



**UNIVERSITI PUTRA MALAYSIA**

***MICROSTRIP TECHNIQUE AND MODELING FOR DETERMINATION OF  
MICROWAVE PROPERTIES OF Ni-Zn FERRITE***

**FAHMIRUDDIN ESA**

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DETERMINATION OF MICROWAVE PROPERTIES OF Ni-Zn  
FERRITE**

**By**

**FAHMIRUDDIN ESA**

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Abstract of thesis presented to the Senate of Universiti Putra Malaysia in  
fulfilment of the requirement for the degree of Doctor of Philosophy

## **MICROSTRIP TECHNIQUE AND MODELING FOR DETERMINATION OF MICROWAVE PROPERTIES OF Ni-Zn FERRITE**

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**January 2015**

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Ni-Zn ferrite has been such important topics since 1900 but the reported works are mainly discussed on the sample preparation technique also microstructural and morphological analysis. Even though microwave properties of Ni-Zn ferrite have also been discovered by various workers using waveguide technique however air gap problems are still remain as the major issues. Furthermore, the effect of different Ni-Zn ratio in  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  on the reflection, transmission and absorption properties in a wideband and higher frequency using microstrip technique has not been investigated. This thesis describes a detailed study on the application of a microstrip technique to determine the microwave properties of  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  in the frequency range between 1 GHz and 10 GHz. The x compositions of the spinel ferrite were 0.1, 0.3, 0.5, 0.7, 0.9. The  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  samples were prepared by 10 hours sintering at 900°C with 4°C/min increment from room temperature. Particles showed phase purity and crystallinity in powder X-ray diffraction (XRD) analysis. Surface morphology measurement of Scanning Electron Microcopy (SEM) was conducted on the plane surfaces of the molded samples which gave information about grain morphology, boundaries and porosity. The tabulated grain size for all samples was in the range of 62 nm – 175 nm. Energy dispersive X-ray analysis (EDX) was done to confirm the elemental composition of the Ni-Zn ferrite samples by their weight and atomic percentage of each element for certain particular composition taken from specific area of the micrograph.

The transmission ( $S_{21}$ ) and reflection ( $S_{11}$ ) properties of the microstrip loaded with  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  were extensively studied theoretically using finite element method. The microstrip measurements were conducted using a

HP8720B vector network analyzer. The electromagnetic field distribution of the microstrip covered with  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  sample was visualized using FEM software COMSOL. It was found that  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  with higher values of  $x$  absorbed more microwave energy which in turn reduced the reflection and transmission coefficients. A good linear relationship was found between the absorption loss  $P_{loss}$  and fractional composition  $x$  at 3 GHz. The waves were totally absorbed by  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  at frequencies above 7 GHz for  $x \geq 0.5$ . An optimization routine was also introduced in this work to determine both the permittivity and permeability of  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  sample by matching the theoretical and measured values of  $S_{11}$  and  $S_{21}$ . The complex permittivity and permeability of  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  sample along the frequency ranges were linked to the other findings. The measured S-parameters were compared with the results obtained using the Nicolson Ross Weir (NRW), Finite Element Method (FEM) and optimization method. The optimization method provides the highest accuracy when compared with the measured  $|S_{11}|$  and  $|S_{21}|$  with a mean error 0.0403 and 0.0177, respectively.

Abstrak tesis yang dikemukakan kepada Senat Universiti Putra Malaysia  
sebagai memenuhi keperluan untuk ijazah Doktor Falsafah

## **KAEDAH MIKROSTRIP DAN PEMODELAN UNTUK MENENTUKAN SIFAT GELOMBANGMIKRO Ni-Zn FERRITE**

Oleh

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Ni-Zn ferit telah menjadi topik yang penting sejak tahun 1900 tetapi kerja-kerja yang dilaporkan adalah lebih kepada perbincangan mengenai teknik penyediaan bahan juga analisis struktur mikro dan morfologi. Walaupun ciri-ciri gelombang mikro telah dipelopori oleh pelbagai penyelidik dengan menggunakan teknik pandu gelombang namun masalah ruang udara adalah masih menjadi isu besar. Tambahan lagi, kesan nisbah Ni-Zn dalam  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  terhadap ciri pantulan, penghantaran dan penyerapan dalam jalur lebar dan frekuensi tinggi menggunakan teknik mikrostrip belum lagi dikaji. Tesis ini memperihalkan kajian yang mendalam terhadap aplikasi teknik mikrostrip untuk menentukan ciri-ciri gelombang mikro bagi  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  dalam frekuensi antara 1 GHz dan 10 GHz. Komposisi  $x$  bagi ferit spinel adalah 0.1, 0.3, 0.5, 0.7, 0.9. Sampel  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  telah disediakan menggunakan kaedah pensinteran selama 10 jam pada suhu 900 °C dengan kadar kenaikan suhu sebanyak 4°C/min dari suhu bilik. Zarah sampel yang terbentuk menunjukkan fasa keaslian dan penghabluran dalam analisis pembelauan sinaran-X (XRD). Pengukuran morfologi permukaan menggunakan imbasan elektron mikrofotokopi (SEM) telah dijalankan pada permukaan satah sampel yang telah diacukan untuk mendapatkan maklumat berkenaan morfologi, sempadan dan keliangan butiran. Saiz butiran untuk semua sampel adalah dalam lingkungan 62 nm – 175 nm. Analisis serakan tenaga sinaran-X (EDX) dijalankan untuk mengenalpasti komposisi unsur sampel Ni-Zn ferit berdasarkan peratusan berat dan atom untuk setiap unsur dalam komposisi tertentu yang diambil dari kawasan mikrogaf yang spesifik.

Ciri penghantaran ( $S_{21}$ ) dan pantulan ( $S_{11}$ ) bagi mikrostrip yang berisi dengan sampel  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  telah dikaji terperinci berdasarkan teori

menggunakan kaedah elemen terhingga (FEM). Pengukuran mikrostrip dijalankan dengan menggunakan HP8720B analisis rangkaian vektor (VNA). Taburan medan elektromagnetik bagi mikrostrip tertutup dengan sampel  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  telah digambarkan menggunakan perisian FEM COMSOL. Hasil kajian ini mendapati  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  dengan nilai  $x$  yang tinggi menyerap lebih banyak tenaga gelombang mikro yang seterusnya merendahkan pekali pantulan dan penghantaran. Hubungan linear yang baik telah didapati antara kehilangan penyerapan  $P_{loss}$  dan pecahan komposisi  $x$  pada 3 GHz. Gelombang ini telah diserap sepenuhnya oleh  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  pada frekuensi lebih daripada 7 GHz bagi sampel dengan  $x \geq 0.5$ . Rutin pengoptimuman turut dijalankan untuk menentukan ketelusan dan ketelapan sampel  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  dengan memadankan nilai  $S_{11}$  and  $S_{21}$  yang diperolehi daripada perkiraan dan pengukuran. Ketelusan dan ketelapan kompleks bagi sampel  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  sepanjang julat frekuensi telah dikaitkan dengan penemuan lain. S-parameter yang diperolehi daripada pengukuran dibandingkan dengan S-parameter yang diperolehi daripada Nicolson Ross Weir (NRW), kaedah elemen terhingga (FEM) dan kaedah pengoptimuman. Kaedah pengoptimuman memberi keputusan yang paling tepat apabila dibandingkan dengan  $|S_{11}|$  dan  $|S_{21}|$  dengan purata ralat masing-masing 0.0403 dan 0.0177.

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This thesis was submitted to the Senate of Universiti Putra Malaysia and has been accepted as fulfilment of the requirement for the degree of Doctor of Philosophy. The members of the Supervisory Committee were as follows:

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## LIST OF ABBREVIATIONS & SYMBOLS

EM	-	Electromagnetic
EMI	-	Electromagnetic interference
MHz	-	Megahertz
GHz	-	Gigahertz
AC	-	Alternating current
DC	-	Direct current
TVS	-	Transient voltage suppressor
$\text{FeO/Fe}_2\text{O}_3$	-	iron(II) oxide/hematite
Ni-Zn ferrite	-	Nickel zinc ferrite
Mn-Zn ferrite	-	Manganese zinc ferrite
Fe	-	Iron
Si	-	Silicon
$\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$	-	Nickel Zinc Ferrite with fractional composition of $x$
$x$	-	Mole fraction
MNDT	-	Microwave Non-Destructive Technique
m	-	Meter
XRD	-	X-ray diffraction
SEM	-	Scanning Electron Microscopy
SEI	-	Secondary electron imaging
BEI	-	Backscattered electron imaging
EDX	-	Energy dispersive X-ray
FDTD	-	finite difference time-domain method
MoM	-	method of moment
FEM	-	finite element method
TEM	-	Transverse electromagnetic

NRW	-	Nicolson Ross Weir
FE	-	field emission
Ni	-	Nickel
Zn	-	Zinc
O	-	Oxide
eV	-	Electron volt
keV	-	Kilo electron volt
cm	-	Centimeter
mm	-	Milimeter
$\mu\text{m}$	-	Micrometer
nm	-	Nanometer
COMSOL	-	COMSOL Multiphysics®
NEC	-	Numerical electromagnetic computational
$\varepsilon'$	-	Dielectric constant
$\varepsilon''$	-	Dielectric loss factor
$\mu'$	-	Permeability
$\mu''$	-	Magnetic loss factor
$\varepsilon$	-	Complex permittivity
$\mu$	-	Complex permeability
$\tan \delta$	-	Loss tangent
$E$	-	Electric field
$H$	-	Magnetic field
MUT	-	Material under test
S-parameters	-	Scattering parameters
RF	-	Radio frequency
TE	-	Transverse electric
TM	-	Transverse magnetic

RBC	-	Reflectionless boundary condition
ABC	-	Absorbing boundary condition
PML	-	Perfectly match layer
CEM	-	Computational electromagnetic
HFSS	-	High frequency structural simulator
TPNR	-	Thermoplastic natural rubber
PP	-	Polypropylene
NR	-	Natural rubber
LNR	-	Liquid natural rubber
RL	-	Reflection loss
PVC	-	Polyvinylchloride
dB	-	Decibel
PU	-	Polyurethane
PANI	-	Polyaniline
Li-Zn ferrite	-	Lithium zinc ferrite
RAM	-	Radar absorbing material
$\epsilon_{eff}$	-	Effective permittivity
$\mu_{eff}$	-	Effective permeability
$\epsilon_r$	-	Relative permittivity
$\mu_r$	-	Relative permeability
NOEs	-	Number of elements
PDE	-	Partial differential equation
$S_{11}$	-	Reflection coefficient
$S_{21}$	-	Transmission coefficient
$ S_{11} $	-	Magnitude of reflection coefficient
$ S_{21} $	-	Magnitude of transmission coefficient
$\angle S_{11}$	-	Phase angle of reflection coefficient

$\angle S_{21}$	-	Phase angle of transmission coefficient
$Z_o$	-	Characteristic impedance / characteristic impedance of the measurement system
$Z_s$	-	Input impedance
$W$	-	Width of the conductor line
$h$	-	Height of the substrate
$d$	-	Sample's height
$l$	-	Length of the substrate
$L$	-	Sample's length
$\tau_{meas}$	-	Measured group delay
$\lambda$	-	Wavelength
$f$	-	Frequency
kV	-	Kilovolt
mA	-	Miliampere
$d_{hkl}$	-	Distance between lattices
$\theta$	-	Diffraction angle
$a$	-	Cell perimeter (lattice constant)
$D_x$	-	X-ray density
$M$	-	Molecular mass
$N$	-	Avogadro's number
DXF	-	Drawing Exchange Format
VNA	-	Vector Network Analyzer
PEC	-	Perfect electric conductor
JCPDS	-	Joint Committee on Powder Diffraction Standards
Å	-	Angstrom



## CHAPTER 1

### INTRODUCTION

Electromagnetic (EM) waves at microwave frequencies have found many applications in various fields such as wireless telecommunication system, radar, local area network, electronic devices, mobile phones, laptops and medical equipment (Lim et al., 2003; Maeda et al., 2004; Jing et al., 2009; Lakshmi et al., 2009). The effect of growth in various applications has led to many electromagnetic interference (EMI) problems that has to be suppressed to acceptable limits. EMI reducing materials (absorbers) may be dielectric or magnetic (Grimes and Grimes, 1993) and the design depends on the frequency range, the desired quantity of shielding and the physical characteristics of the devices being shielded. This EMI could be suppressed by using ferrite materials (magnetic absorbers) due to their various electrical and magnetic properties. A case study on the development of EMI shielding ferrite has been made by Chandran and Cursetji (1999). Thus it is important to determine their high frequency characteristics for the applications of EM in the high GHz ranges (Arshak et al., 2001; Da Silva and Mohallem, 2001; Zabetakis et al., 2005; Hwang, 2006).

#### 1.1 EMI Shielding Materials

EMI shielding and suppression materials can be broadly categorized into three groups (Ramasamy, 1997); EMI shielding materials, surge or transient suppression components and EMI filter materials. The EMI shielding is the use of conductive materials such as copper, aluminum, silver and nickel in the form of adhesive tape or paint coatings to reduce radiated EMI reflection or absorption. It is used for a wide variety of commercial/military EMI shielding applications.

The second category is briefly explained in the transient voltage protection for alternating current (AC) and direct current (DC) power circuits. Circuits or devices protection against high voltage transients or surges of thousands volts caused by lightning strike are intensely needed. Electronic system might be damaged by the unexpected change in voltages if proper protection is not provided. Suppression components such as gas diodes, silicon varistors, metal oxide varistors, transient voltage suppressor (TVS) diodes and clamping principles may be connected indirectly in parallel circuits using decoupling impedances in order to achieve good protection to the circuit.

Low pass EMI filters are used to attenuate conducted noise currents in variety of applications including shielded enclosures and other electrical or

electronic subsystems. Application of filter is very important, whether to protect the equipment from incoming interference or to suppress the interference generated by the equipment to minimum level or to protect the signal lines. The performance of the filter is being judged by its insertion loss and attenuation characteristics. Lossy line or dissipative filters can perform well at high frequency (500 MHz to 10 GHz) and have the great advantage of removing the noise energy in the form of heat. Ferrite beads and ferrite rod are the example of lossy line EMI absorptive filters.

The shielding property of the ferrite is strongly influenced by the process parameters and microstructure (Chandran and Cursetji, 1999). The properties of ferrites which strongly influence the EMI suppression capability include the chemical composition, crystalline structure, grain size, nature of porosity, thickness of grain boundary and magnetocrystalline anisotropy. Each of this property shows an important role in the end properties of the ferrites and thus necessitates fine tuning of each of these to suit the end applications.

#### **1.1.1 Magnetic Absorber**

Ferrites are metallic oxides that contain iron for example that occur in nature and have been known as hematite. The divalent iron ( $\text{FeO}$ ) contains two electrons and the trivalent iron ( $\text{Fe}_2\text{O}_3$ ) contains three electrons with uncompensated magnetic moments. In magnetite, half the trivalent iron occupies a type A crystallographic sites while the divalent iron and the rest of the trivalent iron occupy type B crystallographic sites. At zero Kelvin all moments at a given type site are aligned parallel, and the two types of sites are antiparallel with each other. The result is the net magnetic moment of the divalent iron. Because of the cancellation and dilution by oxygen, the magnetic moment is much smaller than for the metals. The permeability is therefore also much less. Since hematite is conductive, it is not suitable to be as an absorber. Useful material has the divalent iron replaced by another divalent metal; a common one is a mixture of nickel and zinc. Spinel material is cubic and moments are initially in equivalent crystallographic directions.

#### **1.1.2 Nickel Zinc Ferrite**

Nickel Zinc Ferrite (Ni-Zn ferrite), together with manganese zinc ferrites (Mn-Zn ferrite) is a major member of spinel ferrite family. The spinel ferrites can be magnetized or demagnetized easily by externally applied magnetic fields indicating that they have soft magnetic behavior. In addition, they have good magnetic properties with enhanced performance when compared to metallic magnets such as Fe and layered Fe-Si alloys (Sugimoto, 1999). Besides, they have high electrical resistivity, high magnetic permeability and possible modification of intrinsic properties over wide spectrums which enable them to be used as ceramic materials (Hench and West, 1990).

Ni-Zn ferrite ceramics are the preferred ceramic material for high frequency applications in order to suppress generation of Eddy current (Verma et al. 1999). Although Ni-Zn ferrite ceramics have high electrical resistivity to prevent Eddy current generation, they have moderate magnetic permeability compared to Mn-Zn ferrites. However, the electrical and magnetic properties of these ferrite ceramics are heavily influenced by its microstructural features such as grain size, the nature of grain boundaries and the extent and nature of porosity. The microstructural features of interest could be attained via chemical composition and high temperature processing (Jonker and Stuijts, 1971).

The aim of this study is to determine electromagnetic properties of Ni-Zn ferrites prepared at different chemical composition based on chemical formula  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  with  $0.1 \leq x \leq 0.9$  that sintered at constant temperature. The variations in the microstructures, elemental composition and alterations in scattering parameters as well as their electromagnetic properties of the Ni-Zn ferrites are the concern of this study.

## **1.2 An Overview of Microwave Technique**

Microwave Non-Destructive Technique (MNDT) has been used effectively to measure electromagnetic materials. The technique was firstly described in the early 1950's and since then many studies being published. Before this time, there was no equipment for the measurement of such short electromagnetic waves. The research and development in this technique enable the measurement of electromagnetic materials at higher microwave frequencies using more reasonable and robust generators.

The technique allows the measurement of electromagnetic materials at the microwave region with frequency and wavelength approximately between 300 MHz to 300 GHz and  $10^{-3}$  and  $10^{-1}$  m, respectively (Ida, 1992). The measurement is only limited to non-conducting material since MNDT has minimal penetration in good conducting material. However, microwaves are affected by a large number of material properties. The properties that can be measured by MNDT in lossless or lossy dielectrics are material composition, uniformity of the material, moisture and contamination content and other varied properties such as porosity.

Other conventional technique is filling a section of a standard closed transmission line such as a waveguide to measure microwave permittivity and permeability (Singh et al., 2000; Sharma and Afsar, 2011; Bayrakdar, 2011). However, this technique requires several types of sample preparation upon the measurement across the frequency ranges such as from 1.7 to 12.4 GHz. The frequency ranges include five frequency bands that are R (1.70-2.60 GHz), S (2.60-3.95 GHz), G (3.95-5.85 GHz), C (5.85-8.20 GHz) and X (8.20-12.40 GHz). Each band requires a different waveguide dimension and hence the volume of sample used also must be different for each band.

The other great measurement method in a wide band frequency for magnetic thin film materials is microstrip transmission method that have been studied by Saed (2005) and Wu et al. (2009) which the sample is deposited on rigid substrate. The microstrip transmission method is one of planar transmission line method since the thin film materials can be easily loaded in the measurement test fixture. The microstrip transmission line is based on a reflection and transmission technique adapted to a two port microstrip transmission line (Liu et al., 2005). The permittivity and permeability of the thin film can be determined by analyzing the full S-parameters of the two ports.

The microstrip line technique is easy to use, quick, non-destructive and has high sensitivity and accuracy especially for practical routine work. In addition, it should be able to measure samples with small and large cross section.

### **1.3 Microwave Characterization Techniques**

Microwave behaves similar to light wave in terms of travel in straight lines, refract, reflect, diffract, scatter and interfere according to the same physical length. The only difference between them is a wavelength. The wavelength of microwave is usually  $10^5$  larger than the wavelength of light wave. Therefore, the microwave tends to interact with materials and structures on a macroscopic scale. For instance, microwaves are capable of penetrating most nonmetallic materials, reflecting and scattering from internal boundaries and interacting with molecules (Bahr, 1982).

The interaction between microwaves and materials can be deduced from Maxwell's equations and material properties. The relations define a variety of properties such as mode of propagation, reflection, refraction, transmission and impedance. Both permittivity and permeability are complex numbers of which the imaginary part is associated with losses. This rich and complex system of properties allows a very wide range of measurement techniques at microwave frequencies. To date, many different methods have been proposed for microwave measurements of electromagnetic properties of material (Afsar et al., 1986; Ghodgaonkar et al., 1990; Queffelec et al., 1994; Baker-Jarvis et al., 1995; Faircloth et al., 2006).

### **1.4 Electromagnetic Modeling of Wave Interaction with Materials**

The microwave sensor design problem is formally solved using the conventional analytical techniques but recently, some of numerical techniques have been utilized and mostly favored. This is due to the increase in computer's processor speed. Besides, the numerical methods are more accurate, easy and time saving compared to the traditional empirical modeling method which deals with many complex mathematic equations. Currently, variation of the numerical methods, such as finite

difference time-domain method (FDTD), method of moment (MoM) and finite element method (FEM) are being commercialized. In this work, COMSOL interactive environment software for modeling and solving scientific and engineering problems is used. The software enables the visualization view of the system work which provides clear understanding about the designed working system. In this study, the FEM is used to separate the solution region of the designed open microstrip and fully covered microstrip into small elements. The FEM provides a clear contour of field distribution for both cases. The procedure of FEM simulation of the microstrip will be explained in Section 4.4.

### 1.5 Problem Statement

Ni-Zn ferrite has been a subject of intense research since 1900. However, the reported works were mainly on sample preparation techniques followed by conventional characterization techniques such as XRD, FESEM, SEM etc. Although microwave properties of Ni-Zn ferrite have also been investigated by various workers (Ma et al., 2008; Verma et al., 2003) but none has given a detailed description of Ni-Zn ferrite properties in a wide frequency range. The frequency limitation was due to the fact that different microwave techniques utilized different types of sample holder. At the lower end of the microwave frequencies (less than 1 GHz), the fixture holder is usually in the form of parallel plate. At higher frequencies, the closed coaxial and waveguide techniques are the most commonly used method to determine the transmission and reflection properties of materials. Both techniques are prone to measurement error due to the demand of fitting the samples snugly into the sample holder without leaving air gaps between the sample and the walls of the sample holder. An alternative solution is to measure the reflection coefficient of the sample using an open ended coaxial technique. Permittivity can be calculated from the measured reflection coefficient but the open ended coaxial technique could not provide information regarding the transmission and absorption properties of the sample. Microstrip techniques have also been used to measure permittivity and permeability of ferrites. However, the effect of different fractional composition  $x$  in Ni-Zn ferrite ( $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$ ) on the transmission and absorption properties of the sample have not been investigated.

This thesis presents a detailed study on the effect of different composition of  $x$  in Ni-Zn ferrite overlay on the reflection, transmission and absorption of a microstrip transmission line in the frequency range from 1 GHz to 10 GHz. The mixing process of Ni-Zn ferrite samples were prepared using agate mortar and characterized using XRD, SEM and EDX. This work presents a pioneering study on the application of Finite Element Method (FEM) to calculate the scattering parameters of a microstrip covered with Ni-Zn ferrite. The effect of different values of  $x$  in  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  on the reflection, transmission and absorption properties are experimentally investigated.



## 1.6 Objectives

The main objectives of this work are

1. To prepare Ni-Zn ferrite samples using conventional mixing process method according to  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  formula ( $0.1 \leq x \leq 0.9$ ) and characterize the structure and surface morphology of Ni-Zn ferrite by employing XRD and SEM as well as traced element identified by EDX.
2. To determine the complex permittivity of pure NiO, ZnO,  $\text{Fe}_2\text{O}_3$  and  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  in the frequency range between 1 GHz and 10 GHz.
3. To clarify the variation in  $S_{11}$  and  $S_{21}$  with frequency for an open microstrip and covered microstrip on the effect of different fractional composition  $x$  in Ni-Zn ferrite in the range frequency of 1 – 10 GHz.
4. To clarify the relationship between power loss and fractional composition of  $x$  in  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  as well as the electric and magnetic field distribution inside the Ni-Zn ferrite sample using FEM.
5. To estimate complex permittivity and permeability of Ni-Zn ferrite sample by applying an optimization procedure via MATLAB in conjunction with the comparison of the results of  $S_{11}$  and  $S_{21}$  for covered microstrip between measurements, Nicolson Ross Weir (NRW), FEM and optimization.

## 1.7 Thesis Outline

This thesis is divided into six chapters and six appendices. Chapter 1 is a general introduction to give an overview of microwave techniques, nickel zinc ferrite material, electromagnetic modeling of wave interaction with microstrip and characterization techniques involving morphological and electrical properties. This chapter also discusses the problem statements and research objectives in details.

Chapter 2 reviews on the crystal structure of spinel ferrites as well as the cation distribution. Several microwave measurement techniques for the determination of material electromagnetic properties including commercial coaxial probe, free space, resonant cavities, waveguide and coaxial line technique as well as their limitations. The chapter also gives an overview of microstrip transmission line technique and also the advantageous in performing microwave characterization measurement. Several numerical methods are also reviewed in the structure analysis including the basic procedure, advantage and limitations of each technique.

Chapter 3 presents a general survey on the characteristic impedance and effective permittivity for open microstrip using quasi-TEM approximation. Comparison of characteristic impedance calculated between quasi-TEM and FEM is shown to be in a good agreement. The calculation of characteristic impedance of covered microstrip is performed by finite element method (FEM). The calculation of reflection and transmission coefficients of the microstrip line is considered in wave approach. The FEM formulation applies to determine the reflection and transmission coefficient of the covered microstrip. The calculation of  $S_{11}$  and  $S_{21}$  are also been reviewed.

Details of sample preparation, structure characterization, surface morphology and S-parameters experimental setup using microstrip technique will be discussed in Chapter 4. This chapter also describes the implementation procedure of the covered microstrip that has been performed using COMSOL software.

Chapter 5 describes microstructural and electromagnetic characterization results in details. This chapter shows the results of comprehensive S-parameters ( $S_{11}$  and  $S_{21}$ ) measurements for open microstrip as well as for microstrip covered with  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  samples using Vector Network Analyzer 8720B (VNA). Permittivity of  $\text{Ni}_x\text{Zn}_{1-x}\text{Fe}_2\text{O}_4$  samples are also performed using Agilent Dielectric Probe Kit 85070B, which can be used as an initial guess in the optimization process. There are also comparisons of obtained S-parameters using NRW and FEM methods. An optimization procedure to improve NRW formulas and to determine S-parameters of  $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  material by finding the best values of complex permittivity and permeability will be discussed in this chapter.

Finally, in Chapter 6, conclusions are drawn and suggestions are made for future research activities in this field.

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