



UNIVERSITI PUTRA MALAYSIA

VIBRATION-INDUCED STRESS ANALYSIS OF NATURAL GAS VEHICLE

SITI MARHAINIS BINTI ABU MANSOR

FK 2008 58



VIBRATION-INDUCED STRESS ANALYSIS OF NATURAL GAS VEHICLE

By
SITI MARHAINIS BINTI ABU MANSOR

Thesis Submitted to the School of Graduate Studies, Universiti Putra Malaysia, in
Fulfilment of the Requirement for the Degree of Master of Science
June 2008



Abstract of thesis presented to the senate of Universiti Putra Malaysia in fulfilment of the requirements for the degree of Master of Science.

VIBRATION-INDUCED STRESS ANALYSIS OF NATURAL GAS VEHICLE

By

SITI MARHAINIS BINTI ABU MANSOR

June 2008

Chairman: Professor Ir. Barkawi Bin Sahari, PhD

Faculty: Faculty of Engineering

The automotive industry has been exploring alternative vehicle fuel for decades as petrol reserve for the future is reducing. Natural gas is found to be the most suitable alternative choice, but the natural gas storage tank that is to be located in the vehicle requires specific space. Thus, a dedicated natural gas vehicle platform is designed and during the initial design stage of vehicle platform, the study of the self-excited vibration and the affected stress to the vehicle platform structure were analyzed.

There have been little studies about the effects of the vehicle structure natural frequency to the structural stress. Vibration is known as a source of energy that induces structural and mechanical oscillations, self-excited vibration is an unwanted occurrence. Other than resonance, high stresses caused structural failure thus their values are investigated.

In this research, there are three models of compressed natural gas (CNG) vehicle platforms designed from the modification of the conventional petrol fuelled



PROTON Waja's vehicle platform and they are CNG 3T, CNG 4T and CNG 5T Platforms. Finite element analyses were done to these platforms models with the conventional petrol fuelled platform being the benchmark platform.

The modal analysis in searching for the natural frequency values below 50Hz are performed first and the induced stresses due to the natural frequency mode shape deformation is determined through static analysis. The frequencies, mode shape and vibration-induced stress results for all the analyzed platforms are presented.

The analysis results showed that the CNG 3T, CNG 4T and CNG 5T Platforms have a maximum stress of 53.3MPa, 36.0MPa and 43.9MPa accordingly when induced by natural vibrations of frequencies below 50Hz. The maximum stresses are below the yield stress of the applied material. The natural vibration mode shape have been identified to be the main factor of the induced stresses, while the platform's geometry has affected the natural vibration frequency values as the modifications made has increased the platform's stiffness.

However, the relationship between frequency and the induced stress could not be determined due to the inability to predict the natural vibration mode shape that has been the main factor of the vibration-induced stress analysis. Nevertheless, the results obtained will serve as a base for future vibration-induced stress study to structures.

Abstrak tesis yang dikemukakan kepada Senat Universiti Putra Malaysia sebagai memenuhi keperluan untuk ijazah Master Sains

**ANALISIS TEGASAN SEBAGAI HASIL GETARAN KENDERAAN GAS
ASLI**

Oleh

SITI MARHAINIS BINTI ABU MANSOR

Jun 2008

Pengerusi: Professor Ir. Barkawi Bin Sahari, PhD

Fakulti: Fakulti Kejuruteraan

Memandangkan sumber petroleum sebagai bahan bakar kenderaan semakin berkurangan, industri automotif giat mencari bahan bakar alternatif sejak berabad lamanya. Gas asli dipersetujui sebagai bahan bakar kenderaan yang paling sesuai. Namun begitu, tangki penyimpanan gas asli memerlukan ruangan khusus di dalam kenderaan. Maka, lantai kenderaan gas asli khusus direka dan di peringkat awal rekaan, penyiasatan ke atas getaran tabii lantai kenderaan dan penghasilan tegasan daripada getaran tabii tersebut dilakukan.

Akibat daripada getaran tabii struktur kenderaan kepada tegasan tidak banyak dibincangkan. Namun getaran yang diketahui sebagai sumber tenaga dan pengayunan menyebabkan getaran tabii tidak diingini. Selain daripada salunan, nilai tegasan yang tinggi juga akan mengakibatkan kegagalan sesebuah struktur.

Pada penyiasatan ini, tiga buah model lantai kenderaan gas asli telah direka berdasarkan lantai kenderaan yang menggunakan bahan bakar petroleum keluaran



PROTON Berhad, iaitu Waja dan rantai kenderaan tersebut ialah rantai CNG 3T, CNG 4T dan CNG 5T. Analisis elemen tidak terhingga dilakukan ke atas kesemua model rantai tersebut dan rantai kenderaan yang menggunakan bahan bakar petroleum menjadi nilai tara yang dirujuk.

Analisis ragam telah dilaksanakan bagi menentukan nilai frekuensi tabii di bawah 50 Hz. Seterusnya, nilai tegasan hasil daripada getaran yang diperolehi, didapati dari analisis statik. Nilai frekuensi, bentuk mode dan nilai tegasan hasil daripada getaran untuk kesemua model rantai diperolehi dan dibincangkan.

Daripada keputusan yang diperolehi menunjukkan rantai CNG 3T, CNG 4T dan CNG 5T menghasilkan tegasan maksimum iaitu 53.3MPa, 36.0MPa dan 43.9MPa masing-masing apabila rantai-rantai tersebut bergetar dengan nilai frekuensi kurang daripada 50 Hz. Nilai tegasan maksimum tersebut adalah jauh lebih rendah daripada nilai tegasan bagi bahan yang digunakan. Selain itu, geometri yang berbeza dikenalpasti sebagai punca perbezaan nilai frekuensi rantai gas asli rekaan berbanding nilai tara yang dirujuk kerana peningkatan nilai kekakuan rantai.

Walaupun bagaimanapun, perkaitan antara nilai frekuensi dengan tegasan yang terhasil tidak dapat dipastikan kerana bentuk ragam yang menjadi faktor utama penghasilan tegasan tidak dapat diramalkan. Namun begitu, segala keputusan yang diperolehi dapat dijadikan asas kepada kajian ke atas tegasan sebagai hasil getaran struktur kenderaan di masa akan datang.

ACKNOWLEDGEMENTS

I would like to express my sincere gratitude and deep thanks to my supervisor, Professor Ir. Dr. Barkawi Bin Sahari for his kind assistance, support, advice, encouragements and suggestions throughout this work and during the preparation of this thesis.

I would also like to express my appreciation to Associate Professor Dr. Wong Shaw Voon for his suggestions and constructive criticisms given at different stages of this study.

My heartfelt appreciation also goes to all my colleagues for their useful ideas and critical but constructive comments to work on. Our fruitful discussions would never go unmentioned.

Finally, I would like to express my indebtedness to my family for their moral support through this long journey.



I certify that an Examination Committee met on 26th June 2008 to conduct the final examination of Siti Marhainis Binti Abu Mansor on her Master of Science thesis entitled “Vibration-Induced Stress Analysis of Natural Gas Vehicle” in accordance with the Universiti Pertanian Malaysia (Higher Degree) Act 1980 and Universiti Pertanian Malaysia (Higher Degree) Regulations 1981. The Committee recommends that the student be awarded the degree of Master of Science.

Members of the Examination Committee are as follows:

Ir. Desa Ahmad, PhD

Professor
Faculty of Engineering
Universiti Putra Malaysia
(Chairman)

Tang Sai Hong, PhD

Lecturer
Faculty of Engineering
Universiti Putra Malaysia
(Internal Examiner)

Nawal Aswan Abdul Jalil, PhD

Lecturer
Faculty of Engineering
Universiti Putra Malaysia
(Internal Examiner)

Mohd Jailani Mohd Nor, PhD

Professor
Faculty of Engineering
Universiti Kebangsaan Malaysia
(External Examiner)

HASANAH MOHD GHAZALI, PhD

Professor and Deputy Dean
School of Graduate Studies
Universiti Putra Malaysia

Date:



This thesis was submitted to the senate of Universiti Putra Malaysia and has been accepted as fulfilment of the requirement for the degree of Master of Science. The members of the Supervisory Committee were as follows:

Ir. Barkawi Bin Sahari, PhD

Professor
Faculty of Engineering
Universiti Putra Malaysia
(Chairman)

Wong Shaw Voon, PhD

Associate Professor
Faculty of Engineering
Universiti Putra Malaysia
(Member)

AINI IDERIS, PhD

Professor and Dean
School of Graduate Studies
Universiti Putra Malaysia

Date: 13 November 2008



DECLARATION

I declare that the thesis is based on my original work except for the quotations and citation which have been duly acknowledged. I also declare that it has not been previously and is not concurrently submitted for any other degree at UPM or at any other institutions.

Siti Marhainis Binti Abu Mansor

Date:



TABLE OF CONTENTS

	Page
ABSTRACT	ii
ABSTRAK	iv
ACKNOWLEDGEMENTS	vi
APPROVAL	vii
DECLARATION	ix
LIST OF TABLES	xiv
LIST OF FIGURES	xvi
LIST OF ABBREVIATIONS	xxii
CHAPTER	
1 INTRODUCTION	1
1.1 Research Objectives	3
1.2 Significance of the Study	3
1.3 Thesis Layout	4
2 LITERATURE REVIEW	5
2.1 Introduction	5
2.2 Natural Gas Vehicle	5
2.3 Vehicle Body Structure	7
2.4 Vehicle Body Structure Analysis	12
2.4.1 Dynamic Analysis	13
2.4.2 Allowable Stress	15
2.5 Finite Element and Theoretical Analysis of Vehicle Body Structure	16
2.6 Vehicle Platform Structure	27
2.6.1 PROTON Waja's Platform	29
2.7 Vehicle Platform Structure Vibration Analysis	30
2.7.1 Rectangular Plate Analysis	31
2.7.2 Bending Vibration of Thin Plates	34
2.7.3 Free Vibration of the Rectangular Plate	36
2.7.4 The Simply Supported Plate	37
2.8 Vibration-induced Stress	39
2.9 Discussion	45



3	METHODOLOGY	47
	3.1 Introduction	47
	3.2 Flow of the Project	48
	3.3 Data Collection and Design Specifications	50
	3.4 CAD Model Development	51
	3.4.1 Waja Platform	52
	3.4.2 CNG 3 Tanks (CNG 3T)	57
	3.4.3 CNG 4 Tanks (CNG 4T)	60
	3.4.4 CNG 5 Tanks (CNG 5T)	62
	3.5 Finite Element Analysis	65
	3.5.1 Pre-processing	65
	3.6 Post-processing	76
	3.7 Results and Reporting	76
	3.8 Discussion	76
4	RESULT AND DISCUSSION	78
	4.1 Introduction	78
	4.2 Waja Platform	79
	4.2.1 Mode Shape and Natural Frequency of Waja Platform	81
	4.2.2 Vibration-induced Stress of Waja Platform	85
	4.2.3 The Effect of Frequency on Stress for Waja Platform	90
	4.3 CNG 3T Platform	92
	4.3.1 Mode Shape and Natural Frequency of CNG 3T Platform	93
	4.3.2 Vibration-induced Stress of CNG 3T Platform	96
	4.3.3 The Effect of Frequency on Stress for CNG 3T Platform	100
	4.4 CNG 4T Platform	102
	4.4.1 Mode Shape and Natural Frequency of CNG 4T Platform	103
	4.4.2 Vibration-induced Stress of CNG 4T Platform	107
	4.4.3 The Effect of Frequency on Stress for CNG 4T Platform	112
	4.5 CNG 5T Platform	113
	4.5.1 Mode Shape and Natural Frequency of CNG 5T Platform	114
	4.5.2 Vibration-induced Stress of CNG 5T Platform	118
	4.5.3 The Effect of Frequency on Stress for CNG 5T Platform	123



4.6	Verification of The Method	125
4.7	Validation of The Work	129
4.7.1	x, y and z-direction Constraint	130
4.7.2	x, and y-direction Constraint	132
4.8	Discussion	134
4.8.1	The Effects of Geometry on Frequency	135
4.8.2	The Effects of Geometry on Stress-induced Vibration	139
4.9	Conclusion	142
5	CONCLUSION	144
	REFERENCES	148
	APPENDICES	151
	BIODATA OF THE STUDENT	154
	LIST OF PUBLICATIONS	155



LIST OF TABLES

Table		Page
2.1	Theoretical and experimental natural frequencies of chassis frame in Hz (Nossier and Dickinson, 1971)	18
2.2	Theoretical and experimental natural frequencies of the underbody (Nossier and Dickinson, 1971)	19
2.3	Natural frequencies of the complete body model in; (a)bending, (b)torsion (Nossier and Dickinson, 1971)	19
2.4	Comparison between theory and experiment (Jin, 1999)	22
2.5	The frequency values range for each mode for each size mesh (Totonji, 2003)	26
2.6	Maximum stress values (Totonji, 2003)	27
2.7	Comparison between natural frequencies of simply supported plate predicted using different method (Park, Seigmund and Mongeau, 2003)	33
3.1	Designed natural gas vehicle basic specifications	51
3.2	Vehicle body front floor parts	55
3.3	Vehicle body rear floor parts	55
3.4	Finite element mesh parameters	67
3.5	Properties of assigned material	69
4.1	Result obtained for the simply supported Waja platform	80
4.2	Result obtained for the simply supported CNG 3T platform	92
4.3	Result obtained for the simply supported CNG 4T platform	102
4.4	Result obtained for the simply supported CNG 5T platform	113



4.5	Comparison between theoretical and analysis, frequency values of simply supported plate	126
4.6	The first three natural frequency values for CNG 3T platform and simple flat plate of x, y and z-direction constraint boundary condition	130
4.7	The first three natural frequency values for CNG 3T platform and simple flat plate of x, and y-direction constraint boundary condition	132
4.8	Deformation areas of the analyzed platforms of the frequencies below 50 Hz	136



LIST OF FIGURES

Figure		Page
2.1	Typical vehicle body structure – composite construction (Halderman and Mitchell, 2000)	8
2.2	Basic ladder frame channel sections (Halderman and Mitchell, 2000)	8
2.3	Cruciform frame (Halderman and Mitchell, 2000)	9
2.4	An early ladder frame with cruciform (Halderman and Mitchell, 2000)	9
2.5	Typical torsion tube frame (Halderman and Mitchell, 2000)	10
2.6	Space chassis frame (Halderman and Mitchell, 2000)	10
2.7	Integral body structure (Halderman and Mitchell, 2000)	11
2.8	Chassis frame model (Nossier and Dickinson, 1971)	17
2.9	Underbody model (Nossier and Dickinson, 1971)	17
2.10	Model of a complete body (Nossier and Dickinson, 1971)	18
2.11	Natural vibration of four-door sedan (two dimensional built-in body freely supported) (Miki et.al, 1969)	21
2.12	Natural vibration of four-door sedan (three dimensional built-in body freely supported) (Miki et.al, 1969)	21
2.13	Modal analysis at frequency of 36.532 Hz (Jin, 1999)	23
2.14	Modal analysis at frequency of 43.995 Hz (Jin, 1999)	23
2.15	Modal analysis at frequency of 47.377 Hz (Jin, 1999)	24
2.16	Torsional stiffness analysis result (Kridli et al., 2002)	25
2.17	Bending stiffness analysis result (Kridli et al., 2002)	25



2.18	Modal analysis result (Kridli et al., 2002)	25
2.19	PROTON Waja Vehicle (Waja Performance Club, 2002)	29
2.20	PROTON Waja platform (courtesy of PROTON Berhad)	30
2.21	Kinematics of thin plate deformation (Geradin and Rixen,1997)	34
2.22	Simply supported rectangular plate (Geradin and Rixen, 1997)	37
2.23	Typical representation of the different mode shape of the simply supported rectangular plate, $b= (\frac{3}{4})a$ (Geradin and Rixen, 1997)	39
3.1	Methodology flow chart	49
3.2	CAD model of Waja vehicle platform (courtesy of PROTON Berhad)	52
3.3	Waja vehicle platform front floor	53
3.4	Exploded view of Waja vehicle platform front floor	53
3.5	Waja vehicle platform rear floor	54
3.6	Exploded view of Waja vehicle platform rear floor	54
3.7	Waja platform without the reinforcements	56
3.8	Side view of tank location for the 3T vehicle platform	57
3.9	The passenger seat part	58
3.10	Rear floor development for CNG 3T platform	59
3.11	CNG 3T platform without reinforcement	59
3.12	Side view of tank location for the CNG 4T vehicle	60
3.13	Front floor development for the CNG 4T platform	61
3.14	CNG 4T platform without reinforcements	62



3.15	Side view of tank location for the CNG 5T vehicle	63
3.16	Front view of tank location for the CNG 5T vehicle	63
3.17	Front floor development for the CNG 5T	64
3.18	CNG 5T platform without reinforcements	64
3.19	One of the designed CNG platforms (CNG 5T) mesh example.	68
3.20	Example of spot-weld (RBAR) representation viewed in HYPERMESH.	70
3.21	Platform with simply supported (Δ^{123}) along the platform edges.	71
3.22	Part of bulk data formatted (.bdf) file for normal mode analysis	72
3.23	Part of .rpt file showing the z-displacement when the system vibrates with frequency of 33.51 Hz.	73
3.24	Part of bulk data formatted (.bdf) file for prescribed displacement static analysis	75
4.1	Frequency values and its corresponding maximum induced stress of Waja platform	81
4.2	First mode shape of Waja platform (Frequency = 33.51 Hz)	82
4.3	Second mode shape of Waja platform (Frequency = 34.32 Hz).	83
4.4	Third mode shape of Waja platform (Frequency = 41.16 Hz)	83
4.5	Fourth mode shape of Waja platform (Frequency = 43.34 Hz)	84
4.6	Fifth mode shape of Waja platform (Frequency = 44.64 Hz)	85
4.7	Stress distribution of the first mode shape of Waja platform (Frequency = 33.51 Hz, Maximum Von Mises = 31.9MPa).	86
4.8	Stress distribution of the second mode shape of Waja platform (Frequency = 34.31 Hz, Highest VonMises = 25.7MPa)	87



4.9	Stress distribution of the third mode shape of Waja platform (Frequency = 41.16 Hz, Highest Von Mises = 20.5 MPa)	88
4.10	Stress distribution of the fourth mode shape of Waja platform (Frequency = 43.34 Hz, Highest VonMises = 52.1 MPa).	89
4.11	Stress distribution of the fifth mode shape of Waja platform (Frequency = 44.64 Hz, Highest Von Mises = 35.3 MPa)	90
4.12	The relations of frequency and its induced stress for Waja platform	91
4.13	Frequency values and its corresponding maximum induced stress of CNG 3T platform.	93
4.14	First mode shape of CNG 3T platform (Frequency = 33.63 Hz)	94
4.15	Second mode shape of CNG 3T platform(Frequency =34.37Hz)	94
4.16	Third mode shape of CNG 3T platform (Frequency = 44.57 Hz)	95
4.17	Fourth mode shape of CNG 3T platform(Frequency= 49.00Hz).	96
4.18	Stress distribution of the first mode shape of CNG 3T platform (Frequency = 33.63 Hz, Highest Von Mises = 32.2 MPa)	97
4.19	Stress Distribution of the 2 nd Mode Shape of CNG 3T Platform (Frequency = 34.36 Hz, Highest VonMises = 25.8 MPa)	98
4.20	Stress distribution of the third mode shape of CNG 3T platform (Frequency = 44.57 Hz, Highest Von Mises = 53.2 MPa)	99
4.21	Stress distribution of the fourth mode shape of CNG 3T platform (Frequency = 49 Hz, Highest Von Mises = 34.7 MPa)	100
4.22	The relations of frequency and its induced stress for CNG 3T platform.	100
4.23	Frequency values and its corresponding maximum induced stress of CNG 4T platform.	103
4.24	First mode shape of CNG 4T platform (Frequency = 33.29 Hz)	104



4.25	Second mode shape of CNG 4T platform(Frequency=35.23Hz).	104
4.26	Third mode shape of CNG 4T platform(Frequency = 40.79 Hz).	105
4.27	Fourth mode shape of CNG4T platform(Frequency =46.08 Hz).	106
4.28	Fifth mode shape of CNG4T platform (Frequency = 49.81 Hz)	106
4.29	Stress distribution of the first mode shape of CNG 4T platform (Frequency = 33.29 Hz, Highest VonMises = 35.0MPa)	107
4.30	Stress distribution of the second mode shape of CNG 4T platform (Frequency = 33.29 Hz, Highest VonMises=36.0MPa)	108
4.31	Stress distribution of the third mode shape of CNG 4T platform (Frequency = 40.79 Hz, Highest VonMises = 21.0 MPa)	109
4.32	Stress distribution of the fourth mode shape of CNG 4T platform (Frequency = 46.08 Hz, Highest VonMises=33.0MPa)	110
4.33	Stress distribution of the fifth mode shape of CNG 4T platform (Frequency = 49.8 Hz, Highest VonMises = 26.0MPa)	111
4.34	The relations of frequency and its induced stress for CNG 4T platform.	112
4.35	Frequency values and its corresponding maximum induced stress of CNG 5T platform	114
4.36	First mode shape of CNG 5T platform (Frequency = 32.71 Hz)	115
4.37	Second mode shape of CNG 5T platform (Frequency =40.7Hz).	115
4.38	Third mode shape of CNG 5T platform (Frequency = 42.79 Hz)	116
4.39	Fourth mode shape of CNG 5T platform (Frequency=44.56 Hz)	117
4.40	Fifth mode shape of CNG 5T platform (Frequency = 49.19 Hz)	117
4.41	Stress distribution of the first mode shape of CNG 5T platform (Frequency = 32.70 Hz, Highest VonMises = 30.7MPa)	119



4.42	Stress distribution of the second mode shape of CNG 5T platform (Frequency = 40.69 Hz, Highest VonMises=31.6MPa)	120
4.43	Stress distribution of the third mode shape of CNG 5T platform (Frequency = 42.79 Hz, Highest VonMises = 34.4 MPa)	121
4.44	Stress distribution of the fourth mode shape of CNG 5T platform (Frequency = 44.56 Hz, Highest VonMises=43.9MPa)	122
4.45	Stress distribution of the fifth mode shape of CNG 5T platform (Frequency = 49.2 Hz, Highest VonMises = 29.5 MPa)	123
4.46	The relations of frequency and its induced stress for CNG 5T platform.	124
4.47	Flat rectangular plate mode shape from normal mode analysis; (a) Top view, (b) Side view.	127
4.48	Flat rectangular displacement from prescribed displacement static analysis; (a) Top view, (b) Side view.	127
4.49	The comparison displacement obtained in normal modes analysis and static analysis.	128
4.50	Stress distribution from prescribed displacement static analysis; maximum stress value = 2.00×10^{-4} N/m.	128
4.51	The geometry of (a) CNG 3T platform; (b) Simple flat plate	129
4.52	The first three natural frequency mode shape for CNG3T platform and the simple flat plate of x, y and z-direction constraint boundary condition	131
4.52	The first three natural frequency mode shape for CNG3T platform and the simple flat plate of x and y-direction constraint boundary condition	133
4.54	Top view of Waja vehicle platform.	135
4.55	Frequency curve of all platforms models in the study.	136
4.56	The relations of frequency and its induced stress for all analyzed platform models. (Yield stress = 210 MPa)	136





LIST OF ABBREVIATIONS

NGV	Natural gas vehicle
MOSTI	Ministry of Science, Technology and Innovation of Malaysia
PROTON	Perusahaan Otomobil Nasional Berhad
CNG	Compressed natural gas
CAE	Computer aided engineering
VLFS	Very large floating structures
LSFD	Least square-based finite difference
MDOF	Multi degree-of-freedom
CAD	Computer aided design
FEA	Finite element analysis
CNG 3T	Compressed natural gas vehicle with three tanks
CNG 4T	Compressed natural gas vehicle with four tanks
CNG 5T	Compressed natural gas vehicle with five tanks
M_x	Resultant moment in x-direction
M_y	Resultant moment in y-direction
E	Young's Modulus
D	Plate stiffness
ρ	Density
ν	Poisson's ratio
h	Thickness of plate
ω	Angular frequency
M, m	Mass
K, k	Stiffness
x	Displacement
\ddot{x}	Acceleration
T	Kinetic energy
U	Potential energy
σ	Direct stress
ε	Direct strain



τ Shear stress
 γ Shear strain



CHAPTER 1

INTRODUCTION

Vibration is a source of energy that can induce structural and mechanical oscillations to structures and self-excited vibration of structures due to natural frequency is an undesirable phenomenon (Singiresu, 1995). Since the fatigue life of most material is proportional to the stress occurrence (Geradin, 1997), there is a need in understanding the role of self-excited vibration that induces stress as a result of the structure vibration oscillations.

The study of stress-induced vibration of vehicle structure is important to predict the strength and durability of the vehicle structure in the design stage. So far, there has been little studies about the effects of vibration of the vehicle to the structural stress. Several studies have produced accountable results in obtaining the vehicle's natural frequency through the modal analysis, but there is still insufficient data for the effects of the vibration mode shape deformation to the stress of the vehicle structure.

Most of the studies in the modal analysis of a vehicle structure have only focused in obtaining the natural frequency and its mode shape and not the structural stress as a result of vibration especially at the fundamental frequencies. Since high stresses can

