFET	Metal–Oxide–Semiconductor Field-Effect Transistor
MSC	Mechanically Switched Capacitor
MSR	Mechanically Switched Reactor
OGR	Optimal Generation Rescheduling
OLTC	On-Load Tap-Changing
OPF	Optimal Power Flow
OTS	Optimal Transmission Lines Switching
OUPFC	Optimal Unified Power Flow Controller
PAC	Phase Angle Control
PEs	Power Electronics

PFC	Power Flow controller
PI	Performance Index
PST	Phase Shifting Transformer
PWM	Pulse Width Modulation
RDTR	Real-time Dynamic Thermal Rating
RMS	Root Mean Square
RM	Runkle Machine
RPST	Rotary Phase Shifting Transformer
RPFC	Rotary Power Flow Controller
RSW	Reporting Smart Wires
RT	Rotary Transformer
SCR	Silicon Controlled Rectifier
SiC	Silicon Carbide
SPS	Static Phase Shifter
SR	Saturable Reactor
SSM	Simplified Simulink Model
SSSC	Static Synchronous Series Compensator
STATCOM	Static Synchronous Compensator
ST	Sen Transformer
SVC	Static Var Compensator
SW	Smart Wire
TACC	Thin AC Converter
TAST	Power Transistor-Assisted Sen Transformer
TCPS	Thyristor Controlled Phase Shifter
TCR	Thyristor Controlled Reactor
TCSC	Thyristor Controlled Series Capacitor
THD	Total Harmonic Distortion
TLOA	Transmission Lines Overload Alleviation
TNB	Tenaga Nasional Berhad
TRIAC	Triode for AC
TS	Transmission Lines Switching
TSC-TCR	Thyristor Switched Capacitor Thyristor Controlled Reactor
TSR	Thyristor Switched Capacitor
TSS	Two Separate Shafts
TSSC	Thyristor Switched Series Capacitor

TSSR	Thyristor Switched Series Reactor
TST	Transistorized Sen Transformer
TUPFC	Transformer-less Unified Power Flow Controller
UPFC	Unified Power Flow Controller
VFT	Variable Frequency Transformer
VRES	Variable Renewable Energy Source
VRT	Voltage Regulating Transformer
VSI	Voltage-Source Inverter
V2G	Vehicle To Grid



LIST OF SYMBOLS

a_o	DC component (V) or (A)
a_k and b_k	Fourier coefficients
B	Shunt susceptance of transmission line (mho), which is the imaginary part of the shunt admittance Y
B_{kk}	Self susceptance at bus k (mho)
b_{km}	Series susceptance of transmission line (mho) between buses k and m , which is the imaginary part of the series admittance Y_{km} . It includes that of the PFC if connected
c_1^k	Sensitivity of PI with respect to V_T
c_2^k	Sensitivity of PI with respect to ϕ_T
D	Duty cycle
f	Frequency (Hz)
G_{kk}	Self-conductance at bus k (mho)
g_{km}	Series conductance of transmission line (mho) between buses k and m , which is the real part of the series admittance Y_{km} . It includes that of the PFC if connected
I	Current in a transmission line (A)
I_r	Current at the receiving end of a transmission line (A)
I'_k	Current at the effective sending end k' of a transmission line (A)
I_T	Active component of the exciter current of the TAST (A)
I_q	Reactive component of the exciter current of the TAST (A)
Im	Imaginary part of a complex quantity
J	Imaginary unit which is the root of -1
k	Harmonics order
m	Transmission line number
N_l	Number of transmission lines in a grid
N_b	Number of buses in the transmission grid
n	Bus number
n	Real positive integer
P_s	Active power at the sending end of a transmission line (W)
P_r	Active power at the receiving end of a transmission line (W)
P_n	Active power injected at bus n (W)
P_{js}	Addition in the injected active power at bus j as a consequence of the presence of the PFC (W)

P_{km}	Active power flow from bus k to bus m (W)
P_{lm}	Active power flow in line m (W)
P_i^1	Active power flow in line i at terminal bus 1 (W)
P_{lm}^{max}	Maximum allowed active power flow in line m (W)
$P_{se(TAST)}$	Active power of the series part of TAST (W)
$P_{sh(TAST)}$	Active power of the shunt part of TAST (W)
P_{exch}	Active power exchange between line and TAST (W)
Q_s	Reactive power at the sending end of a transmission line (VAR)
Q_r	Reactive power at the receiving end of a transmission line (VAR)
Q_i^1	Reactive power flow in line i at terminal bus 1 (VAR)
Q_{exch}	Reactive power exchange between line and TAST (VAR)
Q_{km}	Reactive power that flow from bus k to bus m (VAR)
$Q_{se(TAST)}$	Reactive power of the series part of TAST (VAR)
R_i	Resistance of transmission line i (Ω)
Re	Real part of a complex quantity
r_{km}	Series resistance (Ω) of transmission line between buses k and m , which is the real part of the series impedance Z_{km} , it includes that of the PFC if connected
S_{km}	Apparent power that flow from bus k to bus m (VA)
$[S]$	Matrix that relates lines flow with the power injections at the buses
S_{mn}	mn^{th} element of Matrix $[S]$
s	Slack or reference bus
T	Period of a signal (s)
t	Time (s)
t_{ON}	On time (s)
t_{OFF}	Off time (s)
V_k	Voltage at bus k (V)
V_p	Peak voltage (V)
V_m	Voltage at bus m (V)
V_S	Voltage at the sending end of a transmission line (V)
V'_S	Effective sending end voltage of a transmission line (V)
V'_k	Effective voltage at bus k' (V)
V_{ST}	The series injection voltage that ST provides (V)
V_{TST}	The series injection voltage that TST provides (V)

V_{TAST}, V_T	The series injection voltage that TASTs provide (V)
V_{cR}	Magnitude of the series injection voltage of PFC (V)
$V_{T(\min)}$	Minimum series injection voltage that TASTs provide (V)
$V_{T(\max)}$	Maximum series injection voltage that TASTs provide (V)
V_d	Direct axis component of the series injection voltage (V)
V_q	Quadrature axis component of the series injection voltage (V)
$v_{TST(in)}$	Input voltage of the TST (V)
$v_{TST(out)}$	Output voltage of the TST (V)
X, X_l	Series reactance of transmission line (Ω)
X_i	Reactance of transmission line i (Ω)
X_k	A control parameter of the PFC
X_{se}	Series reactance of the PFC (Ω)
x_{km}	Series reactance (Ω) of transmission line between buses k and m , which is the imaginary part of the series impedance Z_{km} , it includes that of the PFC if connected
Y_{km}	Series admittance of transmission line (mho) between buses k and m , It includes that of the PFC if connected
Y_{bus}	Admittance matrix of the system
Z_i	Impedance of transmission line i (Ω)
δ	Transmission angle ($^\circ$)
δ_s	Phase angle of the voltage at the sending bus s ($^\circ$)
δ_r	Phase angle of the voltage at the receiving bus r ($^\circ$)
δ'_s	Phase angle of the voltage of the effective sending end (V)
δ_{cR}	Phase angle of the series injection voltage of PFC ($^\circ$)
$\frac{\partial P_k}{\partial \theta_k}$	Jacobian matrix element, which is the first derivative of the active power at bus k to phase angle of voltage at bus k
ΔP_k	Active power mismatch at bus k (W)
ΔQ_k	Reactive power mismatch at bus k (VAR)
$\Delta \theta_k$	Phase angle mismatch at bus k ($^\circ$)
ΔV_k	Voltage magnitude mismatch at bus k (V)
ΔP_{bb}	Active power mismatch of the shunt and series of the TAST (W)
θ_i	Phase angle of the impedance of transmission line i ($^\circ$)
θ_k	Phase angle of voltage at bus k ($^\circ$)
θ_m	Phase angle of voltage at bus m ($^\circ$)
θ_{km}	Angle of the series admittance ($^\circ$) of transmission line between

	buses k and m
$\phi_{(ST)}$	Angle of the series injection voltage of the ST ($^{\circ}$)
$\phi_{(TST)}$	Angle of the series injection voltage of the TST ($^{\circ}$)
$\phi_{(TAST)}, \phi_T$	Angle of the series injection voltage of the TASTs ($^{\circ}$)
$\phi_{T(\min)}$	Minimum angle of the voltage of the TASTs ($^{\circ}$)
$\phi_{T(\max)}$	Maximum angle of the voltage of the TASTs ($^{\circ}$)
ω	Angular power frequency (rad/sec)
ω_s	Angular switching frequency (rad/sec)
ω_m	Real positive weighting coefficient reflects importance of line m



LIST OF SI UNITS

Quantity	SI Unit	SI Unit Name
Voltage	V	Volt
Current	A	Ampere
Resistance	Ω	Ohm
Inductance	H	Hennery
Capacitance	F	Farad
Frequency	Hz	Hertz
Angular Frequency	rad/s	Rad per second
Phase angle	$^{\circ}$	Degree
Time	s	Second
Length	km	Kilometer

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CHAPTER 1

INTRODUCTION

1.1 Background

Many factors adversely affect transmission grid operation and endanger power system security and stability. Among these factors is deregulation of the electricity sector, heavy penetration of Variable Renewable Energy Sources (VRESs), increase of electricity demand, and unwillingness to install new transmission lines. Deregulation of the electricity sector makes the grid open access and gives rise to many difficulties in its operation and control [1]. Heavy penetration of VRESs, especially wind and solar is becoming more and more widespread [2, 3]. These VRESs possess an intermittent nature that accordingly increases grid dynamics, and are non-dispatch-able energy sources [4]. The steady increase in the demand for electrical energy stresses the operation [5]. It consequently increases the chance of components outage that may endanger the operation security [6, 7]. On the other hand, while some transmission lines are congested, some others are lightly loaded [8]. In most cases, utilization of the existing grid infrastructure is low [5, 9, 10]. Concurrently, transmission of more bulk active power at reasonable costs has become more essential. Suitable means for corrective actions that facilitate successful operation of the transmission grids, secure, and stabilize power system operation are crucial. Installation of new lines can relieve the stress. However, its growth rate is slow and the installation is limited by many factors such as high costs, public policies and right of way [5, 11]. Accordingly, there is a relatively small investment in the transmission networks [12, 13]. Also, installation of new lines may not add the required degree of controllability, flexibility, selectivity, precision, and fast control. In such circumstances, a smarter and more dynamically controllable grid is of paramount importance [14]. Greater operating flexibility and controllability are significant as they enable meeting the needs of modern power systems [15]. To this end, implementation of transmission grid Power Flow Controllers (PFCs) and their wide use is imperative as they provide economic and effective solutions [5, 16]. The continuous control enables smooth moving from a steady-state operating condition to another and prevents systems collapse [7]. Besides, the PFCs can realize a self-healing grid that can flexibly, precisely, and quickly respond to the varying operating conditions, and enable harvesting more power from the VRESs. Also, they can augment the power transfer capability and delay or even eliminate the need to install new lines and to ensure the system is able to operate optimally, securely and stably. Nonetheless, both technically and economically attractive PFCs should be used.

Existing transmission grid PFCs can be divided mainly into Conventional PFCs (CPFCs), Flexible AC Transmission Systems (FACTS) controllers, and Hybrid PFCs (HPFCs). CPFCs include mechanically switched capacitors and reactors, transformer and On-Load Tap-Changing (OLTC)-based PFCs such as the Voltage Regulating Transformer (VRT), Phase Shifting Transformer (PST), and recently, Sen

Transformer (ST) and Limited Angle STs (LA-STs) [17, 18]. They also include rotational PFCs, which are the Variable Frequency Transformer (VFT) and Rotary PFC (RPFC). Most dominant FACTS controllers are the Static Var Compensator (SVC), Thyristor Controlled Series Capacitor (TCSC), Static Synchronous Compensator (STATCOM), Static Series Synchronous Compensator (SSSC), Thyristor Controlled Phase Shifter (TCPS), Unified Power Flow Controller (UPFC), and Interline Power Flow Controller (IPFC) [19]. Finally, HPFCs are the Improved ST (IST), Hybrid Phase Shifter (HPS), Hybrid Flow Controller (HFC), Controllable Network Transformer (CNT), Fractionally Rated Back-to-Back converter-based Power Router (FR-BTB-PR), and Compact Dynamic Phase Angle Regulator (CD-PAR).

Advantages of the CPFCs include providing compensation voltage with system frequency without any harmonics, high efficiency, and for most of them, simple construction and simple control [17, 20, 21]. They are also based on technologically proven components and are generally less expensive. Challenges of the CPFCs include their step-wise operation [18], limited operating points and thus, less flexibility, control-error for the transformer and OLTC-based PFCs [20, 22, 23]. They also include the complexity, and rating limitations for the rotational PFCs, as well as the relatively slow response for the rotational PFCs, and slower response in the range of 2 seconds to switch between adjacent taps for OLTC-based CPFCs [18, 24]. It is often not possible to maintain the reliability by conventional mechanical means alone [7].

Advantages of FACTS controllers include their continuous operation mode, high flexibility, precise and tight transmission control action, and fast acting capability [7, 18]. Challenges of FACTS controllers include their high installation costs [21] and thus limited use [25-27], and relatively high operational losses [17, 21]. They also include production of harmonics that necessitate more costly converter topologies or extra components for neutralization, complex construction [28] and complex and expensive control [20].

Advantages of HPFCs include integration of fractionally-rated components that are low-costing and add advantageous characteristics such as the continuous operation mode, high flexibility, precise and error-free control action, and fast response [22]. Challenges of HPFCs differ for the different types with different components and operation principles. They include level of complexity of construction and control, the cost which, is generally less compared to that of the FACTS, but, is still high [29] and the low order harmonics that some of them produce [30, 31]. They also include the power flow control range that they cover as some of them only control active power [32]; some are optimized for active power flow control [30] and some for reactive power flow control [31]. Also, some operate in step-wise mode [33], and some combine energy storage components [23, 34] that may reduce their reliability.

1.2 Problem Statement

In present and future circumstances of power transmission grids, there is an increasing flexibility and controllability requirement [35, 36] owing to existence of many challenging factors [37]. Also, extensive use of FACTS controllers is the main goal ever since their first development [19, 38] as they present key remedies to the power grids arising problems. However, PFCs that are technically competent to realize the transmission grid control goals, and economically effective to enable the wide use, are essential. Nonetheless, installation and operating costs of the FACTS controllers, in particular the Unified Power Flow Controller (UPFC), are high [19, 21, 39, 40]. As a result, there are only three practically installed UPFCs currently [25-27]. Conversely, the comparable conventional Sen Transformer (ST) is relatively cheap [17, 18, 41-43], but, has some technical drawbacks. The step-wise operation, limited operating points, less flexibility, control-error [23], and the relatively slow response of the conventional ST cannot always ensure the exact precision, and desired degree of flexibility and response-rate [15]. While there is an increasing flexibility and controllability requirement in transmission grid operation and control, the high cost of the UPFC negates its wide use, and the technical drawbacks of the ST result in limitations in degree of flexibility, controllability, and preciseness. There is technology gap between the ST and the UPFC that is beneficial to bridge. Bridging such gap enables wide use of effective PFCs to meet the increasing flexibility and controllability requirements.

1.3 Aim and Objectives of Thesis

Difficulty of maintaining secure, stable, and optimized operation of power grids is increasing [44-46]. This situation augments the needs for flexible and self healing grids. In response to that, this thesis aims to bridge the technology gap between the ST and the UPFC to contribute towards meeting the increasing needs to use PFCs in transmission grids, by proposing Power Transistor Assisted ST (TAST) and Limited Angle TASTs (LA-TASTs) as technically competent and economically attractive PFCs. The thesis also aims to techno-economically assess performance of TASTs in significant applications in different power grid test systems.

The objectives, which are set to meet these aims, are:

- i. To design the TASTs, determine ratings of their components, and develop their Comprehensive *SIMULINK* Model (CSM).
- ii. To demonstrate the operational characteristics and control strategies of TAST, test its action, and compare it to that of conventional ST and UPFC, and to investigate the installation costs of a TAST, and compare it to that of a similar UPFC.
- iii. To develop the mathematical Comprehensive Newton-Raphson (NR) Model (CNRM) and the Simplified *SIMULINK* Model (SSM) of the TAST and compare them.

- iv. To assess performance of a TAST in enhancement of the OPF and also in maintaining transmission grid security, and comparing it to similar conventional ST and/or UPFC.

1.4 Scope of Research

Scope of this research covers device level and power system level. In the device level, following a comprehensive review of existing PFCs, a set of new PFCs is proposed. It is the family of TASTs that consists of a basic ST and a fractionally rated Transistorized ST (TST). The TAST is designed and then modeled in *MATLAB/SIMULINK* including the power circuits and the IGBT's driving circuits. The work includes determination of ratings of the components and selection of a suitable AC-AC voltage regulator, the AC-AC chopper, that fits the operation principle of the TAST, and selection of a suitable switching technique. Different control strategies of the TAST are presented. Besides, a TAST's and equivalent ST's and UPFC's operating areas are compared. The work also included demonstration of the improved response rate of TAST as compared to that of conventional ST, and performing harmonics analysis. TAST's cost analysis and comparison with that of a similar UPFC is presented. Additionally, to cover a narrower operating area at a lesser cost, the LA-TASTs are proposed, designed and modeled. In power system level that is related to steady-state power system analysis, performance of TAST is assessed and compared to that of conventional ST and/or UPFC. For that purpose, firstly, power grids including a TAST are modeled in environment of *MATLAB/SIMULINK*. Then, the mathematical CNRM of the TASTs is developed for use in the steady-state Load Flow (LF) analysis. Finally, performance of the TAST is assessed in two significant applications; enhancement of the OPF to reduce the generation cost, and enhancement of transmission grid security.

The research facilitates meeting the increasing requirement of grid controllability and flexibility [47-49] through use of competent and cost effective novel PFCs. The research rectifies the economic demerits of the UPFC and the technical drawbacks of the conventional ST. Possessing most advantages of the UPFC and conventional ST, the TASTs bridge the technology gap. The TASTs provide closely comparable characteristics to the UPFC at far lower cost and thus can be widely used. In the current circumstances of grid operation and the continuing trends, the TASTs represent timely proposed valuable tools that can aid the security and stability, and optimize operation of power systems. TASTs can help open up transmission lines' bottlenecks to push huge amounts of active power, and better utilize the existing grid infrastructure. They can aid integration of more VRESs, and ease harnessing much more of their power. The continuous and smooth control action of the TASTs is advantageous as such characteristics provide repeatable option for power system control [50-52]. The error-free control of the TASTs ensures that it is able to provide the desired precise control action similar to that achieved by a UPFC conversely to the conventional ST [41]. The non-limited operating points of the TASTs, within their control range, provide increased flexibility to grid operations and a performance that is closely similar to that of UPFC. Nonetheless, besides the advantageous technical features, cost of the TAST is far lower compared to that of

the UPFC. Moreover, the extended control range of the TAST reveals that it can operate in some cases beyond the limits of a UPFC that costs more. Also, the improved response of the TAST (in the range of milliseconds) within the operating circles of the TST enables the TAST to mitigate transient stability problems, and control the VRESs to harness more of their power [50].

- i. A novel TAST is proposed for use in dynamic power flow control of transmission grids and enhancement of utilization of existing grid infrastructure. TAST proved to be versatile and closely comparable to UPFC with a far lower installation cost. It can replace UPFC for many utility applications.
- ii. Novel LA-TASTs are proposed for dynamic power flow control of transmission grids and enhancement of utilization of existing grid infrastructure. A LA-TAST has less components count as compared to TAST and thus costs less. It covers a limited-angle control-area that is satisfactory for a specific purpose.
- iii. An accurate model of TAST: CSM is developed for the use in the device level, and its results are validated.
- iv. Two accurate models of TASTs: *SIMULINK*-based, and mathematical comprehensive Newton-Raphson based, are developed, and their results are validated. They are significant tools for steady-state analysis of power systems that incorporate a single TAST or more.

1.5 Outlines of Thesis

Chapter 1 highlights current state of power transmission grids, and existing transmission grid PFCs. It states the problem, introduces aim and objectives of the thesis, and finally presents scope of the research. Chapter 2 of this thesis displays the literature review. The challenges that face transmission grids and the mitigation measures are introduced. Among the mitigation measures, power flow control is emphasized. Benefits of power flow control are emphasized, its fundamental principle is presented, existing PFCs are compared, and based on that, a technology gap between most versatile existing PFCs is emphasized and family of proposed TASTs is introduced.

Chapter 3 of the thesis introduces methodology. Methods of simulation, analytical, and vector analysis are used. Simulation is performed using *SIMULINK* of *MATLAB*. Analytical methods include *Newton-Raphson* based LF analysis and simple power flow equations. Vector analysis is performed utilizing *Microsoft Visio*. Optimal power flow is performed using *MATPOWER*. TASTs are designed, and modeled and the models are validated. Ratings of its components are determined, and operation principle is introduced. More than a method is used in each single study for purpose of validation.

Chapter 4 presents results and discussion. The CSM of TAST is utilized to test its action in regulating voltage and power flow. Control strategies and operational characteristics of TAST are revealed and advantages are presented. TAST's operational characteristics are compared to those of a similar ST. Also, installation cost of a TAST is analyzed and compared to that of a similar UPFC. Validity of the SSM and CNRM is demonstrated prior to their use in power system level. Finally, performance of the TASTs is assessed in two different applications, which are enhancement of the OPF and transmission grid security. In the first application, TAST is techno-economically compared to a similar conventional ST. In the second, TAST is compared to a similar UPFC bearing in mind regulating voltage of shunt bus of the UPFC.

Chapter 5 concludes the thesis. It highlights significance of the research, stresses the findings in line with the objectives, and states key contributions of the thesis. It then acknowledges the limitations, and gives recommendations for future research. Finally, list of the publications that are accompanied by the thesis is provided.

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