



**UNIVERSITI PUTRA MALAYSIA**

***COMBUSTION PROCESS OF HOMOGENEOUS CHARGE  
COMPRESSION IGNITION ENGINE USING NUMERICAL  
MODELING***

***NAJIHAH BINTI MD ZAIN @ ABDUL RAHMAN***

**FK 2014 70**



**COMBUSTION PROCESS OF HOMOGENEOUS CHARGE  
COMPRESSION IGNITION ENGINE USING NUMERICAL  
MODELING**

**By**

**NAJIHAH BINTI MD ZAIN @ ABDUL RAHMAN**

**This thesis submitted to the School of Graduate Studies, Universiti Putra  
Malaysia, in fulfillment of the requirements for the  
Degree of Master of Science**

**March, 2014**

## COPYRIGHT

All material contained within the thesis, including without limitation text, logos, icons, photographs and all other artwork, is copyright material of Universiti Putra Malaysia unless otherwise stated. Use may be made of any material contained within the thesis for non-commercial purposes from the copyright holder. Commercial use of material may only be made with the express, prior, written permission of Universiti Putra Malaysia.

Copyright © Universiti Putra Malaysia



Abstract of thesis is presented to the Senate of Universiti Putra Malaysia in fulfillment of the requirement for the degree of Master of Science

**COMBUSTION PROCESS OF HOMOGENEOUS CHARGE  
COMPRESSION IGNITION ENGINE USING NUMERICAL  
MODELING**

By

**NAJIHAH MD ZAIN @ ABDUL RAHMAN**

**March 2014**

**Chairman : Nuraini Abdul Aziz, PhD**  
**Faculty : Engineering**

A zero dimensional thermodynamic numerical model is developed to simulate the combustion characteristics and performance of a four stroke gasoline engine using homogeneous compression combustion ignition (HCCI) method. This model which applies the first law of thermodynamics for a closed system is inclusive of empirical model for predicting the important parameters for engine cycles: the combustion timing and mass burnt fraction during the combustion process. The hypothesis is the increasing intake temperature can reduce the combustion duration and the fuel consumption at wide range of equivalence ratio, resulting in decreasing peak pressure and friction losses, and hence, increasing the engine efficiency. The intake temperature were increased from 373-433 K with increment of 20 K. The engine was operated over a range of equivalence ratios of 0.2 to 0.5 at constant engine speed of 1200 rpm and intake pressure of 89,950 K Pa. Simulations were performed using Simulink<sup>®</sup> under different engine operating conditions. The model was successfully developed to predict the combustion characteristics and performance. Validations show good agreements between the experimental data and simulation results. Increasing intake temperature allows reducing the combustion duration by 0.99 °CA and 0.26 °CA at equivalence ratios of 0.2 and 0.5, respectively, followed by decreasing the heat released to the wall about 22.79%. The brake power reduces up to 3.56% at any equivalence ratios. However, the brake specific fuel consumption decreases about 6.09%-5.76% at 0.2-0.5 of equivalence ratios, respectively. Increasing intake temperature does not increase the power output. However, it is able to improve the efficiency at richer mixture as the fuel consumption and brake specific fuel consumption also can be decreased.

Abstrak tesis dikemukakan kepada Senat Universiti Putra Malaysia sebagai memenuhi keperluan untuk Ijazah Master Sains

**PROSES PEMBAKARAN BAGI ENJIN PENCUCUHAN MAMPAT  
BERCAJ SERAGAM MENGGUNAKAN PERMODELAN BERANGKA**

Oleh

**NAJIHAH MD ZAIN @ ABDUL RAHMAN**

**March 2014**

**Pengerusi : Nuraini Abdul Aziz, PhD**  
**Fakulti : Kejuruteraan**

Satu permodelan berangka dengan dimensi termodinamik sifar telah dibangunkan untuk mendapatkan simulasi ciri-ciri dan prestasi enjin petrol berlejang empat menggunakan kaedah pencucuhan mampat bercaj seragam. Model yang mengaplikasi hukum pertama termodinamik bagi system tertutup ini merangkumi model empirik untuk meramal parameter penting bagi kitaran enjin: pemaasan pembakaran dan pecahan jisim yang terbakar semasa proses pembakaran. Hipotesis adalah peningkatan suhu masukan boleh mengurangkan tempoh pembakaran dan penggunaan bahan api pada nisbah setara dalam julat yang besar, menghasilkan pengurangan tekanan puncak dan tenaga geseran, dan oleh yang demikian, meningkatkan kecekapan enjin. Suhu masukan telah ditingkatkan daripada 373 K kepada 433 K dengan kenaikan sebanyak 20 K. Enjin telah dijalankan di bawah nisbah kesetaraan daripada 0.2 kepada 0.5 pada kelajuan enjin tetap sebanyak 1200 rpm dan tekanan masukan sebanyak 89,950 KPa. Simulasi dijalankan menggunakan perisian Simulink<sup>®</sup> dalam pelbagai keadaan operasi enjin. Model telah dibangunkan dengan jayanya untuk meramal ciri-ciri pembakaran dan prestasi, yang mana persamaan yang hampir bagi keputusan eksperimen dan simulasi. Peningkatan suhu masukan membolehkan pengurangan tempoh pembakaran sebanyak 0.99 °CA dan 0.26 °CA masing-masing pada 0.2 dan 0.5 nisbah kesetaraan, diikuti oleh pengurangan pelepasan haba kepada dinding sebanyak 22.79%. Kuasa brek berkurangan sehingga 3.56% pada mana-mana nisbah kesetaraan. Walaubagaimanapun, penggunaan bahan api tentu brek berkurangan kira-kira 6.09%-5.76% masing-masing pada 0.2-0.5 nisbah kesetaraan. Peningkatan suhu masukan tidak meningkatkan pengeluaran kuasa. Namun, ia mampu meningkatkan kecekapan pada campuran yang lebih pekat dan mengurangkan penggunaan bahan api dan penggunaan bahan api tentu brek.

## ACKNOWLEDGEMENTS

All the praise and gratitude be upon Allah the Almighty for His mercifulness giving me knowledge, patience and good health to complete my master research successfully.

It is a great pleasure to take this opportunity to express my gratitude for the support of Universiti Putra Malaysia under Research University Grants (RUGS), Project No. 05-05-10-1076RU for this research.

I am so grateful to my supervisor, Dr. Nuraini Abdul Aziz and thankful to the member of the supervisory committee, Dr. Othman Inayatullah for their support in this research work and the entire preparation of the thesis.

I would like to express my appreciation and thanks to Mr. Mohd Hafizul Hashim, technician of thermodynamic laboratory for his assistance in performance engine testing activities, my colleagues, Mr. M. Izadi Najafabadi and Mr. Ahsanul Kaiser, Master candidates for their suggestions and comments on this work.

Finally, I would like to express my gratitude and appreciation to my husband, children and family for their invaluable support and understanding. They have provided me motivations and encouragement to complete this thesis.

*Najihah, March 2014*



© COPYRIGHT UPM

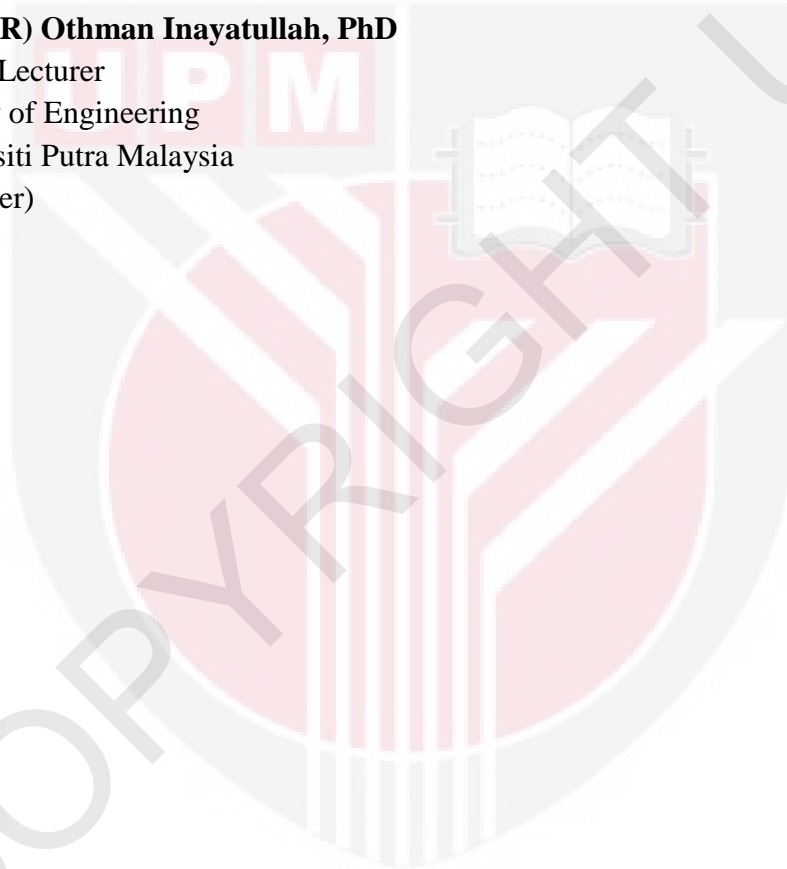
This thesis was submitted to the Senate of Universiti Putra Malaysia and has been accepted as fulfillment of the requirement for the degree of Master of Science. The members of the Supervisory Committee were as follows:

**Nuraini Abdul Aziz, PhD**

Senior Lecturer  
Faculty of Engineering  
Universiti Putra Malaysia  
(Chairman)

**Capt. (R) Othman Inayatullah, PhD**

Senior Lecturer  
Faculty of Engineering  
Universiti Putra Malaysia  
(Member)



---

**BUJANG BIN KIM HUAT, PhD**

Professor and Dean  
School of Graduate Studies  
Universiti Putra Malaysia

Date:



## Declaration by graduate student

I hereby confirm that:

- this thesis is my original work;
- quotations, illustrations and citations have been duly referenced;
- this thesis has not been submitted previously or concurrently for any other degree at any other institutions;
- intellectual property from the thesis and copyright of thesis are fully-owned by Universiti Putra Malaysia, as according to the Universiti Putra Malaysia (Research) Rules 2012;
- written permission must be obtained from supervisor and the office of Deputy Vice-Chancellor (Research and Innovation) before thesis is published (in the form of written, printed or in electronic form) including books, journals, modules, proceedings, popular writings, seminar papers, manuscripts, posters, reports, lecture notes, learning modules or any other materials as stated in the Universiti Putra Malaysia (Research) Rules 2012;
- there is no plagiarism or data falsification/fabrication in the thesis, and scholarly integrity is upheld as according to the Universiti Putra Malaysia (Graduate Studies) Rules 2003 (Revision 2012-2013) and the Universiti Putra Malaysia (Research) Rules 2012. The thesis has undergone plagiarism detection software.

Signature: \_\_\_\_\_

Date: 26 June 2014

Name and Matric No.: Najihah binti Md Zain @ Abdul Rahman (GS30028)

## Declaration by Members of Supervisory Committee

This is to confirm that:

- the research conducted and the writing of this thesis was under our supervision;
- supervision responsibilities as stated in the Universiti Putra Malaysia (Graduate Studies) Rules 2003 (Revision 2012-2013) are adhered to.

Signature: \_\_\_\_\_

Name of  
Chairman of  
Supervisory  
Committee: \_\_\_\_\_

Signature: \_\_\_\_\_

Name of  
Member of  
Supervisory  
Committee: \_\_\_\_\_

## TABLE OF CONTENTS

	<b>Page</b>
<b>ABSTRACT</b>	ii
<b>ABSTRAK</b>	iii
<b>ACKNOWLEDGEMENT</b>	iv
<b>APPROVAL</b>	v
<b>DECLARATION</b>	vi
<b>LIST OF TABLES</b>	vii
<b>LIST OF FIGURES</b>	xii
<b>LIST OF APPENDICES</b>	xv
<b>LIST OF ABBREVIATIONS</b>	xvii
<b>CHAPTER</b>	
<b>1 INTRODUCTION</b>	<b>1</b>
1.1 Background	1
1.2 Problem Statement	3
1.3 Hypothesis	3
1.4 Objectives of Research Work	4
1.5 Scope of Research Work	4
1.6 Thesis Organization	5
<b>2 LITERATURE REVIEW</b>	<b>6</b>
2.1 Homogeneous Charge Compression Ignition Engine	6
2.2 Engine of the Future	8
2.2.1 Effect of Equivalence Ratio on Combustion Process	10
2.2.2 Effect of Intake Temperature on Combustion Process	13
2.2.3 Effects of Combustion Duration on Engine Performances	15
2.2.4 Other Challenges in HCCI Engine	18
2.3 Engine Modeling	19
2.3.1 HCCI Mean Value Model	20
2.3.2 Simulink® Modeling Method	21
2.4 Summary	22
<b>3 RESEARCH METHODOLOGY</b>	<b>24</b>
3.1 Introduction	24
3.2 HCCI Combustion	25
3.3 HCCI Engine Model	25

3.4	Comparison with Experiments	27
<b>4</b>	<b>NUMERICAL MODEL DEVELOPMENT</b>	<b>29</b>
4.1	Introduction	29
4.2	Assumptions	29
4.3	Engine Numerical Modeling	31
4.3.1	Engine Geometry	31
4.3.2	Cylinder Pressure Model	33
4.3.3	Burn Duration Model	34
4.3.4	Heat Release Model	36
4.3.5	Air-Fuel Ratio	37
4.3.6	Heat Transfer	38
4.3.7	Exhaust Flow Model	39
4.3.8	Exhaust Pressure and Temperature	41
4.3.9	Residual Gases	43
4.3.10	Gas Exchange Process	44
4.3.11	Engine Performance	45
4.4	Summary	47
<b>5</b>	<b>RESULTS AND DISCUSSIONS</b>	<b>55</b>
5.1	Introduction	55
5.2	Calibration of Model and Validations	55
5.3	Effect of Intake Temperature on the Pressure	59
5.4	Effect of Intake Temperature on the Work Done	62
5.5	Effect of Intake Temperature on the Burning Duration	63
5.6	Effect of Intake Temperature on the Heat Transfer	65
5.7	Effect of Intake Temperature on the Engine Performance	67
5.8	Summary	71
<b>6</b>	<b>CONCLUSION AND RECOMMENDATIONS FOR FUTURE RESEARCH</b>	<b>73</b>
6.1	Conclusion	73
6.2	Recommendations for Future Research	74
	<b>REFERENCES</b>	<b>75</b>
	<b>APPENDICES</b>	<b>81</b>
	<b>BIODATA OF STUDENT</b>	<b>101</b>
	<b>LIST OF PUBLICATIONS</b>	<b>102</b>

## LIST OF TABLES

<b>Table</b>		<b>Page</b>
2.1	Summary of previous work on input parameter variations	9
3.1	Engine specifications (Guo and et al., 2010)	27
3.2	Engine specifications (Maurya and Agarwal, 2011)	27
4.1	Air-fuel ratio of many fuel substances	37
4.2	Algorithm A	52
4.3	Algorithm B	53
4.4	Engine operating conditions and output results	54

## LIST OF FIGURES

Figure		Page
1.1	Equivalence ratio versus temperature map	2
2.1	Four stroke engine cycle	7
2.2	Effect of the air-fuel ratio on the HCCI combustion timing and duration	11
2.3	Lines of constant equivalence ratio as a function of torque and engine speed	12
2.4	Ratio of heat release at final ignition (AF) to a cool flame (AC) varying equivalence ratio	12
2.5	Ignition delays as a function of equivalence ratio	13
2.6	Heating and hot EGR effects on the auto-ignition timing and combustion duration	15
2.7	Operating range and iso-lines of AFR of gasoline fuels	16
2.8	Engine load for various AFR and exhaust valve timing at 1500rpm	16
2.9	Relationship between engine output and combinations of AFR and intake temperature	17
2.10	Effect of the engine speed on the heat release in HCCI combustion conditions	18
3.1	Flowchart of research work	26
3.2	Schematic diagram of HCCI engine	26
4.1	Piston cylinder and geometries	31
4.2	The mass burn rate profile	35
4.3	Assumption of pressure inside manifold	42
4.4	Assumption of temperature inside manifold	42
4.5	Assumption of exhaust gas temperature	43

4.6	Flow chart for numerical simulation	49
5.1	Comparison between experimental and simulation for pressure traces at 900 rpm	56
5.2	Comparison between experimental and simulated using HCCI engine at 1500 rpm (a) Maximum pressure (b) Maximum temperature	57
5.3	Comparison between experimental and simulated of engine performance using HCCI engine at 1500 rpm; (a) Indicated mean effective pressure (IMEP) (b) Gas exchange efficiency (c) Indicated thermal efficiency (d) Indicated specific fuel consumption (ISFC)	58
5.4	Cylinder pressure at compression stroke versus crank angle at various equivalence ratios of an intake temperature 373 K at 1200 rpm	59
5.5	Cylinder pressure at compression stroke versus crank angle at various equivalence ratios of an intake temperature 433 K at 1200 rpm	60
5.6	Cylinder pressure at compression stroke versus crank angle at various intake temperatures of an equivalence ratio 0.2 at 1200 rpm	60
5.7	Cylinder pressure at compression stroke versus crank angle at various intake temperatures of an equivalence ratio 0.5 at 1200 rpm	61
5.8	Cylinder peak pressure at compression stroke at various intake temperatures at 1200 rpm	61
5.9	Indicated and brake mean effective pressure with respect to equivalence ratios at various intake temperatures at 1200 rpm	62
5.10	Power with respect to equivalence ratios at various intake temperatures at 1200 rpm	63
5.11	Mass fraction burnt versus crank angle at various intake temperature of an equivalence ratio 0.2 at 1200 rpm	64
5.12	Mass fraction burnt versus crank angle at various intake temperature of an equivalence ratio 0.5 at 1200 rpm	65
5.13	Combustion duration versus equivalence ratio (0.2-0.5) at various intake temperature at 1200 rpm	65

5.14	Heat losses respect to equivalence ratio at various intake temperature at 1200 rpm	66
5.15	Indicated power versus equivalence ratios at 1200 rpm	67
5.16	Brake power versus equivalence ratios at 1200 rpm	68
5.17	Indicated fuel consumption efficiency versus equivalence ratios at 1200 rpm	68
5.18	Brake fuel consumption efficiency versus equivalence ratios at 1200 rpm	69
5.19	Brake specific fuel consumption versus equivalence ratios at 1200 rpm	69
5.20	Fuel consumption versus equivalence ratios at 1200 rpm	70

## LIST OF APPENDICES

Appendix	Page
A.1. Combustion duration	81
A.2. Maximum cylinder pressure	81
A.3. Heat losses through the combustion wall	81
A.4. Maximum exhaust temperature	82
A.5. Maximum indicated work done	82
A.6. Indicated mean effective pressure	82
A.7. Brake mean effective pressure	82
A.8. Indicated power	83
A.9. Brake power	83
A.10. Indicated fuel conversion efficiency	83
A.11. Brake fuel conversion efficiency	83
A.12. Brake specific fuel consumption	84
A.13. Fuel consumption	84
B.1. HCCI main block details	86
B.2. Mean piston block details	87
B.3. Engine geometry block details	87
B.4. Engine geometry/Vd block details	88
B.5. Engine geometry/A(CA) block details	88
B.6. Engine geometry/V(CA) block details	88
B.7. Engine geometry/crank geometry block details	89
B.8. Wiebe function block details	89
B.9. Burn duration block details	90
B.10. Fuel block details	91
B.11. Residual gas block details	91



B.12.	Pressure block details	92
B.13.	Pressure/Cf factor block details	93
B.14.	Pressure/Cheat factor block details	93
B.15.	Pressure/Lift valve function block details	93
B.16.	Pressure/Pressure ratio block details	94
B.17.	Pressure/Discharge coefficient block details	94
B.18.	Pressure/Charge mass rate block details	95
B.19.	Exhaust temperature block details	96
B.20.	Woschni correlation block details	97
B.21.	Heat transfer block details	97
B.22.	Work and power block details	97
B.23.	Work and power/Work block details	98
C.1.	Matlab® code for performance calculation	99

## LIST OF ABBREVIATIONS

ATDC	After top dead center
AFR	Air-to-fuel ratio
BTDC	Before top dead center
CAD	Crank angle degree
EGR	Exhaust gas recirculation
HV	heating value
IVO	Intake valve open
IVC	Intake valve close
LHV	Low heating value
MFB	Mass fraction burning
RES	residual gas
SOC	Start of ignition
<i>f</i> mep	frictional loss mean effective pressure
<i>i</i> mep	Indicated mean effective pressure
<i>b</i> mep	Brake mean effective pressure
<i>b</i> sfc	Brake specific fuel consumption
<i>s</i> fc	Specific fuel consumption
<i>i</i> fce	Indicated fuel conversion efficiency
<i>b</i> fce	Brake fuel conversion efficiency
<i>i</i> P	Indicated power
<i>b</i> P	Brake power

### *Latin character*

<i>A</i>	Area	(m <sup>2</sup> )
<i>a</i>	Crank radius	(m)

$B$	Cylinder bore	(m)
$c$	Mass heat capacity	(J/kg.K)
$c_m$	Piston mean speed	(m/s)
$C$	Constant value/factor/coefficient	
$D$	Diameter	(m)
$E_c$	Activation energy	(J/kg)
$h$	Enthalpy	(J/kg)
$h_t$	Heat transfer coefficient	(W/m <sup>2</sup> K)
$k$	Constant	
$l$	Length	(m)
$L_v$	Axial valve lift	(m)
$m$	Mass	(kg)
$M$	Molecular weight	(kg/kmole)
$n_R$	Number of cylinder	
$N$	Engine speed	(rpm)
$P$	Power	(J/s)
$p$	Pressure	(Pa)
$Q$	Heat	(J)
$R_u$	Universal gas constant (8314.34)	(J/kgK)
$r$	Radius	(m)
$s$	Piston stroke	(m)
$t$	Time	(s)
$T$	Temperature	(K)
$u$	Internal energy	(J/kg)
$v$	Specific volume	(m <sup>3</sup> /kg)
$V$	Volume	(m <sup>3</sup> )
$W$	Work done	(J)

# CHAPTER 1

## INTRODUCTION

### 1.1 Background

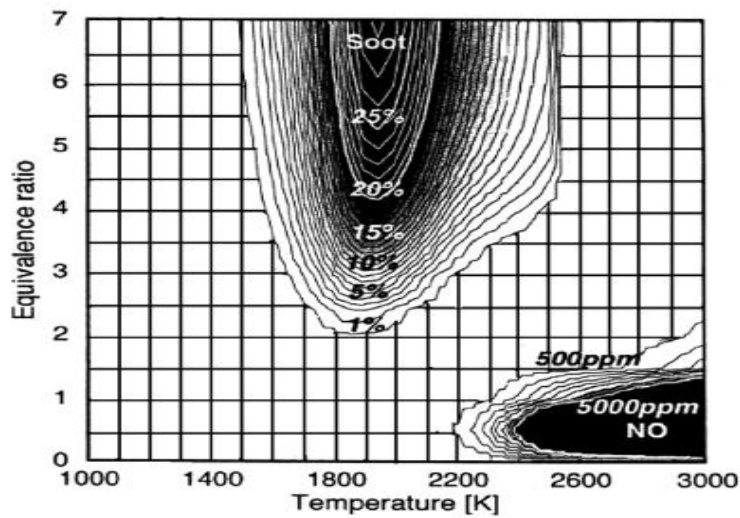
Decreasing primary fuel resources and stringent emission legislations have been motivating many researchers from automotive field to develop and study on engines that are capable of reducing the amount of hazardous emissions and the fuel consumption while maintaining the engine high thermal efficiency. The two conventional engines of spark ignition (SI) and compress ignition (CI) have been utilized over the years and studied to have critical exhaust products problems. The problems have been solved using the after-treatment methods which have added more cost on installation and maintenance. Yet, hazardous emissions are still relatively higher than the emission legislation requirement.

In order to cope with future emission legislation requirements and reduce fuel consumption while maintaining high engine efficiency, one of the most important advancements is to implement Homogeneous Charge Compression Ignition (HCCI) combustion in engine. HCCI is a high efficiency technology to be utilized in any sizes and classes of transportation as well as in stationary applications such as in electric generators (Shahbakti, 2009).

In comparison to SI and CI engines, HCCI engine has higher part load efficiency due to no throttling losses which then contribute to no pumping losses, no particular matters production and very low  $\text{NO}_x$  emissions (Heywood, 1988). It is difficult to reduce smoke and  $\text{NO}_x$  simultaneously through combustion improvement only. Emission control has become one of interest among automotive researchers because current methods like the Three Way Catalyst (TWC) used in SI and non-thermal plasma used in CI are expensive and consume extra 2-4% of overall fuel consumption (Taylor, 2008; Bauer and Bosch, 2011). However, in HCCI engine, the fuel and air should be mixed homogeneously in the combustion chamber before the combustion starts and the mixture would be ignited spontaneously due to temperature increasing at the end of the compression stroke (Maurya and Agarwal, 2009).

The HCCI engine has the advantage of high compression ratio similar to the CI engine; no throttling losses and lean mixture. The auto-ignition temperature, which is equal to the temperature after compression stroke, requires range of 1400K-1500K for completing Carbon Monoxide (CO) and Hydrocarbon (HC) components oxidization and can be below 1800K to prevent  $\text{NO}_x$  formation, due to high dilution of charge by low equivalence ratio of below 0.3 as in Figure 2

(Johansson B. , 2007; Kitamura, et.al, 2003). Thus, the  $\text{NO}_x$  formation and soot formation can be reduced simultaneously.



**Figure 1.1. Equivalence Ratio versus Temperature Map (Johansson B. , 2007)**

However, there are several downsides of HCCI combustion. Firstly, there is no direct combustion trigger, like in SI (triggered by spark) and CI (triggered by fuel injection) engines. This auto-ignition behavior makes the combustion being very sensitive to its initial conditions like inlet pressure, temperature, fuel composition and homogeneity of the mixture (Marriott and Reitz, 2002; Li, Zhao, Brouzos and Ma, 2006; Zhao, 2007; Yao, Zheng and Liu, 2009). These initial conditions need to be controlled to obtain the correct combustion phasing.

Secondly, HCCI combustion process is unstable especially at lower and higher engine loads. It has been proven to work well on medium load where on low load, as it tends to misfire and on high load, it tends to damage the engine (Maurya and Agarwal, 2011). Thirdly, HCCI has smaller operating region than that of the two conventional engines. At high loads, early combustion can produce unacceptable peak cylinder pressure causing excessive noise, potentially damaging the engine and increasing Nitrogen Oxides ( $\text{NO}_x$ ) production, while the late combustion leads to incomplete combustion and increasing Carbon Monoxide (CO) and Unburned Hydrocarbons (UHC) (Olsson J. O., et al., 2002).

The combustion timing can be controlled indirectly through adjustments of parameters involved in the cylinder charge preparation. One of the possible ways is controlling the mixture reactivity which can be actuated by the equivalence ratio. Equivalence ratio control is done by the fuelling system of the engine. The control of injected air-fuel can be done by adjusting the throttle opening size. However, this size will not only affect the in cylinder mixing, but also the

residual gas fraction in a manner that it is not possible to change only this parameter to control of series of engine runs. In this study, the effects of equivalence ratio and intake temperature on the combustion phasing and engine efficiency are predicted by numerical simulation of thermodynamic equations of homogeneous charge compression ignition combustion system so that a leaner mixture of AFR can be utilized accordingly to an appropriate intake temperature to improve the engine efficiency.

## **1.2 Problem Statement**

Different combinations of equivalence ratio and intake temperature have different effects on the combustion timings and the performance of a four-stroke HCCI engine. At increasing engine speeds, combustion timing holds significant role to ensure completeness of combustion process and avoid undesirable pressure rise rate in the cylinder which would cause high fuel consumption and engine damage (Olsson J. O., et al., 2002; Bogemann, 2009). Combustion timing is essential in order to control the load to obtain low fuel consumptions, low emissions and high engine efficiency. It is dependable of chemical reactions inside the cylinder which is influenced by factors such as equivalence ratio and intake temperature. High equivalence ratio increases the overall in cylinder activities and speeds up the combustion process. It will result in combustion timing to decrease and allow undesirable pressure rise rate. This phenomenon may contribute to piston engine damage. However, at low equivalence ratio, compression ratio and intake air temperature must be set properly to ensure auto-ignition. Otherwise, misfiring will occurred and result in very low combustion efficiency. Increasing intake air temperature is able to improve combustion process at low equivalence ratio and decreasing intake air temperature is able to reduce the pressure rise rate and heat release rate at high equivalence ratio. Therefore, both are the best candidates to enhance the combustion characteristics of an HCCI engine. The numerical model is able to simulate the effect of both parameters to the combustion characteristics. Although the computational model is unable to obtain the exact characteristics because there are many complex phenomena taking place in the engine hardly being modeled through numerical method, it is capable to estimate the trend of engine characteristics and allows engine designer to change and test many different parameters without building up the real engines. Therefore, this study is focusing on the simulation.

## **1.3 Hypothesis**

At constant speed, as the equivalence ratio is decreased, the intake temperature must be increased to have higher engine efficiency and advance the start of combustion. Increasing intake temperature can produce higher combustion efficiency and lower fuel consumption at any low equivalence ratios. At constant

temperature, the equivalence ratio plays important parameter to boost the power produced and increase the combustion efficiency.

#### **1.4 Objectives of Research Work**

The main objective of this research is to study the effects of equivalence ratio and intake temperature values on the four-stroke, gasoline fueled HCCI engine performance and combustion phasing using computer simulation. Thus, specific objectives to achieve main objective are:

1. To develop a physical based four-stroke gasoline fueled HCCI engine model based on thermodynamic equations of HCCI engine using Simulink® software for predicting power characteristics in order to study the effects of some parameters on the engine performances.
2. To predict burn duration of different combinations of equivalence ratios and intake temperature which is needed to study the combustion timing.
3. To evaluate the combustion characteristic and engine performance of the HCCI engine with varying equivalence ratio and intake temperature under constant speed.

#### **1.5 Scope of Research Work**

The scope of work covers the evaluation of HCCI engine performance on several combinations of equivalence ratios and intake temperature. In this study, the engine performance and combustion characteristics are based on the numerical analysis and then validated with the experimental data from literatures. The fuel chosen for this study is gasoline because it is easily evaporated and homogeneously mixed with air. For this fuel, the engine operating condition is varied from 0.2 to 0.5 of the fuel-air equivalence ratios. For each equivalence ratio, the intake air temperature is varied from 373 K to 433 K. Combustion characteristics are evaluated from burn duration of fuel based on the different combinations of equivalence ratios and intake temperatures.

The four-stroke engine model is developed under Matlab/Simulink® for numerical simulation. The parameters, engine geometries and valve timing layout are adopted from existing spark ignition engines. Modification is made on the ignition method to suit the combustion behavior of an HCCI engine. This study focuses on the developing HCCI engine model based on the thermodynamic equations of an engine with some assumptions made on the changing characteristics of fuel-air mixture inside the combustion chamber and no throttle body effect during wide open throttle condition. The simulation results are validated with the experimental data from the literature.

## 1.6 Thesis Organization

The details of this thesis are structured in six chapters. Chapter 1 is the Introduction. This chapter explains problem statement, objectives and scope of this study. Chapter 2 is the Literature Review. It gives fundamental of HCCI engine processes, theory of HCCI engine modeling and reviews of previous researches related to this study. Chapter 3 is the Research Methodology. This chapter describes the method used to develop the numerical HCCI engine model and to simulate the model for performance prediction. Chapter 4 is the Numerical Engine Development. It describes the model development including theory of each component in details, procedure for data validation and procedure of the simulation program. Chapter 5 is the Results and Discussions. In this chapter, model validation is done by comparing the simulated data and the experimental data. The combustion characteristics and engine performance are discussed. The last chapter, Chapter 6, is the Conclusion and Recommendation where this research work is concluded and suggestions for future research are included.



## REFERENCES

- Alkidas, A. C. (2007). Combustion Advancements in Gasoline Engines, *Energy Conversion and Management* 48, Page 2751–2761.
- Angelos, J. P. (2009, June). Fuel Effects in HCCI Engine. PhD Theses. Massachusetts Institute of Technology.
- Bauer, H. and Bosch, R. (2011). *Automotive Handbook* (5th ed.). Michigan: Robert Bosch GmbH, 2000.
- Bayraktar, H. (2003). Mathematical Modeling of Spark Ignition Engine Cycles. *Energy Resources, Part A: Recovery, Utilization, and Environmental Effects* 25(7), 651-666.
- Bengtsson, J., Gafvert, M. and Strandh, P. (2004a). Modeling of HCCI Engine Combustion for Control Analysis. *IEEE Conference on Decision and Control*, 1682-1687.
- Bengtsson, J., Strandh, P., Johansson, R., Tunestal, P. and Johansson, B. (2004b). Closed-Loop Combustion Control of Homogeneous Charge Compression Ignition (HCCI) Engine Dynamics. *International Journal of Adaptive Control and Signal Processing* 18, 167-179.
- Blair, G. P. (1996). *Design and Simulation of Two Stroke Engine*. Society of Automotive Engineers.
- Bogemann, S. R. (2009, December). Control Design for Disturbance Rejection on a HCCI Model.
- Caton, J. A. and Heywood, J. B. (1981). An Experimental and Analytical Study of Heat Transfer in an Engine Exhaust Port. *International Journal of Heat Mass Transfer* 24(4), 581-595.
- Chen, R. and Milovanovic, N. (2002). A Computational Study into The Effect of Exhaust Gas Recycling on Homogeneous Charge Compression Ignition Combustion in Internal Combustion Engines Fuelled with Methane. *International Journal of Thermal Sciences* 41, 805-813.
- Christie, M. A., Glimm, J., Grove, J. W., Higdon, D. M., Sharp, D. H., and Wood-Schultz, M. M. (2005). Error Analysis and Simulations of Complex Phenomena. *Las Alamos Science* (29), 6-26.
- Duret, P., Dabadie, J.C., Lavy, J., Allen, J., Blundell, D., Oscarsson, J., Emanuelsson, G., Perotti, M., Kenny, R. and Cunningham, G. (2000). The Air Assisted Direct Injection ELEVATE Automotive Engine Combustion System. SAE Paper No. 2000-01-1899.

- Erlandsson, O. (2002). Early Swedish Hot-Bulb Engines - Efficiency and Performance Compared to Contemporary Gasoline and Diesel Engines. SAE Paper No. 2002-01-0115.
- Fathi, M., Saray, R. K. and Checkel, M.D. (2011). The influence of exhaust gas recirculation (EGR) on combustion and emissions of n-heptane/natural gas fueled homogeneous charge compression ignition (HCCI) engines. Applied Energy 88, 4719-4724.
- Ferguson, C. R. (1986). Internal Combustion Engine, Applied Thermosciences. John Wiley & Sons.
- Flowers, D. L., Aceves, S. M., Martinez-Frias, J. and Dibble, R. W. (2002). Prediction of Carbon Monoxide and Hydrocarbon Emissions in Iso-Octane HCCI Engine Combustion Using Multizone Simulations. Proceedings of the Combustion Institute (29), Page 687-694.
- Ghidella, J. (2012, September). SIMULINK: Simulation and Model-Based Design. Retrieved June 14, 2013, from MathWorks Web site: <http://www.mathworks.com/products/simulink/>
- Guo, H., Neil, W. S., Chippior, W, Li, H. and Taylor, J. D. (2010). An Experimental and Modeling Study of HCCI Combustion Using n-Heptane. Journal of Engineering for Gas Turbines and Power, Page 1-10.
- Gupta, H. N. (2006). Fundamentals of Internal Combustion Engines. New Delhi: Prentice Hall of India.
- Gussak, L. A. (1975). High Chemical Activity of Incomplete Combustion Products and a Method of Prechamber Torch Ignition for Avalanche Aviation of Combustion in Internal Combustion Engines. SAE Paper No. 750890.
- Guzzella, L. and Christopher, O. H. (2009). Introduction to Modeling and Control of Internal Engine Combustion System. Zurich: Springer.
- Haroldsson, G., Hyvonen, J., Tunestal, P. and Johansson, B. (2004). HCCI Closed-Loop Combustion Control Using Fast Thermal Management. SAE Paper 2004-01-0943.
- Haroldsson, G., Tunestal, P., Johansson, B. and Hyvonen, J. (2003). HCCI Combustion Phasing with Closed-loop Combustion Control Using Variable Compression Ratio in a Multi-Cylinder Engine. SAE Paper.
- Heywood, J. B. (1988). Internal Combustion Engine Fundamentals. McGraw-Hill.
- Hyvonen, J., Haraldsson, G. and Johansson, B. (2003). Supercharging HCCI to Extend the Operating Range in Multi-Cylinder VCR HCCI Engine. SAE Paper.

- Iida, N. (1997). Alternative Fuels and Homogeneous Charge Compression Ignition Combustion Technology. SAE Paper.
- Iida, N. and Igarashi, T. (2000). Auto-ignition and combustion of n-butane and DME/air mixtures in a homogeneous charge compression ignition engine. SAE Paper No. 2000-01-1832.
- Ishibashi, Y., Nishida, K. and Asai, M. (2001). Activated Radical Combustion in High Speed High Power Pneumatic Direct Injection Two Stroke Engine in Duret P, A New Generation of Engine Combustion Processes for the Future? IFP International Seminar, Rueil-Malmaison, France, Editions Technip.
- Ishibashi, Y. and Asai, M. (1996). Improving the Exhaust Emission of Two-Stroke Engines by Applying the Activated Radical Concept. SAE Paper.
- Jennische, M. (2003). Closed-loop Control of Start of Combustion in a Homogeneous Charge Compression Ignition Engine. M.Sc. Thesis, Lund Institute of Technology.
- Johansson, B. (2007). Homogeneous Charge Compression Ignition: The Future of IC Engines? International Journal of Vehicle Design, 44 (1-2), 1-19.
- Johansson, R., Tunestal, P. and Widd, A. (2010). Modeling and Model-Based Control of Homogeneous Charge Compression Ignition (HCCI) Engine Dynamics. In L. D. Re, Automotive Model Predictive Control: Models, Methods and Applications (pp. 89-104). Springer.
- Kirkpatrick, A. (2006, November). Engine Thermodynamic: A Slider Crank Model. Retrieved June 2, 2013, from CSU Engine Web Pages: <http://www.engr.colostate.edu/~allan/thermo/page2/page2.html>
- Kitamura, T., Ito, T., Senda, J. and Fujimoto, H. (2003). Soot Kinetic Modeling and Empirical Validation of Smokeless Diesel Combustion with Oxygenated Fuels. SAE Paper .
- Koch, C. R. and Shahbakhti, M. (2010). Physic Based Control Oriented Model for HCCI Combustion Timing. Journal of Dynamic Systems, Measurement, and Control, 1-12.
- Lee, W., Park, S. and Sunwoo, M. (2004). Towards a Seamless Development Process for an Automotive Engine-control System. Control Engineering Practice, 977-986.
- Li, Y. F., Zhao, H., Brouzos, N. and Ma, T. (2006). Effect of Injection Timing on Mixture and CAI Combustion in a GDI Engine with an Air-assisted Injector. SAE Paper.
- Machrafi, H. and Cavadiasa, S. (2008). An Experimental and Numerical Analysis of the Influence of the Inlet Temperature, Equivalence Ratio and Compression Ratio on the HCCI Auto-ignition Process of Primary

Reference Fuels in an Engine. Fuel Processing and Technology 89, 1218-1226.

Maiwald, O., Schiebl, R. and Maas, U. (2004). Investigations using laser diagnostics and detailed numerical modeling of the ignition in an HCCI engine. International Symposium fur Verbrennungstechnik, Baden-Baden.

Marriott, C. D. and Reitz, R. D. (2002). Experimental Investigation of Direct Injection-gasoline for Premixed Compression Ignited Combustion Phasing Control. SAE Paper.

Martinez-Frias, J., Aceves, S. M., Flowers, D. L., Smith, J. R. and Dibble, R. (2000). HCCI Engine Control By Thermal Management. SAE Paper No. 2000-01-2869.

Martinez-Frias, J., Aceves, S. M., Smith, J. R. and Dibble, R. W. (2001). Equivalence Ratio-EGR Control of HCCI Engine Operation and the Potential for Transition to Spark-Ignited Operation. SAE Paper No. 2001-01-3613.

Maurya, R. K. and Agarwal, A. K. (2009). Experimental Investigation of the Effect of the Intake Air Temperature and Mixture Quality on the Combustion of a Methanol and Gasoline-Fueled Homogeneous Charge Compression Ignition Engine. Automobile Engineering, 2041-2091.

Najt, P.M & Foster, D.E. (1983). Compression-Ignited Homogeneous Charge Combustion. SAE Paper No. 830264.

Nedler, J. A. and Mead, R. (1965). A simplex method for function minimization. The Computer Journal (1965) 7 (4): 308-313.

Noguchi, M., Tanaka, Y., Tanaka, T., & Takeuchi, Y. (1979). A Study on Gasoline Engine Combustion by Observation of Intermediate Reactive Products during Combustion. SAE Paper No. 790840.

Olsson, J. O., Tunestal, P., Johansson, B., Fiveland, S., Agama, R. and Willi, M. (2002). Compression Ratio Influence on Maximum Load of a Natural Gas Fueled HCCI Engine. SAE Paper No. 2002-01-0111.

Onishi, S., Jo, S. H., Shoda, K., Jo, P. D. and Kato, S. (1979). Active Thermo-Atmosphere Combustion (ATAC) A New Combustion Process for Internal Combustion Engines. SAE Paper No. 790501.

Rausen, D. J. and Stefanopoulou, A. G. (2005). A Mean-value Model for Control of Homogeneous Charge Compression Ignition (HCCI) Engines. Journal of Dynamic Systems, Measurement and Control, 127, 355-362.

Shahbakhti, M. and Koch, C. R. (2007). Control Oriented Modeling of Combustion Phasing for an HCCI Engine. Proceeding of American Control Conference.

- Shahbakti, M. (2009). Modeling and Experimental Study of HCCI Engine for Ignition Combustion Control. PhD Thesis.
- Shaver, G. M. and Gerdes, J. C. (2003). Cycle-to-cycle control of HCCI engines. ASME International Mechanical Engineering Congress and Exposition, (pp. IMECE2003-41966). Washington, DC.
- Shaver, G. M., Roelle, M. and Gerdes, C. (2005). Decoupled Control of Combustion Timing and Work Output in Residual-Affected HCCI Engines. Proceedings of American Control Conference, Portland, OR , 3871-3876.
- Sherazi, H. I. and Li, Y. (2010). Homogeneous Charge Compression Ignition Engine: A Technical Review. International Conference on Automation & Computing, University of Huddersfield, 315-320
- Sjoberg, M. and Dec, J. E. (2005). An Investigation into Lowest Acceptable Combustion Temperatures for Hydrocarbon Fuels in HCCI Engines. Proceedings of the Combustion Institute (30), 2719-2726.
- Stone, R. (1999). Introduction to Internal Combustion Engines (3rd ed.). New York: MacMillan.
- Stone, R. and Ball, J. K. (2004). Automotive Engineering Fundamentals . SAE International.
- Swan, K., Shahbakhti, M. and Koch, C. R. (2006). Predicting Start of Combustion Using a Modified Knock Integral Method for an HCCI Engine. SAE Paper No.2006-01-1086.
- Taylor, A. M. (2008). Science Review of Internal Combustion Engines. Energy Policy, 4657-4667.
- Thring, R. H. (1989). Homogeneous Charge Compression Ignition (HCCI) Engines. SAE Paper No. 892068.
- U.S. Congress, R. (2001). Homogeneous Charge Compression Ignition (HCCI) Technology. Technical Report.
- Weeks, R. W. and Moskwa, J. J. (1995). Automotive Engine Modeling for Real-Time Control Using Matlab/Simulink. SAE Paper 950417, 1-15.
- Woschni, G. (1967). A Universally Applicable Equation for Instantaneous Heat Transfer Coefficient in the Internal Combustion Engine. SAE Technical Papers 670931.
- Yao, M., Zheng, Z. and Liu, H. (2009). Progress and Recent Trends in Homogeneous Charge Compression Ignition (HCCI) Engines. Progress in Energy dan Combustion Science 35, 398-437.

Yap, D., Wyszynski, M. L., Megaritis, A. and Xu, H. (2005). Applying Boosting to Gasoline HCCI Operation With Residual Gas Trapping. SAE Paper No. 2005-01-2121.

Zhao, H. (2007). Homogeneous Charge Compression Ignition (HCCI) and Controlled Auto Ignition (CAI) Engines for the Automotive Industry. Brunel University UK: Wood-head Publishing Ltd.

Zhu, G. and Haskara, I. W. (2005). Stochastic Limit Control and its Application to Spark Limit Control using Ionization Feedback. American Control Conference, Portland, OR, USA, 5027-5034.

