

UNIVERSITI PUTRA MALAYSIA

EFFECT OF BIAXIAL FABRIC PRESTRESSING ON THE MECHANICAL PROPERTIES OF PLAIN–WEAVE E–GLASS/POLYESTER COMPOSITES

NAWRAS HAIDAR MOSTAFA

FK 2017 104



EFFECT OF BIAXIAL FABRIC PRESTRESSING ON THE MECHANICAL PROPERTIES OF PLAIN–WEAVE E–GLASS/POLYESTER COMPOSITES



NAWRAS HAIDAR MOSTAFA

Thesis Submitted to the School of Graduate Studies, Universiti Putra Malaysia, in Fulfillment of the Requirements for the Degree of Doctor of Philosophy

May 2017

COPYRIGHT

All material contained within the thesis, including without limitation text, logos, icons, photographs and all other artwork, is copyright material of Universiti Putra Malaysia unless otherwise stated. Use may be made of any material contained within the thesis for non–commercial purposes from the copyright holder. Commercial use of material may only be made with the express, prior, written permission of Universiti Putra Malaysia.

Copyright © Universiti Putra Malaysia



DEDICATION

This thesis is dedicated to my parents and my wife for their love and support. Without them, none of this would have been possible.

Nawras H. Mostafa May 2017

Abstract of thesis presented to the Senate of Universiti Putra Malaysia in fulfillment of the requirement for the Degree of Doctor of Philosophy

EFFECT OF BIAXIAL FABRIC PRESTRESSING ON THE MECHANICAL PROPERTIES OF PLAIN–WEAVE E–GLASS/POLYESTER COMPOSITES

By

NAWRAS HAIDAR MOSTAFA

May 2017

Chairman : Associate Professor Nur Ismarrubie Bt Zahari, PhD Faculty : Engineering

It is of interest whether induced residual stresses would affect the mechanical properties of fibre–reinforced composites. One of the methods that can be used for altering the induced residual stresses within the matrix is the method of fibre prestressing. Although this method was previously used for developing the mechanical properties of unidirectional composites, its application to the woven composites was very rare. There are many applications of composite materials where woven fabric has been used instead of unidirectional fibre such as for helmets, armours, boats, and the automotive components. The mechanical properties of woven composite may be improved without increasing its volume and/or weight. Therefore, this study emphasizes on improving the mechanical properties and fatigue behaviour of the plain–weave composite by applying biaxial fabric prestressing.

Firstly, the induced residual stresses within the composite's constituents due to fibre prestress was calculated theoretically by developing the macro-mechanics theory. Secondly, numerical modelling of the prestressed composites was implemented using ANSYS[®] software for validating the theoretical results and estimating the full distribution of the residual stresses within the composite's constituents. The biaxial prestressing frame was used for providing biaxial fabric pretension load. Prestressed composites were manufactured with different levels of prestressing ranging from 25 to 100 MPa and prepared at different fibre orientation angles such as 0, 15, 30 and 45°. Lastly, experimental tests such as tensile, flexural and fatigue were conducted on the E–glass plain–weave/polyester resin composite in order to assess the advantages that might result from applying biaxial fabric prestressing.



Theoretical results showed that the level of the induced residual stresses within the composite's constituents depends on fibre prestress level, fibre volume fraction, and the elastic properties of the composite's constituents. Residual stresses calculated by the developed macro-mechanics theory were in agreement with those obtained by the numerical modelling and previous studies of no less than 1.53%. Numerical simulation of the prestressed composite showed that the maximum induced residual stresses due to fibre prestressing were located at the fibre-matrix interface. Increasing the fibre prestress level increases both the induced compressive residual stresses within the matrix and the fibre-matrix interfacial shearing stress. Experimental results showed that prestressing level of 50 MPa offered the highest improvement in the quasi-static properties and fatigue life behaviour. Enhancements in the tensile and flexural properties were about 20% (from 3.74 to 4.4 GPa of tensile modulus and from 35 to 42 MPa of critical stress) and 15% (from 2.54 to 2.96 GPa of flexural modulus and from 87.11 to 99.88 MPa of flexural strength), respectively. Fatigue cycles to failure were prolonged up to 43% (from 19949 to 28594 cycles) at 0.4 normalised peak stress in comparison with non-prestressed counterparts. The levels of improvement were reduced with increasing the fibre orientation to 45°. Empirical functions were estimated to include the prestress effect in the tensile, flexural and fatigue behaviours. Prestressed composite specimens with 50 MPa showed a decline in the improved tensile strength, flexural strength and fatigue cycles to failure which were about 3.56 % (from 42.07 to 40.56 MPa), 1.96% (from 99.88 to 97.92 MPa) and 14.55% (from 28594 to 24432 cycles) after six months since they were manufactured, respectively. These declines resulted from the stress relaxation effect within the matrix.

Considering all findings, it was concluded that the proposed prestressing method enhanced the mechanical properties of the plain-weave composite. This improvement resulted from increasing the composite resistance against quasi-static and fatigue loadings by reducing both fibre waviness and the tensile residual stresses induced within the matrix. The fibre prestress method enhanced the mechanical properties of the plain-weave composite in both on-axis and off-axis directions. These improvements still existed after complete redistribution of the induced residual stresses within the matrix. Abstrak tesis yang dikemukakan kepada Senat Universiti Putra Malaysia sebagai memenuhi keperluan untuk Ijazah Doktor Falsafah

KESAN PRATEGASAN FABRIK DWIPAKSI KE ATAS SIFAT-SIFAT MEKANIKAL KOMPOSIT E-KACA/POLIESTER TENUNAN-BIASA

Oleh

NAWRAS HAIDAR MOSTAFA

Mei 2017

Pengerusi : Profesor Madya Nur Ismarrubie Bt Zahari, PhD Fakulti : Kejuruteraan

Adalah sesuatu yang diminati sama ada tegasan baki akan memberi kesan kepada sifat mekanikal bahan komposit bertetulang-gentian. Salah satu kaedah yang boleh digunakan untuk mengubah tegasan baki yang diaruhi di dalam matriks ialah kaedah prategasan gentian. Walaupun kaedah tersebut sebelum ini digunakan untuk membangunkan sifat-sifat mekanikal komposit satu-arah, penggunaanya bagi komposit tenunan sangat jarang berlaku. Terdapat banyak penggunaan bahan komposit di mana fabrik tenun telah digunakan dan bukan gentian satu-arah seperti untuk topi keledar, perisai, bot, dan komponen automotif. Sifat mekanikal komposit tenunan boleh ditambah baik tanpa meningkatkan isipadu dan/atau beratnya. Oleh itu, kajian ini memberi penekanan kepada peningkatan sifat mekanikal dan tingkah laku lesu komposit tenunan biasa dengan menggunakan prategasan fabrik dwipaksa.

Pertama, tegasan baki teraruh di dalam juzuk komposit akibat prategasan gentian dikira secara teori dengan membangunkan teori makro-mekanik. Kedua, pemodelan berangka bagi komposit prategasan telah dilaksanakan menggunakan perisian ANSYS[®] untuk mengesahkan hasil teori dan menganggarkan agihan sepenuhnya tegasan baki di dalam juzuk komposit ini. Bingkai prategasan dwipaksi digunakan untuk menyediakan beban prategangan fabrik dwipaksa. Komposit prategasan telah dibuat dengan tahap prategasan yang berbeza berjulat antara 25 hingga 100 MPa dan disediakan dengan sudut orientasi gentian yang berbeza seperti 0, 15, 30 dan 45°. Keputusan ujikaji seperti tegangan, lenturan dan lesu telah dijalankan ke atas komposit tenunan-biasa sistem E-kaca/poliester untuk menilai kelebihan yang mungkin timbul daripada penggunaan prategasan dwipaksa fabrik.

iii

Keputusan teori menunjukkan bahawa tahap tegasan baki yang teraruh di dalam juzuk komposit bergantung pada tahap prategasan gentian, pecahan isipadu gentian, dan sifat elastik juzuk komposit. Tegasan baki yang dikira dengan teori makromekanik yang dibangunkan adalah sepadan dengan yang diperoleh oleh pemodelan berangka dan kajian terdahulu dengan nilai kurang daripada 1.53%. Simulasi berangka komposit prategasan menunjukkan bahawa tegasan baki teraruh maksimum disebabkan oleh prategasan gentian terletak pada antara muka gentianmatriks. Meningkatkan tahap prategasan gentian boleh meningkatkan kedua-dua tegasan sisa mampatan teraruh di dalam matriks dan tegasan ricih antara muka seratmatriks. Keputusan ujikaji menunjukkan bahawa paras prategasan 50 MPa boleh memberikan peningkatan tertinggi bagi sifat-sifat kuasi-statik dan tingkah laku jangka hidup lesu. Tambahan pada sifat tegangan dan lenturan adalah lebih kurang 20% (daripada 3.74 hingga 4.4 GPa modulus tegangan dan 35 hingga 42 MPa tegasan kritikal) dan 15% (daripada 2.54 hingga 2.96 GPa modulus lenturan dan dari 87.11 hingga 99.88 MPa kekuatan lenturan) masing-masing. Kitaran sehingga kegagalan lesu telah dipanjangkan hingga 43% (daripada 19949 hingga 28594 kitaran) pada tekanan puncak normal 0.4 berbanding dengan yang tanpaprategasan. Tahap peningkatan telah dikurangkan dengan meningkatkan orientasi gentian ke arah pincang. Fungsi empirikal dianggarkan termasuk kesan prategasan ke atas tingkah laku tegangan, kelenturan dan lesu. Spesimen komposit prategasan dengan 50 MPa menunjukkan penurunan dalam kekuatan tegangan, kekuatan lenturan dan kitaran lesu yang lebih baik hingga kegagalan yang kira-kira 3.56% (daripada 42.07 hingga 40.56 MPa), 1.96% (daripada 99.88 hingga 97.92 MPa) dan 14.55% (daripada 28594 hingga 24432 kitaran)selepas enam bulan dibuat, masingmasing. Penurunan ini adalah hasil daripada kesan tekanan santaian di dalam matriks.

Berdasarkan kepada penemuan, disimpulkan bahawa kaedah prategasan yang dicadangkan dapat meningkatkan sifat mekanikal komposit tenunanbiasa. Peningkatan ini hasil daripada peningkatan rintangan komposit terhadap beban kuasi-statik dan lesu dengan mengurangkan kedua-dua sifat berombak gentian dan tegasan baki tegangan di dalam matriks. Kaedah prategasan serat dapat meningkatkan sifat-sifat mekanik komposit tenunan di kedua-dua arahpaksi dan arah nentang-paksi. Peningkatan ini masih wujud selepas pengedaran semula sepenuhnya tegasan baki yang diaruh dalam matriks.

ACKNOWLEDGEMENTS

All praises be to almighty Allah, the lord of whole creations, for inspiring and guiding me towards the utmost goodness

I also would like to express my sincere gratitude and appreciation to my supervisor Assoc. Prof. Dr. Nur Ismarrubie Zahari for her priceless guidance, continued supervision, advice, comment, encouragement and support throughout the research journey. Many thanks and gratitude also goes to the supervisory committee for their guidance and advice.

Also, I would like to express my utmost appreciation and gratitude to Universiti Putra Malaysia (GP–IPS/2015/9463000) for the financial support. The research was partially supported by Fundamental Research Grant Scheme (FRGS/1/2012/TKO1/UPM/02/1) by the Ministry of Higher Education Malaysia. Special thanks to Mr. Ahmad Shaifudin, Mr. Muhammad Wildan and Mr. Mohd Saiful for their technical supports

Finally, I would like to thank the University of Babylon, Ministry of Higher Education and Scientific Research, Iraq for the financial supporting of the scholarship.

Nawras Haidar Mostafa May 2017 I certify that a Thesis Examination Committee has met on 29 May 2017 to conduct the final examination of Nawras Haidar Mostafa Al-Said Haidar on his thesis entitled "Effect of Biaxial Fibre Prestressing on the Mechanical Properties of Plain-Weave E-Glass/Polyester Composites" in accordance with the Universities and University Colleges Act 1971 and the Constitution of the Universiti Putra Malaysia [P.U.(A) 106] 15 March 1998. The Committee recommends that the student be awarded the Doctor of Philosophy.

Members of the Thesis Examination Committee were as follows:

Nuraini binti Abdul Aziz, PhD

Associate Professor Faculty of Engineering Universiti Putra Malaysia (Chairman)

Barkawi bin Sahari, PhD

Professor Ir. Faculty of Engineering Universiti Putra Malaysia (Internal Examiner)

Edi Syams bin Zainudin, PhD

Associate Professor Faculty of Engineering Universiti Putra Malaysia (Internal Examiner)

Raj Das, PhD

Senior Lecturer University of Auckland New Zealand (External Examiner)

NOR AINI AB. SHUKOR, PhD Professor and Deputy Dean School of Graduate Studies Universiti Putra Malaysia

Date: 28 September 2017

This thesis was submitted to the Senate of the Universiti Putra Malaysia and has been accepted as fulfillment of the requirement for the degree of Doctor of Philosophy. The members of the Supervisory Committee were as follows:

Nur Ismarrubie Bt Zahari, PhD

Associate Professor Faculty of Engineering Universiti Putra Malaysia (Chairman)

Mohd Sapuan B. Salit, PhD Professor Ir Faculty of Engineering Universiti Putra Malaysia (Member)

Mohamed Thariq B. Hameed Sultan, PhD

Associate Professor Ir Faculty of Engineering Aerospace Manufacturing Research Centre (AMRC) Universiti Putra Malaysia (Member)

ROBIAH BINTI YUNUS, PhD Professor and Dean

School of Graduate Studies Universiti Putra Malaysia

Date:

Declaration by graduate student

I hereby confirm that:

- this thesis is my original work;
- quotations, illustrations and citations have been duly referenced;
- this thesis has not been submitted previously or concurrently for any other degree at any institutions;
- intellectual property from the thesis and copyright of thesis are fully-owned by Universiti Putra Malaysia, as according to the Universiti Putra Malaysia (Research) Rules 2012;
- written permission must be obtained from supervisor and the office of Deputy Vice-Chancellor (Research and innovation) before thesis is published (in the form of written, printed or in electronic form) including books, journals, modules, proceedings, popular writings, seminar papers, manuscripts, posters, reports, lecture notes, learning modules or any other materials as stated in the Universiti Putra Malaysia (Research) Rules 2012;
- there is no plagiarism or data falsification/fabrication in the thesis, and scholarly integrity is upheld as according to the Universiti Putra Malaysia (Graduate Studies) Rules 2003 (Revision 2012-2013) and the Universiti Putra Malaysia (Research) Rules 2012. The thesis has undergone plagiarism detection software

Signature:	Date:

Name and Matric No.: Nawras Haidar Mostafa, GS39714

Declaration by Members of Supervisory Committee

This is to confirm that:

- the research conducted and the writing of this thesis was under our supervision;
- supervision responsibilities as stated in the Universiti Putra Malaysia (Graduate Studies) Rules 2003 (Revision 2012-2013) were adhered to.

Signature: Name of Chairman of Supervisory Committee:	Associate Professor Dr. Nur Ismarrubie Bt Zahari
Signature: Name of Member of Supervisory Committee:	Professor Ir Dr. Mohd Sapuan B. Salit
Signature: Name of Member of Supervisory Committee:	Associate Professor Ir Dr. Mohamed Thariq B. Hameed Sultan

TABLE OF CONTENTS

Page

ABS ABS ACK APPI DEC LIST LIST LIST	FRACT FRAK NOWLEDGEMENTS ROVAL LARATION OF TABLES OF FIGURES OF ABBREVIATIONS	i iii v vi viii xiii xv xv xxv
CHAP	PTER	
1	 INTRODUCTION 1.1 General 1.2 Composite materials and their applications 1.3 Motivation 1.4 Problem statement 1.5 Scope and limitation of the study 1.6 Research hypotheses 1.7 Research objectives 1.8 Contributions of the study 1.9 Thesis layout 	1 1 3 3 5 5 6 6 7
2	 LITERATURE REVIEW 2.1 Introduction 2.2 Manufacturing of composites 2.3 Matrix micro-cracking damage in composite materials 2.4 Residual stresses in composite materials 2.4.1 Effects of residual stresses on composite failure 2.4.2 Measurement of residual stresses 2.4.3 Determination of residual stresses 2.5 Failure of composite materials 2.5.1 Matrix cracking 2.5.2 Interfacial debonding/intra-ply debonding 2.5.3 Fibre breakage 2.5.4 Failure criteria of a lamina 	8 8 9 11 11 14 16 18 20 21 22 22
	 2.6 Stress analysis of laminated composite 2.7 Types of fibre pretension (prestressing) methods 2.8 The proposed governing mechanisms associated with prestressing 2.9 Fibre pretension concepts 2.10 Application mechanisms of fibre prestressing methods 2.10.1 Elastically fibre prestressed PMCs (EFPPMCs) 2.10.2 Viscoelastically fibre prestressed PMCs (VEFPPMCs) 2.11 Mechanical behaviour of PMCs 	24 30 30 39 40 41 48 49

		2.11.1 Tensile behaviour	49
		2.11.2 Flexural behaviour	57
		2.11.3 Fatigue behaviour	64
		2.11.4 Longevity of fibre prestressed PMCs	74
	2.12	Overview of fibre prestressing studies	83
	2.13	Potential applications and future trends of fibre prestressed	83
		composites	
	2.14	Evaluation of fibre prestressing methodologies	85
	2.15	Summary	88
3	ME	THODOLOGY	90
	3.1	Introduction	90
	3.2	Research methodology	90
	3.3	Performing the fibre prestressing method	93
	3.4	Stresses analysis of PMCs	99
		3.4.1 Modelling based on the macro–mechanical level	99
		3.4.2 Modelling based on finite element method (FEM)	105
	3.5	Experimental tests	111
		3.5.1 Raw materials	112
		3.5.2 Prestressing frame	114
		3.5.3 Composite sample fabrication	118
		3.5.4 Tensile test	122
		3.5.5 Flexural test	125
		3.5.6 Fatigue test	128
		3.5.7 Evaluation of EFPPMCs with time (longevity	131
		2.5.8 Eailure morphology observation	122
	36	Summary	133
	5.0	Summary	155
	DEG		124
4	RES	ULTS AND DISCUSSION	134
	4.1	Introduction	134
	4.2	I neoretical analysis results	134
	4.5	Numerical results	145
	4.4	A 4.1 Properties of composite's constituent materials	155
		4.4.1 Froperties of composite's constituent materials	150
		4.4.2 Flexural test	100
		4.4.4 Eatique test	187
		4.4.5 Effect of stress relaxation on the longevity aspect	200
	4.5	Summary	200
5	CON	ICLUSIONS AND RECOMMENDATIONS FOR	204
5	FUT	URE STUDIES	204
	5.1	Theoretical analysis of prestressed composites	204
	5.2	Numerical modelling of prestressed composites	204
	5.3	Ouasi-static mechanical properties, fatigue behaviour and	205
		longevity	200
	5.4	Recommendations for future studies	206

xi

C

REFERENCES	207
APPENDICES	225
BIODATA OF STUDENT	265
LIST OF PUBLICATIONS	266



LIST OF TABLES

Table		Page
2.1	Techniques of residual stresses reduction in the polymeric composites	14
2.2	The average strain released using EFPI and FBG sensors with 108 MPa prestressed composite (Krishnamurthy et al., 2016)	16
2.3	Unstressed and prestressed unidirectional tensile properties (Brown, 1976)	32
2.4	Effect of fibre prestressing on the mean strength of a unidirectional carbon fibre/epoxy composite (Chi and Chou, 1983)	33
2.5	Mechanical properties (with standard deviations) of the pre- stressed and non-pre-stressed laminate (Schulte and Marissen, 1992)	50
2.6	Flexural modulus of nylon 6,6-epoxy composites (Pang and Fancey, 2009)	60
2.7	Prestressing methodologies and their limitations	86
2.8	The positive and negative aspects of the elastic and viscoelastic prestressing methods	87
2.9	The accomplished and pending tests related to prestressed PMCs	88
3.1	The standard properties of the E-glass woven fabric (EWR600)	112
3.2	Standard properties of the unsaturated polyester resin (Reversol P9509)	113
3.3	Approximated geometrical parameters of the plain-weave fabric lamina (E-glass/polyester) under different biaxial fabric prestressing levels	114
3.4	Number of tested samples for different tests	114
4.1	Residual stress in the matrix for a composite fabricated from a range of fibre volume fractions (unidirectional fibre) and prestressed at different levels using two theoretical models	135
4.2	Residual stress in the fibre for a composite fabricated from a range of fibre volume fractions (unidirectional fibre) and prestressed at different levels using two theoretical models	135

4.3	Thermomechanical properties of a composite system used by Krishnamurthy (2006)	136
4.4	Residual strain measurements versus current work results	136
4.5	Residual stresses within the matrix induced by fibre prestress only using Naik's (Naik and Ganesh, 1995) and Gay's (Gay, 2015) approaches	139
4.6	Tensile residual stresses in the fibre after matrix cure due to applying different biaxial fabric prestressing levels	141
4.7	Average tensile properties of the E-glass fibre and polyester resin	157
4.8	Tensile test results of composite sample batches at different initial fibre preloadings	162
4.9	Typical tensile test results for non-prestressed samples tested at different orientations with respect to the warp yarn	163
4.10	Comparison between theoretical and experimental results of the tensile elastic modulus of the plain-weave composite with different fibre orientation angles	169
4.11	Polynomial's coefficients of the tensile elastic modulus at different orientation angles and prestressing levels	172
4.12	Polynomial's coefficients of the tensile strength at different orientation angles and prestressing levels	172
4.13	Mean values of flexural properties for prestressed samples aligned at warp	178
4.14	Polynomial's coefficients of the flexural modulus at different orientation angles and prestressing levels	182
4.15	Polynomial's coefficients of the flexural strength at different orientation angles and prestressing levels	183
4.16	Tensile strength decay per decade for composite samples with different fibre orientations and prestressing levels	190
4.17	Polynomial's coefficients of the $S-N_f$ at different orientation angles	196
4.18	Summary of the Weibull's modulus of non-prestressed and prestressed composites samples	200

LIST OF FIGURES

Figure		Page
2.1	Weight gain curves for $[0/\pm 45/0]$ s composites conditioned in 50 °C distilled water (Li, 2000)	10
2.2	Tensile strength for ± 45 laminates at different testing temperatures, dry and wet (Li, 2000)	10
2.3	Defects caused by residual stresses (Stamatopoulos, 2011; Parlevliet et al., 2007b). (a) Fibre waviness, (b) matrix cracking, (c) interlaminar delamination, and (d) warpage	12
2.4	Cracked composites (Talreja, 2016). (a) Crack initiation along fibre–matrix interfaces, (b) crack spread between the interlaced yarns of woven composites	13
2.5	Induced residual strain in [0 ₂ /±45]s graphite/polyimide composite specimens (Daniel and Liber, 1977)	15
2.6	Failure mechanisms of unidirectional fibre-reinforced composites (Montesano, 2012). (a) Matrix cracking, (b) fibre fracture, and (c) fibre-matrix interface debonding	18
2.7	Schematic representation of damage development in plain- woven fabric composites during loading. (a) Quasi-static tensile damage (Naik, 2003) and (b) fatigue damage (on-axis) (Montesano, 2012)	20
2.8	Examples of matrix cracks observed in: (a) Continuous fibre cross-ply laminates (Katerelos et al., 2008) and (b) woven fabric polymer composite laminates (Rios-Soberanis et al., 2012; Talreja and Singh, 2012)	21
2.9	Intra-ply debonding occurring in woven fabric-reinforced composites (Naik et al., 2001)	22
2.10	Fibre breakage in fibre-reinforced composite (Lingang, 2013)	22
2.11	Principal directions of the unidirectional laminated composite material (Jones, 1999)	23
2.12	Geometrical parameters of a typical plain-weave fabric lamina unit cell and its idealisation according to Naik and Ganesh (1995). (a) Cross-section in fill direction, (b) cross-section in warp direction, and (c) idealised unit cell	28
2.13	Schematic representation of a fibre which undergoes bending Mills and Dauksys (1973)	31

 \bigcirc

2.14	Prestressing equipment used by Brown (1976)	32
2.15	A schematic view of fibre prestressing by bending as used by Chi and Chou (1983)	33
2.16	In-plane and out-of-plane fibre waviness examples (Potter et al., 2008)	34
2.17	Effect of residual stresses in composites failure by crack propagation: (a) Non-prestressed composite without external load, (b) non-prestressed composite with external load, and (c) fibre-prestressed composite with external load	35
2.18	Number of initial transverse cracks versus strain (Schulte and Marissen, 1992)	36
2.19	A scheme of fracture by impact in non-prestressed and prestressed samples: (a) Crack propagated through shearing the fibre, (b) Crack propagated along fibre/matrix interfacial region	37
2.20	Schematic diagram of the crack developing in the silica modified glass fibre-reinforced epoxy composite (Cao and Cameron, 2006b)	38
2.21	Schematic representation of mechanism–V (Pang and Fancey, 2009): (a) Effect of remaining tension force on the vertical force, and (b) neutral axis shifting due to the presence of the compressive residual stress within the matrix	39
2.22	The apparatus used by Zhigun (1968)	40
2.23	The rig used by Jorge et al. (1990) for fabricating the prestressed composite plates	41
2.24	The dead–weight prestressing rig used by: (a) Sadiq (2007), and (b) Schlichting et al. (2010)	42
2.25	The prestressing device with V-shaped slots used by Schulte and Marissen (1992)	43
2.26	The schematic representation of pressure forming moulds used by Bekampienė et al. (2011)	43
2.27	Schematic drawing of the pretensioning device used by Hadi and Ashton (1998)	44
2.28	Schematic drawing of the hydraulic cylinder–prestressing device used by Tuttle et al. (1996)	45
2.29	Schematic drawing of a horizontal tensiometer machine device used by Motahhari and Cameron (1999, 1998, 1997)	45

	2.30	The fibre-stretching frame used by Zhao and Cameron (1998)	46
,	2.31	The fibre–stretching frame used by Krishnamurthy (2006) and Daynes et al. (2010, 2008)	47
,	2.32	Fibre misalignment near end-tab region (Krishnamurthy, 2006)	47
	2.33	Biaxial fibre prestressing frame used by Jevons (2004)	48
	2.34	Effect of fibre prestress on the tensile properties of E-glass/polyester composite (Jorge et al., 1990): (a) Tensile strength, and (b) tensile elastic modulus	49
,	2.35	Stress-strain curves of aluminium alloy and VIRALL laminates with different levels of fibre prestress (Sui et al., 1995)	50
,	2.36	Tensile strength and modulus as a function of prestress (Zhao and Cameron, 1998)	51
	2.37	Variation of composite elastic modulus with fibre volume fraction at different fibre prestress levels (Hadi and Ashton, 1998)	52
2	2.38	Effect of fibre prestress on shape and position of initial damage envelopes for S-glass/epoxy laminate (Dvorak and Suvorov, 2000)	53
	2.39	Failure strain as a function of prestress (Krishnamurthy, 2006)	54
	2.40	The tensile curves of composite material reinforced with (Bekampiene et al., 2011): (a) Cotton, and (b) glass fabric	54
	2.41	Tensile stress-strain plots for a batch of test (prestressed) and control samples showing typical curve shape. Strain-limited toughness is determined from the shaded area under each curve (Pang and Fancey, 2008)	55
	2.42	Effect of fibre prestrain on the tensile properties of final composites (Zaidi et al., 2015). (a) Tensile strength, and (b) tensile elastic modulus	56
\bigcirc	2.43	Tensile properties of a carbon fibre/epoxy composite versus the prestressing level (Abdullah and Hassan, 2016): (a) Ultimate strength, and (b) tensile elastic modulus	57
	2.44	Flexural strength and modulus as a function of prestress (Zhao and Cameron, 1998)	58
2	2.45	Flexural properties versus prestressing level foe E-glass/epoxy composites (Motahhari and Cameron, 1999): (a) Flexural modulus, and (b) flexural strength	59

2.46	Flexural properties comparison of the unidirectional E–glass fibre/epoxy composite samples (Cao and Cameron, 2006a): (a) Flexural strength, and (b) flexural modulus	60
2.47	Flexural strength versus fibre pretension level (Širvaitienė et al., 2013b)	61
2.48	Flexural modulus values determined from the three-point bend tests. Each value represents the mean of three samples with corresponding standard error (Fazal and Fancey, 2013a)	62
2.49	Effect of prestressing on the flexural properties of final composites (Zaidi et al., 2015). (a) Flexural strength, and (b) flexural modulus	63
2.50	Flexural properties of a carbon fibre/epoxy composite versus the prestressing level (Abdullah and Hassan, 2016): (a) Flexural strength, and (b) flexural modulus	63
2.51	Comparison of the tension/tension fatigue results for composites consist of the glass fibre/different types of epoxy resins (Fernando and Al-khodairi, 2003): (a) Straight line fitting, and (b) quadratic fitting	64
2.52	Modulus decay and damage accumulation in woven fabric composites during fatigue life (Naik, 2003)	65
2.53	Fatigue life of woven fabric composites (Pandita et al., 2001)	66
2.54	The stress-cycles curves of composite sample at different orientations (Tamuzs et al., 2004)	67
2.55	Changes in the elastic modulus during a cyclic loading at 0° (Tamuzs et al., 2004)	68
2.56	Normalized S–N _f relationships at different temperatures (Kawai and Taniguchi, 2006). (a) Room temperature, and (b) 100 $^{\circ}$ C	69
2.57	Maximum stress-fatigue cycles relationships (Kawai and Matsuda, 2012)	70
2.58	S–N curves at symmetrical sinusoidal loading ($R = -1$) for three directions of specimens (Tamuzs et al., 2008)	71
2.59	Typical curve of reduction of modulus during the cyclic loading (Tamuzs et al., 2008)	71
2.60	Fatigue stress-life curves for a VIRALL laminate with various levels of prestraining (Sui et al., 1996)	72

2.61	Comparison of normalised fatigue of non-prestressed and prestressed composites (Krishnamurthy, 2006): (a) Tension- tension, and (b) tension-compression	74
2.62	Creep behaviour of polymers (Papanicolaou and Zaoutsos, 2011): (a) Application of constant stress, (b) strain response	75
2.63	Stress relaxation in polymers (Papanicolaou and Zaoutsos, 2011): (a) Application of constant strain, and (b) stress relaxation	75
2.64	Analysis of stress relaxation data of nylon 6,6 (Fancey, 2005)	77
2.65	Total compliance plotted as a function of creep time for carbon fibre/epoxy composite at a creep stress of 169.2 MPa measured at different temperatures (Raghavan and Meshii, 1997)	78
2.66	Experimental creep compliance of [0,90] ₆ plain weave carbon/epoxy composite at various temperatures and 450 MPa (Gupta and Raghavan, 2010)	79
2.67	Effect of fibre reinforcement on Epoxy adhesive (Miravalles, 2007)	80
2.68	Creep curves of the polyester and polymer matrix composites (holding peak stresses: for matrix, 35 MPa; composites 40% and 50%, 140 MPa) by Kang et al., (2009)	81
2.69	Comparison of experimental creep of plain weave carbon/epoxy composites under on-axis (0) loading and off-axis (45°) loading at a stress of 20% ultimate tensile strength and a temperature of 80 °C (Gupta and Raghavan, 2010)	82
2.70	Filament winding (Gay, 2015)	84
3.1	Flow chart of research methodology	92
3.2	Schematic representation of fibre prestressing during the manufacturing process and its effects on load-deflection behaviour	94
3.3	Axially loaded composite bar	96
3.4	Plain-weave fabric undergoes the prestressing process	98
3.5	Deformation in an orthotropic material	100
3.6	Rotation of principal fibre material axes from x-y axes	103
3.7	Representation of an elementary structure and typical mesh model of a UFRC	108

3.8	Effect of element number on the matrix residual stress at fibre- matrix interface with fibre prestress of 25 MPa.	108
3.9	Representation of an elementary structure and typical mesh model of a PWRC	109
3.10	Geometry of element type SOLID185	110
3.11	The plan-view of the biaxial fabric prestressing rig	115
3.12	The hydraulic system used in applying and measuring the fabric pretension	117
3.13	Accuracy of the pressure gauge-hydraulic system	118
3.14	Samples with different fibre orientation angles (on-axis and off-axis)	119
3.15	Interlacing angle in the plain-weave fabric	122
3.16	Specimen dimensions of tensile test according to ASTM D3039 (2014)	122
3.17	Specimen dimensions according to ASTM D638 (2004)	123
3.18	Setting the E-glass yarn	123
3.19	Tensile test machine, INSTRON 3382	124
3.20	Flexural test machine, INSTRON 3365	125
3.21	Specimen dimension of flexural test and its setting	127
3.22	Fatigue parameters of the load-time curve	128
3.23	Fatigue test machine, INSTRON 8874	130
3.24	KAPA Multistation testing machine	132
4.1	Longitudinal residual stresses within the matrix of a unidirectional composite cured at 50 °C and cooled down to 25 °C with different levels of fibre prestress	137
4.2	Transverse residual stresses within the matrix of a unidirectional composite cured at 50 °C and cooled down to 25 °C with different levels of fibre prestress	138
4.3	Longitudinal residual stresses (warp direction) within the matrix of a plain–weave composite cured at 50 °C and cooled down to 25 °C with different levels of equi–biaxial fabric prestress	140

	4.4	Transverse residual stresses (weft direction) within the matrix of a plain–weave composite cured at 50 °C and cooled down to 25 °C with different levels of equi–biaxial fabric prestress	140
	4.5	Total axial stress versus applied external axial stress in the composite lamina (E-glass/Polyester) cured at 50 °C and cooled down to 25 °C and prestressed with different levels	141
	4.6	Total flexural stress versus applied flexural stress in the composite lamina (E-glass/Polyester) cured at 50 °C and cooled-down to 25 °C and prestressed with different levels	142
	4.7	Applied maximum fatigue stress versus fatigue cycles to failure in the composite lamina (E-glass/Polyester) cured at 50 °C and cooled down to 25 °C and prestressed with different levels	143
	4.8	Effect of the fibre elastic modulus on the induced residual stresses in the composite's constituents in the fibre with prestressing level equals to 25 MPa	144
	4.9	Effect of the matrix elastic modulus on the induced residual stresses in the composite's constituents in the matrix with prestressing level equals to 25 MPa	145
	4.10	Axial stress distribution within the matrix due to applying different fibre prestressing levels. (a) 25 MPa, (b) 50 MPa, (c) 75 MPa, and (d) 100 MPa	147
	4.11	Axial stress distribution in the matrix along its radial direction due to applying different fibre prestressing levels	147
	4.12	Shear stress distribution in the unidirectional composite due to applying different fibre prestressing levels. (a) 25 MPa, (b) 50 MPa, (c) 75 MPa, and (d) 100 MPa	148
	4.13	Shear stress distribution in the matrix along its radial direction due to applying different fibre prestressing levels	149
	4.14	Axial stress distribution within the matrix due to applying different equi–biaxial fabric prestressing levels at 25 °C. (a) 25 MPa, (b) 50 MPa, (c) 75 MPa, and (d) 100 MPa	150
	4.15	Compressive residual distribution within the matrix due to applying different equi-biaxial fabric prestressing levels at 25 $^{\circ}\mathrm{C}$	151
	4.16	Comparison between analytical and numerical (FEM) results of induced residual stresses within the matrix of equi–biaxial prestressed plain–weave composites at 25 °C	152

xxi

	4.17	Axial stress at the outer surface of the matrix due to applying axial or transverse loads with different fibre prestress levels	153
	4.18	Maximum bending stress distribution of the tensioned part of the matrix under transverse loading of 30 N	154
	4.19	Maximum bending stress distribution of the non-prestressed and prestressed samples; the applied transverse load is equal to 30 N	155
	4.20	Tensile stress-strain curves of the composite's constituents used in this work. (a) E–glass fibre, and (b) polyester resin	157
	4.21	Normalised stress vs logarithmic fatigue cycles $(S-N_f)$ of the composite's constituent materials. The arrowheads indicated that these samples survived for one million cycles.	158
	4.22	Creep compliance versus time history of the E–glass fibre at a constant applied stress of 100 MPa	159
	4.23	Stress versus time history of the polyester resin at a constant applied strain of 0.078%	159
	4.24	Prediction of the stress redistribution of polyester resin using Fancey's model (Fancey, 2005)	160
	4.25	Samples with different fibre prestressing conditions. (a) Unloaded fabric (uncontrolled), (b) uniaxially loaded (weft), and (c) equi-biaxially loaded	162
	4.26	Typical tensile stress-strain curves for composite samples tested at different fibre orientations. (a) Non-prestressed samples, and (b) prestressed samples with 50 MPa	164
	4.27	Specimens fractured in quasi-static tension. (a) Warp direction (0°) , (b) 15° with respect to warp, (c) 30° with respect to warp, and (d) bias direction (45°)	165
	4.28	Micrographs of the failure types for prestressed specimens subjected to tensile load. (a) Matrix cracking, (b) fibre-matrix debonding	166
	4.29	Quasi-static tensile properties of composite samples with different levels of equi-biaxial fabric prestressing tested at different fibre orientations. (a) Tensile elastic modulus, and (b) ultimate tensile strength	168
	4.30	Tensile properties changing with fabric prestressing level at different orientation angles. (a) Tensile elastic modulus, and (b) critical stress	170

	4.31	Comparison between the predicted empirical equations and the experimental data. (a) Tensile modulus, and (b) tensile strength.	173
	4.32	Frictional parameter versus fibre prestressing level	174
	4.33	Effect of biaxial fabric prestress on the percentage crimp along the warp and weft yarns	175
	4.34	Micrographs of fabric within the composite. (a) Without fabric prestressing, and (b) with fabric prestressing (50 MPa)	175
	4.35	Limited toughness changing with fabric prestressing level at different orientation angles	176
	4.36	In-plane shearing of the composite caused by inclined yarn (off-axis)	177
	4.37	Typical load-deflection curves of composite samples with different levels of fabric prestressing	178
	4.38	The details of the mechanisms that attribute to the enhancement in flexural properties of equi–biaxial fabric prestressing composites. (a) Improving the straightness of yarns, and (b) increasing the contact pressure and reducing crimping	179
	4.39	Flexural properties changing with fabric prestressing level at different orientation angles. (a) Flexural modulus, and (b) flexural strength	181
	4.40	Comparison between the predicted empirical equations and the experimental data. (a) Flexural modulus, and (b) Flexural strength.	184
	4.41	The directions of bending and compressive residual stresses	185
	4.42	Failure pattern images of specimens subjected to three-point bending test	186
	4.43	Normalised stress vs logarithmic fatigue cycles $(S-N_f)$ of composite samples with different levels of equi–biaxial fabric prestressing tested at different fibre orientations. (a) At 0°, (b) at 15°, (c) at 30°, and (d) at 45°	189
	4.44	Non-prestressed and prestressed specimens failed at different normalised peak stresses	192
	4.45	Normalised stiffness evolution at 0.55 of normalised peak stress	193
	4.46	The map of adopting the fabric–prestressing method to improve fatigue life or vice versa	194

4.47	Comparison between the predicted empirical equations and the experimental data of normalised stress vs fatigue cycles to failure $(S-N_f)$ at different fibre orientations. (a) 0°, (b) 15°, (c) 30°, and (d) 45°.	198
4.48	Weibull's distribution for fatigue life of the 50 MPa prestressed samples at different normalised peak stress tested at on-axis	199
4.49	Effect of longevity on the quasi–static properties of prestressed samples. (a) Critical stress, (b) flexural strength	201
4.50	Effect of longevity on the fatigue life of prestressed samples at 50 MPa (<i>S</i> =0.55)	202
A-1	Biaxial prestressing frame and its dimensions	225
A-2	Details of the mould used in this work (symmetrical part)	226
B-1	Composite bar's dimensions (axisymmetric)	227
B-2	Axial stress distribution in the matrix with different fibre prestressing levels. (a) Non–prestressed, (b) prestressed with 25 MPa, (c) prestressed with 50 MPa, (d) prestressed with 75 MPa, and (e) prestressed with 100 MPa	230
C-1	A composite beam's geometry and loading details	231
C-2	Flexural stress distribution for selected elements around the mid-span of the composite beam with different fibre prestressing levels. (a) Non-prestressed, (b) prestressed with 25 MPa, (c) prestressed with 50 MPa, (d) prestressed with 75 MPa, and (e) prestressed with 100 MPa	236

C

LIST OF ABBRIVATIONS

PMCs	Polymeric Matrix Composites
EFPPMCs	Elastically Fibre Prestressed PMCs
VEFPPMCs	Viscoelastically Fibre Prestressed PMCs
FEM	Finite Element Method
ANSYS	Analysis System
МЕКР	Methyl Ethyl Ketone Peroxide
UNC	Unified Coarse
E-glass	Electrical-grade glass
EWR600	E-glass woven roving with area density of 600 g/m ²
UFRC	Unidirectional Fibre–Reinforced Composite
PWRC	Plain-Weave Fabric Reinforced Composite
ASTM	American Society for Testing and Materials
EFPI	Extrinsic Fabry-Pérot Interferometric
FBG	Fibre Bragg Grating
ERSG	Electrical Resistance Strain Gauge

CHAPTER 1

INTRODUCTION

This study investigates the effect of elastic fibre prestress on the performance of fibre– reinforced composites subjected to (i) a quasi–static load (tensile and flexural) and (ii) a fatigue load. The endurance aspect of the prestressed composites is examined over different periods of time. The present study includes theoretical, numerical and experimental investigations. The fibre pretension method has been used mainly to minimise the induced tensile residual stress and fibre waviness within composites.

This chapter highlights the problem statement, motivation, research hypotheses, main objectives and contributions to knowledge. A brief introduction to composite materials and their applications, along with the thesis layout are also presented.

1.1 General

The development of composite materials has been fast growing in recent times due to their influence on human life, whether civilian or military. The mechanical behaviour of the final composite product depends mainly on the mechanical properties of constituent materials, their fractional volume, their arrangement, and the manufacturing technology. Unfortunately, designing and manufacturing of a composite part with an improved mechanical behaviour are usually accompanied by relatively high–cost requirements. Low-cost-design is a very critical parameter that should be considered by designers in developing the behaviour of composite materials. One method that can be used to improve the structural properties of fibre– reinforced composites is the method of fibre prestressing.

The effect of equi-biaxial fabric prestressing on the quasi-static (tensile and flexural), fatigue and creep behaviours of a plain-weave fabric-reinforced composite has been considered in this study. This chapter briefly introduces the applications of composite materials, the problem statement, the scope of the work, the aims of the study, the contributions of the present study and finally the organisation of the thesis.

1.2 Composite materials and their applications

Modern structures that are made from fibre–reinforced based polymer composites have many advantages over the structures that are made from conventional materials such as high strength and stiffness–to–weight ratios, the ability to form complex shapes, high corrosion resistance, durability and low cost of maintenance in comparison with most metals (Andersson et al., 2014; Khan et al., 2014). However, the production cost of composites is relatively more expensive than common metals (Ashby and Jones, 2012; Lässig et al., 2012).

A composite material is simply defined as a combination of two or more materials, on a macroscopic scale, with significantly different properties to form a useful third material (Jones, 1999). The basic constituents of a composite consist of two phases, i.e. the reinforcement and the matrix. The essential role of the reinforcement is to absorb the traction force; however, the matrix has the role of transferring the load to the reinforcement phase, protecting the reinforcement phase from the environment, maintaining the cohesion of the component, providing the lateral support and resisting the shear and compression forces and to provide stable shape (Vigo and Kinzig, 1992). The usual reinforcing fibres used today are carbon, glass, boron, and aramid. While epoxy, polyester, and vinyl–ester are the most common resins used in the fabrication of the polymer composites (Murray et al., 2007).

Over the few last decades, composite structures have become popular in many applications where there is exposure to different external loadings and different environmental conditions. They are used instead of various conventional metallic materials for their relatively good chemical, physical and mechanical properties. Composite materials are widely used in many applications such as the aircraft, automotive components, military components, renewable energy, marine and offshore structures, and medical devices (Thomas et al., 2012). Components that are made from composite materials in aircraft structures can save the weight by up to a half in comparison with conventional metals (Greszczuk, 1975). The automotive industry has followed this with the successful use of composites in the production of the light and stiff components (Sapuan et al., 1995). Recently, the requirements for safer, faster cars have been achieved using the advanced technologies of composite materials (Thomas et al., 2012).

Generally, there are four common types of composite materials (Jones, 1999):

- Fibrous composites: this type consists of fibres (long or short) embedded in a matrix.
- Laminated composites: this type consists of different layers of materials.
- Particulate composites: this type is composed of particles in a matrix.
- Combinations of some or all of the above three types.

Fibrous composites with long fibres is used in this study as a reinforcement phase.

1.3 Motivation

Improving the composite's structural behaviour under quasi-static and/or cyclic loading, while keeping its mass and volume as low as possible, is one of the most significant challenges that designers might face. Fibre prestressing method can offer such improvement in the structural behaviour of the unidirectional composites. Because composites reinforced by plain-weave fabrics are widely used in most composite structures, the biaxial fabric prestressing method is intended to be investigated in order to see if this method can be exploited using such reinforcement form.

1.4 Problem statement

It is widely agreed that the use of composite structures is increasing, leading to an increased demand for the development of new techniques that can improve the mechanical behaviour of such advanced materials. In spite of the superior mechanical properties of the currently available composites compared with conventional metallic materials, research on their improvement is still ongoing. Moreover, the cost of producing composites that are more reliable is continuing to rise because they need either additive materials and/or improved fabrication techniques. Residual stresses are generated within the composites during manufacturing process (Shokrieh, 2014; Parlevliet et al., 2007b; Motahhari, 1998). These residual stresses can develop in composite materials due to several reasons such as the chemical shrinkage of the polymer matrix, the different thermomechanical properties of the constitutions, moisture absorption, and fibre pretension (Krishnamurthy, 2006). Residual stresses within the matrix can arise due to the phase change of the resin from liquid to solid state (chemical shrinkage). The mismatch in the coefficient of thermal expansion between the fibre and the matrix will produce residual stresses in the composite when it is cooled from its curing temperature (Shokrieh, 2014; Cao and Cameron, 2007; Krishnamurthy, 2006; Motahhari and Cameron, 1999; Motahhari, 1998; Fletcher and Oakeshott, 1994a, 1994b). Whereas moisture absorption by the polymeric matrix and the fibre leads to the deformation and expansion of the constituents of the composite at different levels depending on the swelling permeability (Li, 2000; Motahhari, 1998). Manufacturing processes such as the filament winding fabrication technique can add another source of induced residual stress in the final composite product due to the stretching of the fibre during the fabrication processes (Tabuchi et al., 2012; Mertiny and Ellyin, 2002; Binienda and Wang, 1999; Gabrys and Bakis, 1998; Cohen, 1997; Knight, 1972).

Residual stresses produced by resin chemical shrinkage and a mismatch in thermal expansion between the fibre and the matrix have a negative effect on the final mechanical properties of composites as their nature are always tensile (Krishnamurthy, 2006; Motahhari, 1998; Motahhari and Cameron, 1997). However, moisture absorption by the matrix generally acts to oppose the negative effects of both the chemical shrinkage and the thermal strains developed in the composites, but at the same time it may attack the fibre in a critical way (Li, 2000; Motahhari, 1998).

Fibre pretension could be one of the available options for enhancing the properties of polymeric matrix composites (PMCs) without increasing their section dimensions or mass (Graczykowski et al., 2016; Fancey, 2010). Up to now, the improvement obtained in the mechanical properties of fibre–reinforced composites due to using the fibre–prestressing method is not well established. However, some researchers have effectively confirmed the advantages of fibre prestressed composites for unidirectional composites. Prestressed PMCs were first used by Zhigun (1968) and this was followed by other researchers, such as Manders and Chou (1983) and Tuttle (1988).

Fibre pretension (prestressing) during matrix cure has in general a positive effect on the composite mechanical behaviour as it generates compressive residual stresses in the matrix. It is important to mention that fibre pretension has this beneficial effect only if it is applied to a limited level or range (Krishnamurthy, 2006; Jevons, 2004; Motahhari and Cameron, 1999; Motahhari, 1998). In particular, the existence of tensile residual stresses in composites can reduce the resistance to matrix micro– cracking. The presence of undesirable residual stresses and the waviness of the fibre may have a detrimental effect on the mechanical properties of composite structures and this may decrease the service life of a composite structure (Parlevliet et al., 2007a). Therefore, it is of importance to minimise the magnitude of the unfavourable residual stresses and the waviness of the fibre. It was previously proven that fibre pretension in simple laminates (unidirectional fibre) during curing process can generate compressive stresses in the matrix and thus help to support damage initiation and propagation (Krishnamurthy, 2006; Motahhari, 1998).

In case of using 2D woven fabrics as a reinforcement, the effect of fibre pretension on the mechanical properties of the composites is more complicated than those fabricated with unidirectional fibres. As the yarns of 2D woven fabric are crimped and interlaced between each other, pretensioning these yarns may affect the structural behaviour of composites in different kind. The main problems associated without having the fabric prestressing to plain–weave composite are directly related to fibre defects such as fibre waviness, wrinkling and high crimping. On the other hand, tensile residual stresses are induced during the fabrication process within the matrix at both the warp and fill yarn directions. The presence of tensile residual stresses within the matrix of the composite and fibre waviness have negative effects on the structural behaviour of the plain–weave composites.

 \bigcirc

The method of fibre pretension had confirmed its positive effects regarding the structural behaviour of the unidirectional fibre–reinforced composites under quasistatic and fatigue loadings (Sadiq, 2007; Krishnamurthy, 2006; Cao and Cameron, 2006a; Hadi and Ashton, 1998). However, from the author's knowledge this method is not assessed yet for a composite reinforced with a biaxially prestressed plain– weave fabric under these loadings. Therefore, investigating the effect of biaxial fibre pretension during the matrix cure process theoretically, numerically and experimentally on the behaviour of a composite reinforced by a plain–weave fabric needs to be considered.

1.5 Scope and limitation of the study

This work deals with the study of the quasi-static (tensile and flexural), fatigue and endurance aspect of the elastically prestressed composite behaviour fabricated from a plain-weave E-glass fabric (EWR600)/unsaturated polyester (Reversol P9509) system. The presence of the induced tensile residual stresses within the matrix has a detrimental effect on the mechanical properties of the composite; therefore, the tensile residual stresses within the matrix should be reduced, released or if possible reversed to compressive stresses. Therefore, prestressed composite samples are fabricated with different fibre pretension levels applied in biaxial directions (warp and weft yarn directions). The fibre prestress levels are within the linear elastic limit of the fibre materials. Specimens are then tested under quasi-static (tensile and flexural) and fatigue loadings at different orientation angles of the fabric (0, 15, 30 and 45°). Theoretical analyses of the fibre pretension method for both unidirectional and bidirectional composite lamina are achieved. A numerical modelling and analysis of prestressed composites is performed to validate the theoretical analyses and to estimate the distribution and development of residual stresses within the composite's constituents. Reducing the tensile residual stresses within the matrix can improve the composite strength by preventing the cracks to develop easily. Several factors that can directly affect the tensile residual stress magnitude within the matrix are studied such as the elastic moduli of composite's constituents and fibre pretension level. The prospective practical applications of unidirectional fibre prestressed composites include filament winding to fabricate pressure pipes, vessels, wind turbine blades and cylindrical shells. However, fibre pretension can be performed for composites reinforced with 2D woven fabric such as helmets, armours, boats, bistable morphing structures, and automotive industry. The current study is limited to using composite samples fabricated with only a single layer of fabric at ambient conditions.

1.6 Research hypotheses

This research is carried out with three main hypotheses. They are as follows:

- 1. Fibre prestressing during the matrix cure process can change the state of the internal residual stresses of the fibre–reinforced composites. Upon releasing the fibre pretension, compressive residual stresses are imparted from the pretensioned fibres into the matrix. Therefore, it is expected that the new state of residual stresses within the matrix could prevent the initiation and development of micro–cracks.
- 2. The presence of the fibre pretension can increase its straightness. Thereby, it can provide the instantaneous load transfer from the matrix to the fibre. The architecture of the reinforced phase can improve significantly when pretensioned. Fibre waviness and crimping are decreased significantly, thereby leading to the enhancement of the structural behaviour of the composite as a whole.

3. Prestress have a significant effect on the total flexural stiffness of the composite structure. The remaining tension force in the fibre after releasing the pretension load in the fibre can reduce the deflection of the prestressed composite when subjected to transverse and/or bending load.

1.7 Research objectives

The objectives of this study are:

- 1. To develop material model for the fibre prestressed composites theoretically by deriving new equations and developing the macro-mechanical analysis of a laminated composite to include the term of biaxial fabric prestressing in the modelling of plain-weave composites.
- 2. To develop the model for the fibre prestressing method numerically using a commercial finite element software on the meso-scale in order to explore how fibre prestressing affects the state of internal stresses within the composite's constituents and verify the numerical results with those obtained from the developed theoretical equations.
- 3. To investigate the effect of applying different levels of biaxial fabric prestressing on the quasi-static (tensile and flexural) properties and fatigue behaviour of plain-weave composites tested at different fibre orientation angles. The same tests are performed at different timescales in order to include the effect of residual stress relaxation within the polymeric matrix on the mechanical behaviour of fibre prestressed composites.

1.8 Contributions of the study

The contributions of this study are:

- 1. Focusing on the prediction of the quasi-static, fatigue life and stress relaxation behaviour of such improved composite materials. Thereby, giving a good indication of the behaviour of the prestressed composite under the different loading conditions that it may be exposed to in practical applications.
- 2. The mechanical properties are improved without adding new material to the composite's constituent and neither increasing the volume nor the mass of the composite when employing the fibre pretension method. This could reduce the overall cost of composite production.
- 3. In most practical applications, composite structures are subjected to multidirectional or complex loadings that require improvements in the mechanical properties of the composite structures in each direction. The equi-biaxial fabric pretension method of a plain-weave fabric could offer this advantage efficiently.

1.9 Thesis layout

This study has been broken down into five chapters.

Chapter 1 presents a short background of the composite materials applications, the research motivation, the problem statement, the scope of the study, the hypotheses and objectives of the research, the contributions of the study and the layout of this thesis.

Chapter 2 presents a literature review on residual stresses accompanied with composite material manufacturing and their effects on the mechanical behaviour of the composite products. The failure modes in the polymeric matrix composite are reviewed briefly. This is followed by the description of mechanisms related to the fibre pretension method. The types of fibre prestressing methods and the associated application techniques are also reviewed in this chapter. The effects of the fibre pretension method on the structural behaviours of the composite under tensile, flexural and fatigue loading are reported. The final part discusses the assessment of the prestressing methodologies and their potential applications.

Chapter 3 presents the methodology used in the current study. The research methodology is explained and the prestressing philosophy has been described. This is followed by the derivation of new theoretical equations and development of the macro-mechanical theory to calculate and include the effect of the residual stresses induced in the composite due to prestressing the fibre before and during the matrix cure process. The finite element method is used to model the fibre prestressing method numerically and to validate the theoretical analysis results. The final section explains the experimental part such as raw material selection and manufacturing a suitable prestressing frame. Experimental tests such as tensile, flexural, fatigue, stress relaxation, percentage crimping and endurance aspect of the plain-weave E-glass fabric/polyester composites are described in detail.

Chapter 4 presents and discusses the results obtained using the theoretical, numerical and experimental procedures.

Chapter 5 provides the overall conclusions obtained in this study are given and directions for future research studies are presented.

REFERENCES

- Abdullah, O. A., & Hassan, A. K. F. (2016). Effect of prestress level on the strength of CFRP composite laminate. Journal of Mechanical Science and Technology, 30(11), 5115–5123.
- Advani, S., and Hsiao, K.-T. (2012). *Manufacturing techniques for polymer matrix composites (PMCs)* (First). 80 High Street, Sawston, Cambridge CB22 3HJ, UK: Woodhead Publishing Limited.
- Alcoutlabi, M., Mckenna, G. B., and Simon, S. L. (2003). Analysis of the development of isotropic residual stresses in a bismaleimide/spiro orthocarbonate thermosetting resin for composite materials. *Journal of Applied Polymer Science*, 88, 227–224.
- Andersson, F., Hagqvist, A., Sundin, E., and Björkman, M. (2014). Design for manufacturing of composite structures for commercial aircraft – the development of a DFM strategy at SAAB aerostructures. In Proceedia CIRP, Variety Management in Manufacturing - Proceedings of the 47th CIRP Conference on Manufacturing Systems (Vol. 17, pp. 362–367). Elsevier B.V.
- Ashby, M. F., and Jones, D. R. H. (2012). Engineering Materials 1: An Introduction to Properties, Applications, and Design. Engineering Materials 1 (Fourth edi). The Boulevard, Langford Lane, Kidlington, Oxford: Elsevier.
- ASTM D3039 / D3039M 14. Standard Test Method for Tensile Properties of Polymer Matrix Composite Materials. (2014). Retrieved from http://www.astm.org/Standards/D3039.htm
- ASTM D3479 / D3479M-12, Standard Test Method for Tension-Tension Fatigue of Polymer Matrix Composite Materials. (2012). Retrieved from http://www.astm.org/Standards/D3479.htm
- ASTM D790 10 Standard Test Methods for Flexural Properties of Unreinforced and Reinforced Plastics and Electrical Insulating Materials. (2014). Retrieved from http://www.astm.org/Standards/D790.htm
- ASTM D2990 Standard Test Methods for Tensile, Compressive, and Flexural Creep and Creep-Rupture of Plastics. (2017). Retrieved from https://www.astm.org/Standards/D2990.htm
- ASTMS D638 Standard Test Method for Tensile Properties of Plastics. (2004). Retrieved from https://www.astm.org/Standards/D638.htm
- Batra, S. (2009). Creep Rupture and Life Prediction of Polymer Composites. Master Thesis, Department of Chemical Engineering Morgantown, West Virginia, USA.

- Bekampienė, P., Domskienė, J., and Širvaitienė, A. (2011). The effect of pre-tension on deformation behaviour of natural fabric reinforced composite. *Materials Science (Medziagotyra)*, 17(1), 56–61.
- Binienda, W. K., and Wang, Y. (1999). Residual stresses reduction in filament wound composite tubes. *Journal of Reinforced Plastics and Composites*, 18(8), 684–701.
- Bott, T. R., and Barker, A. J. (1967). Creep in glass fiber reinforced plastics. Industrial and Engineering Chemistry, 59(7), 46–51.
- Brown, G. (1976). *Development of prestressed graphite processing techniques*. USA: Space Division, North American Rockwell.
- Cao, Y., and Cameron, J. (2006a). Flexural and shear properties of silica particle modified glass fiber reinforced epoxy composite. *Journal of Reinforced Plastics and Composites*, 25(4), 347–359.
- Cao, Y., and Cameron, J. (2006b). Impact Properties of silica particle modified glass fiber reinforced epoxy composite. *Journal of Reinforced Plastics and Composites*, 25(7), 761–769.
- Cao, Y., and Cameron, J. (2007). The effect of curing conditions on the properties of silica modified glass fiber reinforced epoxy composite. *Journal of Reinforced Plastics and Composites*, 26(1), 41–50.
- Cheng, W., and Finnie, I. (2007). Residual stress measurement and the slitting method. New York, NY 10013, USA: Springer Science+Business Media, LLC.
- Chi, Z., and Chou, T. (1983). An experimental study of the effect of prestressed loose carbon strands on composite strength. *Journal of Composite Materials*, 17(3), 196–209.
- Cohen, D. (1997). Influence of filament winding parameters on composite vessel quality and strength. *Composites Part A: Applied Science and Manufacturing*, 28(12), 1035–1047.
- Cui, H. X., Guan, M. J., Zhu, Y. X., and Zhang, Z. Z. (2012). The flexural characteristics of prestressed bamboo slivers reinforced parallel strand lumber (PSL). *Key Engineering Materials*, 517, 96–100.
- Daniel, I. M., and Liber, T. (1977). Effect of laminate construction on residual stresses in graphite/polyimide composites. Experimental Mechanics, 17(1), 21–25.
- Daniel, I. M., and Charewicz, A. (1986). Fatigue damage mechanisms and residual properties of graphite/epoxy laminates. *Engineering Fracture Mechanics*, 25(5–6), 793–808.

- Das, S., Jagan, S., Shaw, A., and Pal, A. (2015). Determination of inter-yarn friction and its effect on ballistic response of para-aramid woven fabric under low velocity impact. *Composite Structures*, *120*, 129–140.
- Davis, D. C., Wilkerson, J. W., Zhu, J., and Hadjiev, V. G. (2011). A strategy for improving mechanical properties of a fiber reinforced epoxy composite using functionalized carbon nanotubes. *Composites Science and Technology*, 71(8), 1089–1097.
- Daynes, S., Diaconu, C. G., Potter, K. D., and Weaver, P. M. (2010). Bistable prestressed symmetric laminates. *Journal of Composite Materials*, 44(9), 1119–1137.
- Daynes, S., Potter, K. D., and Weaver, P. M. (2008). Bistable prestressed buckled laminates. *Composites Science and Technology*, 68(15–16), 3431–3437.
- Deve, H. E., and Maloney, M. J. (1991). On the toughening of intermetallics with ductile fibers: Role of interfaces. *Acta Metallurgica et Materialia*, 39(10), 2275–2284.
- Dixit, A., Mali, H. S., and Misra, R. K. (2014). A micromechanical unit cell model of 2 × 2 twill woven fabric textile composite for multi scale analysis. *Journal* of The Institution of Engineers (India): Series E, 95(1), 1–9.
- Dobreva, A., Gutzow, I., & Schmelzer, J. (1997). Stress and time dependence of relaxation and the Kohlrausch stretched exponent formula. Journal of Non-Crystalline Solids, 209(3), 257–263.
- Dvorak, G. J., and Prochazka, P. (1996). Thick-walled composite cylinders with optimal fiber prestress. *Composites Part B: Engineering*, 27(6), 643–649.
- Dvorak, G. J., Prochazka, P., and Srinivas, M. V. (1999). Design and fabrication of submerged cylindrical laminates–I. *International Journal of Solids and Structures*, 36(26), 3917–3943.
- Dvorak, G. J., and Suvorov, A. P. (2000). The effect of fiber pre-stress on residual stresses and the onset of damage in symmetric laminates. *Composites Science and Technology*, *60*(8), 1129–1139.
- E739-10, Standard Practice for Statistical Analysis of Linear or Linearized Stress-Life and Strain-Life Fatigue Data. (2012). Annual Book of ASTM Standards (Vol. i).
- Fancey, K. S. (2000a). Investigation into the feasibility of viscoelastically generated pre-stress in polymeric matrix composites. *Materials Science and Engineering: A*, 279(1–2), 36–41.

- Fancey, K. S. (2000b). Prestressed polymeric composites produced by viscoelastically strained nylon 6,6 fibre reinforcement. *Journal of Reinforced Plastics and Composites*, 19(15), 1251–1266.
- Fancey, K. S. (2005). A mechanical model for creep, recovery and stress relaxation in polymeric materials. *Journal of Materials Science*, 40(18), 4827–4831.
- Fancey, K. S. (2010). Viscoelastically prestressed polymeric matrix composites -Potential for useful life and impact protection. *Composites Part B: Engineering*, 41(6), 454–461.
- Fancey, K. S. (2015a). Prestressed Polymeric Composites: An Alternative Approach. In et al. A.L. Araújo, J.R. Correia, C.M. Mota Soares (Ed.), 10th International Conference on Composite Science and Technology, ICCST/10. Lisbon, Portugal.
- Fancey, K. S. (2015b). Prestressed polymeric composites: An alternative approach. In A. L. Araújo, J. R. Correia, and C. M. Mota Soares (Eds.), 10th International Conference on Composite Science and Technology, ICCST/10 (pp. 1–12).
- Fancey, K. S., and Fazal, A. (2016). Prestressed polymeric matrix composites: Longevity aspects. *Polymer Composites*, 37(7), 2092-2097.
- Fancey, K. S. (2016). Viscoelastically prestressed polymeric matrix composites: An overview. Journal of Reinforced Plastics and Composites, 35(17), 1290–1301.
- Fazal, A., and Fancey, K. S. (2013a). Viscoelastically generated prestress from ultrahigh molecular weight polyethylene fibres. *Journal of Materials Science*, 48(16), 5559–5570.
- Fazal, A., and Fancey, K. S. (2013b). Viscoelastically prestressed polymeric matrix composites Effects of test span and fibre volume fraction on Charpy impact characteristics. *Composites Part B: Engineering*, *44*(1), 472–479.
- Fazal, A., and Fancey, K. S. (2014a). Performance enhancement of nylon/kevlar fiber composites through viscoelastically generated pre-stress. *Polymer Composites*, *35*(5), 931–938.
- Fazal, A., and Fancey, K. S. (2014b). UHMWPE fibre-based composites: Prestressinduced enhancement of impact properties. *Composites Part B: Engineering*, *66*, 1–6.
- Fernando, G. F., and Al-khodairi, A. A. (2003). The fatigue of hybrid composites. InB. Harris (Ed.), Fatigue in Composites (First, pp. 189–238). Cambridge, UK:Woodhead Publishing Ltd and CRC Press LLC.

- Fletcher, A. J., and Oakeshott, J. L. (1994a). Thermal residual microstress generation during the processing of unidirectional carbon fibre/epoxy resin composites: random fibre arrays. *Composites*, 25(8), 806–813.
- Fletcher, A. J., and Oakeshott, J. L. (1994b). Thermal residual microstress generation during the processing of unidirectional carbon fibre/epoxy resin composites: regular fibre arrays. *Composites*, 25(8), 797–805.
- Fu, J., Liu, W., Liu, X., Tuladhar, S. L., Wan, Q., and Wang, H. (2014). Properties of a new dental photocurable resin based on the expanding monomer and three-component photoinitiator system. *Journal of Wuhan University of Technology-Mater. Sci. Ed.*, 29(2), 384–390.
- Gabrys, C. W., and Bakis, C. E. (1998). Simplified Analysis of Residual Stresses in In-Situ Cured Hoop-Wound Rings. *Journal of Composite Materials*, 32(13), 1325–1343.
- Gamstedt, E. K., and Sjögren, B. (1999). Micromechanisms in tension-compression fatigue of composite laminates containing transverse plies. Composites Science and Technology, 59(2), 167–178.
- Gay, D. (2015). *Composite Materials: Design and Applications* (Third). 6000 Broken Sound Parkway NW, Suit 300, Boca Raton, FL, USA: CRC Press (Taylor and Francis Group, LLC).
- Ge, C., Wang, B., and Fancey, K. S. (2015). Techniques to investigate viscoelastically generated prestress in polymeric composites. In A. L. Araújo, J. R. Correia, and C. M. Mota Soares (Eds.), 10th International Conference on Composite Science and Technology, ICCST/10 (pp. 1–11). Lisbon, Portugal.
- Giancane, S., Panella, F. W., and Dattoma, V. (2010). Characterization of fatigue damage in long fiber epoxy composite laminates. *International Journal of Fatigue*, 32(1), 46–53.
- Gibson, R. F. (2012). *Principles of Composite Material Mechanics* (Third edit). 6000 Broken Sound Parkway NW, Suite 300 Boca Raton, FL 33487-2742: CRC Press, Taylor and Francis Group.
- Goodman, D., and Palmese, G. (2002). Curing and bonding of composites using electron beam processing. In A. K. Kulshreshtha and C. Vasile (Eds.), *Handbook of Polymer Blends and Composites, Volume 1* (pp. 459–499). Shawbury, Shrewsbury, Shropshire, SY4 4NR, UK: Rapra Technology Ltd.
- Gopal, A. K., Adali, S., and Verijenko, V. E. (2000). Optimal temperature profiles for minimum residual stress in the cure process of polymer composites. *Composite Structures*, 48(1), 99–106.

- Graczykowski, C., Orlowska, A., and Holnicki-Szulc, J. (2016). Prestressed Composite Structures - Modeling, Manufacturing, Design. *Composite Structures*, 151, 172–182.
- Greszczuk, L. B. (1975). Foreign object impact damage to composites (Vol. STP 568 No. Vol. STP 568). Philadelphia: American Society for Testing and Materials.
- Gupta, A., and Raghavan, J. (2010). Creep of plain weave polymer matrix composites under on-axis and off-axis loading. Composites Part A: Applied Science and Manufacturing, 41(9), 1289–1300.
- Hadi, A. S., and Ashton, J. N. (1998). On the influence of pre-stress on the mechanical properties of a unidirectional GRE composite. *Composite Structures*, 40(3–4), 305–311.
- Han, C. D., and Chin, H. B. (1988). Development of a mathematical model for the pultrusion of unsaturated polyester resin. *Polymer Engineering and Science*, 28(5), 321–332.
- Harris, B. (1977). Fatigue and accumulation of damage in reinforced plastics. *Composites*, 8(4), 214–220.
- Hassan, A. K. F., and Abdullah, O. A. (2015). New Methodology for Prestressing Fiber Composites. Universal Journal of Mechanical Engineering, 3(6), 252– 261.
- Heckel, R. W., Zaehring, R. J., and Cheskis, H. P. (1972). *Optimization of the range* of elastic behavior of unidirectional composites by prestraining (technical report No. 5). Pittsburgh, Pa., USA: Office of naval research.
- Hibbeler, R. C. (2014). *Mechanics of Materials* (Ninth edit). USA: Pearson Prentice Hall.
- Hinton, M. J., Kaddour, A. S., and Soden, P. D. (Eds.). (2004). Failure criteria in fibre reinforced polymer composites: The world-wide failure exercise (First edit). The Boulevard, Langford Lane, Kidlington, Oxford OX5 1GB, UK: Elsevier Ltd.
- Hoa, S. V. (2009). *Principles of the Manufacturing of Composite Materials*. Lancaster, Pennsylvania, USA: DEStech Publications, Inc.
- Huang, Z. M. (2000). Strength formulae of unidirectional composites including thermal residual stresses. *Materials Letters*, 43(1–2), 36–42.
- Hyer, M. W. (1998). Stress Analysis of Fiber-Reinforced Composite Materials. Journal of Chemical Information and Modeling (First). Singapore: McGraw-Hill.

- Jain, L. K., and Mai, Y.-W. (1996). On Residual Stress Induced Distortions during Fabrication of Composite Shells. *Journal of Reinforced Plastics and Composites*, 15(8), 793–805.
- Jevons, M. P. (2004). *The effects of fibre pre-stressing on the impact performance of composite laminates*. PhD thesis, Engineering Systems Department, College of Defence Technology, Cranfield University, UK.
- Jevons, M. P., Fernando, G. F., and Kalsi, G. S. (2002). Effect of pre-tensioning on the low velocity impact performance of glass fibre composites. In *10th European conference on composite materials (ECCM-10)*. Brugge (Belgium).
- Jia, Y., Yan, W., and Liu, H.-Y. (2012). Carbon fibre pullout under the influence of residual thermal stresses in polymer matrix composites. *Computational Materials Science*, 62, 79–86.
- Jimenez, F. L., and Pellegrino, S. (2012). Constitutive modeling of fiber composites with a soft hyperelastic matrix. *International Journal of Solids and Structures*, 49(3–4), 635–647.
- Jones, R. M. (1999). *Mechanics of composite materials. CRC Press* (Second edi). Philadelphia, PA: Taylor and Francis.
- Jorge, L. D. A., Marques, A. T., and De Castro, P. M. S. (1990). The influence of prestressing on the mechanical behaviour of uni-directional composites. In J. Füller, G. Grüninger, K. Schulte, A. R. Bunsell, and A. Massiah (Eds.), *Developments in the Science and Technology of Composite Materials* (pp. 897–902). Stuttgart,Germany: Springer Netherlands.
- Kang, G., Liu, Y., Wang, Y., Chen, Z., and Xu, W. (2009). Uniaxial ratchetting of polymer and polymer matrix composites: Time-dependent experimental observations. Materials Science and Engineering A, 523(1–2), 13–20.
- Kannan, M., Kalaichelvan, K., and Sornakumar, T. (2015). Development and Mechanical Testing of Filament Wound FRP Composite Components. *Applied Mechanics and Materials*, 787, 578–582.
- Katerelos, D. T. G., Varna, J., and Galiotis, C. (2008). Energy criterion for modelling damage evolution in cross-ply composite laminates. *Composites Science and Technology*, *68*(12), 2318–2324.
- Kawai, M., Morishita, M., Fuzi, K., Sakurai, T., and Kemmochi, K. (1996). Effects of matrix ductility and progressive damage on fatigue strengths of unnotched and notched carbon fibre plain woven roving fabric laminates. *Composites Part A: Applied Science and Manufacturing*, *27*, 493–502.

- Kawai, M., and Taniguchi, T. (2006). Off-axis fatigue behavior of plain weave carbon/epoxy fabric laminates at room and high temperatures and its mechanical modeling. *Composites Part A: Applied Science and Manufacturing*, 37(2), 243–256.
- Kawai, M., and Matsuda, Y. (2012). Anisomorphic constant fatigue life diagrams for a woven fabric carbon/epoxy laminate at different temperatures. Composites Part A: Applied Science and Manufacturing, 43(4), 647–657.
- Kessler, M. R. (2004). Advanced Topics in Characterization of Composites. Victoria, BC, Canada: Trafford Publishing.
- Khan, L. A., Mahmood, A. H., Hassan, B., Sharif, T., Khushnod, S., and Khan, Z. M. (2014). Cost-effective manufacturing process for the development of automotive from energy efficient composite materials and sandwich structures. *Polymer Composites*, 35(1), 97–104.
- Knight, C. E. (1972). Orthotropic photoelastic analysis of residual stresses in filament-wound rings. *Experimental Mechanics*, 12, 107–112.
- Korenev, S. (2001). Electron beam curing of composites. *Vacuum*, 62(2–3), 233–236.
- Krishnamurthy, S. (2006). Prestressed advanced fibre reinforced composites: fabrication and mechanical performance. PhD thesis, Engineering System Department, Defence College of Management and Technology, Cranfield University, UK.
- Lässig, R., Eisenhut, M., Mathias, A., Schulte, R. T., Peters, F., Kühmann, T., ... Begemann, W. Series production of high-strength composites (2012). Munich.
- Lee, J., Harris, B., Almond, D. P., and Hammett, F. (1997). Fibre composite fatiguelife determination. *Composites - Part A: Applied Science and Manufacturing*, 28A, 5–15.
- Li, M. (2000). *Temperature and moisture effects on composite materials for wind turbine blades*. MSc thesis, Montana State University-Bozeman, Bozeman, Montana, USA.
- Lin, C. T., Kao, P. W., and Yang, F. S. (1991). Fatigue behaviour of carbon fibrereinforced aluminium laminates. *Composites*, 22(2), 135–141.
- Lingang, Z. (2013). Investigations on damage resistance of carbon fiber composite panels toughened using veils. *Chinese Journal of Aeronautics*, 26(3), 807–813.
- Liu, S.-C. (1999a). *Residual stress characterization for laminated composites*. PhD dissertation, University of Florida.

- Liu, H. (1999b). On steady-state fibre pull-out: II computer simulation. *Composites Science and Technology*, *59*(15), 2191–2199.
- Lu, H. (2005). Effects of Tape Tension on Residual Stress in Thermoplastic Composite Filament Winding. Journal of Thermoplastic Composite Materials, 18(6), 469–487.
- Madhukar, M. S., Genidy, M. S., and Russell, J. D. (2000). A new method to reduce cure-induced stresses in thermoset polymer composites, part I: test method. *Journal of Composite Materials*, *34*(22), 1882–1904.
- Mall, S. (1997). Laminated Polymer Matrix Composites. In P. K. Mallick (Ed.), *Composites Engineering Handbook* (p. 878). New York, USA: Marcel Dekker, Inc.
- Mandell, J. F., Reed, R. M., and Samborsky, D. D. (1992). *Fatigue of fiberglass wind turbine blade materials*. Contractor Report SAND92-7005, Albuquerque, New Mexico 87185, USA.
- Mandell, J., and Meier, U. (1983). Effect of stress ratio, frequency and loading time on the tensile fatigue of glass-reinforced epoxy. In T. O'Brien (Ed.), *Long-Term Behavior of Composites* (pp. 55–77). West Conshohocken, PA: ASTM International.
- Manders, P. W., and Chou, T. (1983). Enchancement of Strength in Composites Reinforced with Previously Stressed Fibers Mof. *Journal of Composite Materials*, 17(January 1983), 26–44.
- Miravalles, M. (2007). The creep behaviour of adhesives: A numerical and experimental investigation. Master thesis, Department of Civil and Environmental Engineering, Chalmers University of Technology, Göteborg, Sweden.
- Masuko, Y., and Kawai, M. (2004). Application of a phenomenological viscoplasticity model to the stress relaxation behavior of unidirectional and angle-ply CFRP laminates at high temperature. *Composites Part A: Applied Science and Manufacturing*, 35(7–8), 817–826.
- McMahon, P. E., and Ying, L. (1982). Effect of fiber/matrix interactions on the properties of graphite/epoxy composites. USA: National Aeronautics and Space Administration (NASA), Scientific and Technical Information Branch, NASA Contractor Report 3607.
- Mertiny, P., and Ellyin, F. (2002). Influence of the filament winding tension on physical and mechanical properties of reinforced composites. *Composites Part A: Applied Science and Manufacturing*, *33*(12), 1615–1622.

- Metehri, A., Serier, B., Bachir bouiadjra, B., Belhouari, M., and Mecirdi, M. A. (2009). Numerical analysis of the residual stresses in polymer matrix composites. *Materials and Design*, *30*(7), 2332–2338.
- Mills, G. J., and Dauksys, R. J. (1973). Effects of prestressing boron/epoxy prepreg on composite strength properties. *AIAA Journal*, *11*(11), 1459–1460.
- Miyake, T. (2011). Measuring fiber strain and creep behavior in polymer matrix composites using Raman spectroscopy. In R. M. Guedes (Ed.), Creep and Fatigue in Polymer Matrix Composites (First edition, pp. 149–183). Cambridge, UK: Limited, Woodhead Publishing.
- Montesano, J. (2012). Fatigue damage characterization of braided and woven fiber reinforced polymer matrix composites at room and elevated temperatures. Ryerson, University, Toronto, Ontario, Canada.
- Montesano, J., Fawaz, Z., Behdinan, K., and Poon, C. (2012). Fatigue Damage in On-Axis and Off-Axis Woven-Fiber/Resin Composite. *Key Engineering Materials*, 488–489, 230–233.
- Motahhari, S. (1998). Fiber prestressed composites: A study of the influences of fibre prestressing on the mechanical properties of polymer matrix composites. PhD thesis, Queen's University, Kingston, Ontario, Canada.
- Motahhari, S., and Cameron, J. (1997). Measurement of Micro-Residual Stresses in Fiber-Prestressed Composites. *Journal of Composite Materials*, 16(12), 1129–1137.
- Motahhari, S., and Cameron, J. (1998). Impact strength of fiber pre-stressed composites. *Journal of Reinforced Plastics and Composites*, 17(2), 123–130.
- Motahhari, S., and Cameron, J. (1999). Fibre prestressed composites: Improvement of flexural properties through fibre prestressing. *Journal of Reinforced Plastics and Composites*, 18(3), 279–288.
- Murasawa, G., Tohgo, K., and Ishii, H. (2004). Deformation behavior of NiTi/polymer shape memory alloy composites experimental verifications. *Journal of Composite Materials*, *38*(5), 399–416.
- Murray, G., White, C. V., and Weise, W. (2007). *Introduction to engineering materials*. Bosa Roca, USA: Taylor and Francis Group, CRC Press.
- Murugan, R., Ramesh, R., and Padmanabhan, K. (2014). Investigation on static and dynamic mechanical properties of epoxy based woven fabric glass/carbon hybrid composite laminates. In *Procedia Engineering, 12th Global Congress on Manufacturing and Management, GCMM 2014* (Vol. 97, pp. 459–468). Vellore, India: Elsevier B.V.

- Myers, D. G. (2004). *Method for measurement of residual stress and coefficient of thermal expansion of laminated composites*. University of Florida, USA.
- Naghashian, S., Fox, B. L., and Barnett, M. R. (2014). Actuation curvature limits for a composite beam with embedded shape memory alloy wires. *Smart Materials and Structures*, 23, 1–10.
- Naik, N. K. (2003). Woven-fibre thermoset composites. In B. Harris (Ed.), *Fatigue in composites:Science and technology of the fatigue response of fibrereinforced plastics* (First Ed., pp. 296–313). England: Woodhead Publishing Ltd and CRC Press LLC.
- Naik, N. K., and Ganesh, V. K. (1992). Prediction of on-axes elastic properties of plain weave fabric composites. *Composites Science and Technology*, 45(2), 135–152.
- Naik, N. K., and Ganesh, V. K. (1995). An analytical method for plain weave fabric composites. *Composites*, 26(4), 281–289.
- Naik, N. K., and Ganesh, V. K. (1996). Failure Behavior of Plain Weave Fabric Laminates under On-Axis Uniaxial Tensile Loading: I-Analytical Predictions. Journal of Composite Materials, 30(16), 1779–1822.
- Naik, R. A., Patel, S. R., and Case, S. W. (2001). Fatigue damage mechanism characterization and modeling of a woven graphite/epoxy composite. *Journal of Thermoplastic Composite Materials*, 14(5), 404–420.
- Nairn, J. A. (2000). Matrix Microcracking in Composites. In R. Talreja and J. A. Manson (Eds.), *Polymer matrix composites* (Vol. 2, pp. 403–432). Elsevier Science.
- Nakamura, T., and Suresh, S. (1993). Effects of thermal residual stresses and fiber packing on deformation of metal-matrix composites. *Acta Metallurgica et Materialia*, 41(6), 1665–1681.
- Nath, R. B., Fenner, D. N., and Galiotis, C. (2000). Progressional approach to interfacial failure in carbon reinforced composites: Elasto-plastic finite element modelling of interface cracks. *Composites Part A: Applied Science and Manufacturing*, *31*(9), 929–943.
- Nilakantan, G., and Gillespie, J. W. (2013). Yarn pull-out behavior of plain woven Kevlar fabrics: Effect of yarn sizing, pullout rate, and fabric pre-tension. *Composite Structures*, 101, 215–224.
- Ohno, N., Toyoda, K., Okamoto, N., Miyake, T., and Nishide, S. (1994). Creep Behavior of a Unidirectional SCS-6/Ti-15-3 Metal Matrix Composite at 450 °C. Journal of Engineering Materials and Technology, 116(2), 208–214.

- Pan, N. (1996). Analysis of woven fabric strengths: Prediction of fabric strength under uniaxial and biaxial extensions. *Composites Science and Technology*, 56(3), 311–327.
- Pan, N., Kovar, R., Dolatabadi, M. K., Wang, P., Zhang, D., Sun, Y., and Chen, L. (2015). Origin of tensile strength of a woven sample cut in bias directions. *Royal Society Open Science*, 2(5), 1–18.
- Pandita, S. D., Huysmans, G., Wevers, M., and Verpoest, I. (2001). Tensile fatigue behaviour of glass plain-weave fabric composites in on- and off-axis directions. *Composites - Part A: Applied Science and Manufacturing*, 32(10), 1533–1539.
- Pang, J. W. C., and Fancey, K. S. (2006). An investigation into the long-term viscoelastic recovery of Nylon 6,6 fibres through accelerated ageing. *Materials Science and Engineering A*, 431(1–2), 100–105.
- Pang, J. W. C., and Fancey, K. S. (2008). Analysis of the tensile behaviour of viscoelastically prestressed polymeric matrix composites. *Composites Science and Technology*, 68(7–8), 1903–1910.
- Pang, J. W. C., and Fancey, K. S. (2009). The flexural stiffness characteristics of viscoelastically prestressed polymeric matrix composites. *Composites Part* A: Applied Science and Manufacturing, 40(6–7), 784–790.
- Papanicolaou, G. C., and Zaoutsos, S. P. (2011). Viscoelastic constitutive modeling of creep and stress relaxation in polymers and polymer matrix composites. In R. M. Guedes (Ed.), *Creep and fatigue in polymer matrix composites* (first edit, pp. 3–47). Abington Hall, Granta Park, Great Abington, Cambridge, UK: Woodhead Publishing Limited.
- Parlevliet, P. P., Bersee, H. E. N., and Beukers, A. (2006). Residual stresses in thermoplastic composites - a study of the literature. Part I: Formation of residual stresses. *Composites Part A: Applied Science and Manufacturing*, 37(6), 1847–1857.
- Parlevliet, P. P., Bersee, H. E. N., and Beukers, A. (2007a). Residual stresses in thermoplastic composites - a study of the literature. Part III: Effects of thermal residual stresses. *Composites Part A: Applied Science and Manufacturing*, 38, 1581–1596.
- Parlevliet, P. P., Bersee, H. E. N., and Beukers, A. (2007b). Residual stresses in thermoplastic composites a study of the literature. Part II: Experimental techniques. *Composites Part A: Applied Science and Manufacturing*, 38, 651–665.
- Parlevliet, P. P., van der Werf, W. A. W., Bersee, H. E. N., and Beukers, A. (2008). Thermal effects on microstructural matrix variations in thick-walled composites. *Composites Science and Technology*, 68(3–4), 896–907.

- Parthenios, J., Psarras, G. C., and Galiotis, C. (2001). Adaptive composites incorporating shape memory alloy wires. Part 2: development of internal recovery stresses as a function of activation temperature. *Composites Part A: Applied Science and Manufacturing*, 32(12), 1735–1747.
- Piggott, M. R. (1995). The effect of fibre waviness on the mechanical properties of unidirectional fibre composites: A review. *Composites Science and Technology*, 53(2), 201–205.
- Potluri, P., and Thammandra, V. S. (2007). Influence of uniaxial and biaxial tension on meso-scale geometry and strain fields in a woven composite. *Composite Structures*, 77(3), 405–418.
- Potter, K. (1997). Introduction to Composite Products Design, development and manufacture (First edit). Chapman and Hall, London, UK.
- Potter, K., Khan, B., Wisnom, M., Bell, T., and Stevens, J. (2008). Variability, fibre waviness and misalignment in the determination of the properties of composite materials and structures. *Composites Part A: Applied Science and Manufacturing*, 39(9), 1343–1354.
- Psarras, G. C., Parthenios, J., and Galiotis, C. (2001). Adaptive composites incorporating shape memory alloy wires, Part I: Probing the internal stress and temperature distributions with a laser Raman sensor. *Journal of Materials Science*, *36*(3), 535–546.
- Raghavan, J., and Meshii, M. (1997). Creep rupture of polymer composites. Composites Science and Technology, 57(4), 375–388.
- Rao, S. S. (2005). The Finite Element Method in Engineering (Fourth). Oxford, UK: Elsevier Butterworth-Heinemann.
- Ravi, S., Iyengar, N. G. R., Kishore, N. N., and Shukla, A. (2000). Influence of fiber volume fraction on dynamic damage in woven glass fabric composites: An experimental study. *Advanced Composite Materials*, 9(4), 319–334.
- Reinhart, T. J. (1998). Overview of composite materials. In S. T. Peters (Ed.), *Handbook of Composites* (Second edi, pp. 21–33). Tonbridge, England: Springer Science+Business Media Donlrecht.
- Riley, M. B., and Whitney, J. M. (1966). Elastic properties of fiber reinforced composite materials. *AIAA Journal*, 4(9), 1537–1542.
- Rios-Soberanis, C. R., Cruz-Estrada, R. H., Rodriguez-Laviada, J., and Perez-Pacheco, E. (2012). Study of mechanical behavior of textile reinforced composite materials. *Dyna*, 176, 115–123.

- Rohen, L., Margem, F., Neves, A., Monteiro, S., Gomes, M., de Castro, R., ... de Paula, F. (2015). Izod impact test in epoxi matrix composites reinforced with hemp fiber. In J. Carpenter, C. Bai, J. Escobedo-Diaz, J.-Y. Hwang, S. Ikhmayies, B. Li, ... M. Zhang (Eds.), *Characterization of Minerals, Metals, and Materials 2015* (pp. 557–562). Walt disney World, Orlando, Florida, USA: John Wiley and Sons, Inc., Hoboken, New Jersy.
- Sadiq, A. (2007). *The effect of fiber pre-tension on the static and dynamic behavior of composite plates*. PhD thesis, Machines and Equipments Engineering, University of Technology, Iraq.
- Saiman, M. P., Wahab, M. S., and Wahit, M. U. (2014). The effect of fabric weave on the tensile strength of woven kenaf reinforced unsaturated Polyester composite. In *Proceedings of the International Colloquium in Textile Engineering, Fashion, Apparel and Design 2014 (ICTEFAD 2014)* (pp. 25– 29).
- Sapuan, S. M. (2010). Concurrent engineering for composites. Universiti Putra Malaysia Press (First edit). Selangor: Universiti Putra Malaysia.
- Sapuan, S. M., Abdalla, H. S., and Nash, R. J. (1995). Proposed design and manufacturing techniques of polymeric based composite pedal box system. In D. Stockton and C. Wainwright (Eds.), Advances in manufacturing technology IX: Proceedings of the 11th national conference on manufacturing research (pp. 77–81). CRC Press.
- Scherf, J., and Wagner, H. D. (1992). Interpretation of fiber fragmentation in carbon/epoxy single fiber composites: Possible fiber pre-tension effects. *Polymer Engineering and Science*, 32(4), 298–304.
- Schlichting, L. H., de Andrada, M. A. C., Vieira, L. C. C., de Oliveira Barra, G. M., and Magne, P. (2010). Composite resin reinforced with pre-tensioned glass fibers. Influence of prestressing on flexural properties. *Dental Materials*, 26(2), 118–125.
- Schlottermuller, M., Lu, H., Roth, Y., Himmel, N., Schledjewski, R., and Mitschang,
 P. (2003). Thermal Residual Stress Simulation in Thermoplastic Filament
 Winding Process. *Journal of Thermoplastic Composite Materials*, 16(6), 497–519.
- Schlottermuuller, M., Schledjewski, R., and Mitschang, P. (2004). Infuence of process parameters on residual stress in thermoplastic filament-wound parts. *Journal of Materials: Design and Applications*, *218*(2), 157–164.
- Schulte, K., and Marissen, R. (1992). Influence of artificial pre-stressing during curing of CFRP laminates on interfibre transverse cracking. *Composites Science and Technology*, 44(4), 361–367.

- Scida, D., Aboura, Z., Benzeggagh, M. L., and Bocherens, E. (1999). A micromechanics model for 3D elasticity and failure of woven-fibre composite materials. *Composites Science and Technology*, 59(4), 505–517.
- Selezneva, M., Montesano, J., Fawaz, Z., Behdinan, K., and Poon, C. (2011). Microscale experimental investigation of failure mechanisms in off-axis woven laminates at elevated temperatures. *Composites Part A: Applied Science and Manufacturing*, 42(11), 1756–1763.
- Shimbo, M., Ochi, M., Inamura, T., and Inoue, M. (1985). Internal stress of epoxide resin modified with spiro ortho-ester type resin. *Journal of Materials Science*, 20, 2965–2972.
- Shokrieh, M. (2014). *Residual stresses in composite materials. Residual Stresses in Composite Materials.* Cambridge: Woodhead Publishing Limited.
- Singh, A. (2001). Radiation processing of carbon fibre-reinforced advanced composites B. Nuclear Instruments and Methods in Physics Research, 185(1-4), 50-54.
- Širvaitienė, A., Jankauskaite, V., Bekampiene, P., and Kondratas, A. (2013a). Influence of natural fibre treatment on interfacial adhesion in biocomposites. *Fibres and Textiles in Eastern Europe*, 100(4), 123–129.
- Širvaitienė, A., Jankauskaitė, V., Bekampienė, P., and Norkaitis, J. (2013b). Vegetable fiber pre-tensioning influence on the composites reinforcement. *Polymer Composites*, 34(9), 1533–1537.
- Srinivas, M. V, Dvorak, G. J., and Prochazka, P. (1999). Design and fabrication of submerged cylindrical laminates-II. Effect of fiber pre-stress. *International Journal of Solids and Structures*, 36(26), 3917–3943.
- Stamatopoulos, K. (2011). *Measurement of residual stresses in composite materials with the incremental hole drilling method*. National Technical University of Athens, Greece.
- Sui, G. X., Yao, G., and Zhou, B. L. (1995). Influence of artificial pre-stressing during the curing of VIRALL on its mechanical properties. *Composites Science and Technology*, 53(4), 361–364.
- Sui, G. X., Yao, G., and Zhou, B. L. (1996). Effects of prestrain on the fatigue of VIRALL laminate properties. *Composite Science and Technology*, 56, 929– 932.
- Suvorov, A. P., and Dvorak, G. J. (2001). Optimal design of prestressed laminate/ceramic plate assemblies. *Meccanica*, *36*(1), 87–109.
- Suvorov, A. P., and Dvorak, G. J. (2002). Stress Relaxation in Prestressed Composite Laminates. *Journal of Applied Mechanics*, 69(4), 459–469.

- Swain, R. E. (1992). The Role of the Fiber/Matrix Interphase in the Static and Fatigue Behavior of Polymeric Matrix Composite Laminates. PhD thesis, Virginia Polytechnic Institute and State University.
- Syngellakis, S. (Ed.). (2015). *Natural filler and fibre composites: development and characterisation*. Southampton, UK: WIT Press.
- Tabuchi, D., Sajima, T., Doi, T., and Onikura, H. (2012). Residual stress of hoopwound CFRP composites manufactured with simultaneous heating. *Sensors and Materials*, 24(2), 99–111.
- Talreja, R. (2016). Fatigue damge mechanisms. In R. Talreja and J. Varna (Eds.), Modeling Damge, Fatigue and Failure of Composite Materials (pp. 25–39). Cambridge, UK: Woodhead Publishing.
- Talreja, R., and Singh, C. V. (2012). Damage and failure of composite materials (First edit, Vol. 1). University Press, Cambridge, UK: Cambridge University Press.
- Tamuzs, V., Dzelzitis, K., and Reifsnider, K. (2004). Fatigue ofWoven Composite Laminates in Off-Axis Loading II. Prediction of the Cyclic Durability. Applied Composite Materials, 11(5), 281–293.
- Tamuzs, V., Dzelzitis, K., and Reifsnider, K. (2008). Prediction of the cyclic durability of woven composite laminates. *Composites Science and Technology*, 68(13), 2717–2721.
- Tan, S. C., and Nuismer, R. J. (1989). A Theory for progressive matrix cracking in composite laminates. *Journal of Composite Materials*, 23(10), 1029–1047.
- Thomas, S., Joseph, K., Malhotra, S. K., Goda, K., and Sreekala, M. S. (Eds.). (2012). *Polymer Composites, Macro- and Microcomposites*. Singapore: John Wiley and Sons.
- Tisza, M., Lukacs, Z., and Gal, G. (2008). Integrated process simulation and diedesign in sheet metal forming. *International Journal of Material Forming*, *1*, 185–188.
- Tsai, S. W., and Hahn, H. T. (1980). Introduction to composite materials (First Edit). Lancaster, Pennsylvania, USA: Technomic Pub, Inc.
- Tsai, J.-L., and Chi, Y.-K. (2008). Investigating thermal residual stress effect on mechanical behaviors of fiber composites with different fiber arrays. *Composites Part B: Engineering*, *39*(4), 714–721.
- Tuttle, M. E. (1988). A mechanical/thermal analysis of prestressed composite laminates. *Journal of Composite Materials*, 22(8), 780–792.

- Tuttle, M. E., Koehler, R. T., and Keren, D. (1996). Controlling thermal stresses in composites by means of fiber prestress. *Journal of Composite Materials*, 30(4), 486–502.
- Vigo, T. L., and Kinzig, B. J. (Eds.). (1992). Composite applications: The role of matrix, fiber and interface. Advanced Materials (First edit). New York, USA: Wiley-VCH.
- Vizzini, A., and Orso, J. (1994). The effects of an expanding monomer on the tensile properties of graphite/epoxy. *Journal of Composites, Technology and Research*, *16*(3), 270–274.
- Wang, B., and Fancey, K. S. (2015a). Shape-Changing (Bistable) Composites Based on Viscoelastically Generated Prestress. In A. L. Araújo, J. R. Correia, and C. M. Mota Soares (Eds.), 10th International Conference on Composite Science and Technology, ICCST/10 (pp. 1–9). Lisbon, Portugal.
- Wang, B., and Fancey, K. S. (2015b). Towards optimisation of load-time conditions for producing viscoelastically prestressed polymeric matrix composites. *Composites Part B: Engineering*, 87, 336–342.
- Wang, B. L., Sun, Y. G., and Zhang, H. Y. (2008). Multiple cracking of fiber/matrix composites-Analysis of normal extension. *International Journal of Solids* and Structures, 45(14–15), 4032–4048.
- Warrier, S. G., Rangaswamy, P., Bourke, M. a. M., and Krishnamurthy, S. (1999). Assessment of the fiber/matrix interface bond strength in SiC/Ti-6Al-4V composites. *Materials Science and Engineering: A*, 259(2), 220–227.
- Weber, C. H., Du, Z. Z., and Zok, F. W. (1996). High temperature deformation and fracture of a fiber reinforced titanium matrix composite. Acta Materialia, 44(2), 683–695.
- White, S. R., and Hahn, H. T. (1992a). Process Modeling of Composite Materials: Residual Stress Development during Cure. Part I. Model Formulation. Journal of Composite Materials, 26(16), 2402–2422.
- White, S. R., and Hahn, H. T. (1992b). Process Modeling of Composite Materials: Residual Stress Development during Cure. Part II. Experimental Validation. Journal of Composite Materials, 26(16), 2423–2453.
- White, S. R., and Hahn, H. T. (1993). Cure cycle optimization for the reduction of processing-induced residual stresses in composite materials. *Journal of Composite Materials*, 27(14), 1352–1378.
- Wicaksono, S., and Chai, G. B. (2013). A review of advances in fatigue and life prediction of fiber-reinforced composites. Proceedings of the Institution of Mechanical Engineers, Part L: Journal of Materials: Design and Applications, 227(3), 179–195.

- Wijskamp, S., Akkerman, R. and Lamers, E. A. D. (2003). Residual stresses in non-symmetrical carbon/epoxy laminates. In Proceedings of the 14th International Conference on Composite Materials (ICCM-14). San Diego, California USA.
- Williams, J. C., and Starke, E. A. (2003). Progress in structural materials for aerospace systems. *Acta Materialia*, 51(19), 5775–5799.
- Xu, J., Miao, Y., Qiao, M., and Li, S. (2014). Tension design of heated-mandrel winding process based on analytical algorithm. *Journal of Reinforced Plastics and Composites*, 33(16), 1529–1541.
- Zaidi, B. M., Magniez, K., and Miao, M. (2015). Prestressed natural fibre spun yarn reinforced polymer-matrix composites. *Composites Part A: Applied Science* and Manufacturing, 75, 68–76.
- Zhao, J., and Cameron, J. (1998). Polypropylene matrix composites reinforced with pre-stressed glass fibers. *Polymer Composites*, 19(3), 218–224.
- Zhao, L. G., Warrior, N. a., and Long, A. C. (2006). A micromechanical study of residual stress and its effect on transverse failure in polymer-matrix composites. *International Journal of Solids and Structures*, 43(18–19), 5449–5467.
- Zhigun, I. G. (1968). Experimental evaluation of the effect of prestressing the fibers in two directions on certain elastic characteristic of woven-glass reinforced plastics. *Polymer Mechanics*, 4(4–6), 691–695.