Maritime Circulation of the South China Sea: 
A Numerical Study

Alejandro Camerlengo and Monica Ines Demmler

Faculty of Fisheries and Marine Science Centre
Universiti Pertanian Malaysia
Mengabang Telipot, 21030 Kuala Terengganu, Malaysia

Received 15 April 1995

ABSTRACT
A numerical model employing the classic hydrodynamic equations of conservation of mass and momentum, vertically integrated, has been developed. The model solves the external, or barotropic, mode. The computational mode is eliminated by employing a Euler backward scheme at every N (odd) time level. A similar model is used for issuing flood warnings of hurricanes and extratropical storms. This type of model is also used in a variety of situations such as oil spill simulations, storm surges, tsunamis, and tidal simulations. The aim of this investigation is to gain some insight into the circulation of the South China Sea during the NE and SW monsoon seasons. Thus the circulation of the Malaysian EEZ has been simulated. Our results compare well with Wyrtki’s (1961) observations.

Keywords: circulation, Malaysian EEZ, numerical simulation, barotropic mode
INTRODUCTION

Coastal oceanography is a continually expanding field. Continuous demands of economic development necessitate the investigation of the physical principles involved in coastal circulation. Knowledge of coastal oceanography is also extremely useful for the planning of fisheries activities (Liew et al. 1987).

Coastal projects can severely modify the existing hydro-dynamic pattern. It is advisable to understand the ways in which the environment is affected by the execution of such projects so the necessary steps to preserve the ecosystem can be undertaken.

Due to increased activity on the South China Sea and the Malacca Straits over the past few years and the danger of major oil spills, Malaysian research into various aspects of containment of oil spills under adverse weather conditions, mainly due to the NE and SW monsoons, must experience a rapid growth in the near future.

The main purpose of this investigation is to accurately simulate wind-driven coastal circulation of the South China Sea (Fig. 1). For this purpose, a hydrodynamic numerical model was constructed. Problems such as oil spill simulations, circulation (due to winds and tides), tidal simulations,
volume transports, flood warning systems, nonlinear tidal interactions, energy calculations, storm surges, tsunamis, barotropic residual circulation could be readily addressed with this model.

The model used in this study is similar to the one used is the storm tide warning system for the North Sea. It operates, on a routine basis, at the Weather Service at Bracknell, UK. An identical model (the SLOSH model), warning of hurricanes for the east coast of the US, is operated by the National Weather Service.

Wyrtki (1961) made field observations of the South China Sea. As pointed out by Pohlmann (1987), no significant improvement has been achieved in the understanding of the dynamics of the South China Sea since then. Understandably, our results are compared with Wyrtki's (1961). A numerical simulation of this area was undertaken by Azmy et al. (1991). They considered the wind data of Kuala Terengganu as representative of the whole eastern coast of the Malay Peninsula. Pohlmann (1987) used a 12-layer model to simulate the circulation of the South China Sea due to the mean winter and mean summer monsoons. His numerical results compare relatively well with Wyrtki's (1961) observations.

**THE MODEL**

The model equations are the classic hydrodynamic equations of conservation of mass and momentum, vertically integrated. The model solves the external, barotropic mode. The Boussinesq approximation and the hydrostatic pressure in the vertical are assumed.

The equations for the external mode are:

\[
\frac{\partial \mathbf{V}}{\partial t} + \mathbf{V} \cdot \nabla \mathbf{V} + f \mathbf{k} \times \mathbf{V} = -g \nabla \eta + \left( \Gamma_{W} - T_{B} \right) / (\rho (H + \eta)) + A \Delta \mathbf{V} \\
\frac{\partial \eta}{\partial t} + \nabla \cdot (\mathbf{V}(H + \eta)) = 0
\]

where \( \mathbf{V} \) represents the Eulerian velocity vector. Its east-west and north-south velocity components, \( u \) and \( v \), correspond to the horizontal coordinates \( x \) and \( y \) (positive in the east and north direction, respectively); \( \nabla \) is the horizontal gradient; \( \Delta \) the Laplacian operator; \( \eta \), the free surface elevation; \( H \), the mean depth; \( f(=\beta y) \), the Rosby parameter; \( g \), the gravity's acceleration; \( \Gamma_{W} \), the wind stress; \( T_{B} \), the bottom friction; \( K \) the vertical normal vector; \( \rho \), the water density and \( A \), the horizontal coefficient of eddy diffusion.

The terms on the left-hand side of the momentum equations represent the local time derivative, the nonlinear (advective) term, and the Coriolis deflection term. The terms on the right-hand side are, respectively, the pressure gradient due to the slope of the sea surface, tangential wind stress on the sea surface, linear bottom friction, and the horizontal momentum diffusion modelled empirically by the horizontal Laplacian operator.
The bottom friction is represented by:

\[(T^X_B, T^Y_B) = R(u, v)\]

where \(R\) represents friction coefficient. A linear bottom friction is implemented.

We assume a constant density \(\rho = 1020 \text{ kg m}^{-3}\). The other constants are the Coriolis parameter \(\beta = 2.10 \text{ m}^{-1} \text{s}^{-1}\); the acceleration of gravity, \(g = 9.8 \text{ m}^2 \text{s}^{-1}\); the horizontal diffusion coefficient, \(A = 100 \text{ m}^2 \text{s}^{-1}\); and the bottom friction coefficient, \(R = 0.002\).

\(A\) is kept very small, in such a way that it will not affect the interior solutions. Thus, the order of magnitude of the Laplacian (lateral viscous terms) will be five orders of magnitude fewer than the leading terms of the momentum equations. The wind stress forcing used for this study is that of Hellerman and Rosenstein (1983).

The model extends from 99° 10'E - 109° 30'E longitude and 13° 45'N - 0° 30'S latitude. Therefore, 32 grid points are used in the east-west direction, and 29 in the north-south direction. The Cartesian grid spacing has
Dx = 37.5 km and Dy = 55.5 km. This represents a distance of 1162.5 km in the east-west direction and 1554 km in the north-south direction (Fig. 2).

Solid walls are implemented at coastal boundaries. At the open boundaries, Camerlengo and O'Brien's (1980) boundary conditions are implemented. A centred in space and time integration (leapfrog) scheme is used; this introduces no computational damping of the physical solutions of the system (Camerlengo and O'Brien 1980). It conserves mass and momentum to second order accuracy. The time step used is 300 seconds. The free surface elevation is calculated at the centre of the grid, while u is calculated at the east and west sides, and v is evaluated at the north and south sides (Arakawa and Lamb 1977).

The model starts from rest, i.e., \( u = v = \eta = 0 \). At every N (odd) time level an Euler backward (Matsuno 1966) scheme is activated. Therefore, the spurious (computational) mode is eliminated at every N time level. The value of N is set at 9. The x and y coordinates are transformed into a new coordinate system so either a regular or an irregular grid spacing can be used in either direction (Camerlengo 1982).

For the purpose of avoiding the undesirable effects of numerical inertial oscillations, the wind stress forcing is gradually increased via an hyperbolic tangent. The original bathymetry used is based on the values of the nautical chart of the British Admiralty No. 2414 and 2660A. The values taken from these charts represent an average depth for \( Dx \times Dy \) square centred on the \( \eta \) grid point (Fig. 1).

A stationary state is reached within two days in all cases being considered.

**DISCUSSION AND CONCLUSIONS**

Typical values for the length scale (\( L = 10^6 \text{ m} \)), the time scale (\( T = 10^6 \text{ sec} \)), and the velocity scale (\( U = 0.1 \text{ m sec}^{-1} \)) are used. Upon scaling the momentum equations, and because of the lower latitudes of the region under consideration, it can be shown that the dominant terms are the wind stress, Coriolis parameter and the pressure gradient. The results of our numerical simulations show a clear response of the ocean model to wind stress forcing.

A relatively short period of integration is needed to reach a steady state solution. Following Philander (1990), this short period makes the Coriolis terms play a secondary role. (Furthermore, at these latitudes, the magnitude of \( f \) is in the order of \( 10^{-5} \text{ sec}^{-1} \)). This is precisely what happens in our numerical simulations.

The numerical simulation of February, a typical month of the NE monsoon season, is analysed (Fig. 3). In accordance with Wyrtki (1961), the numerical model resolves reasonably well the northeasterly jet located along the Vietnamese coast (Fig. 4). Pohlmann (1987) located this same jet, further away from the Vietnamese coast.
Fig. 3. Model results of the circulation of February. Thicker lines represent closed boundaries; thinner lines represent open boundaries. Numbers in the abscissa represent degrees of longitude; numbers in the ordinate represent degrees of latitude.

Fig. 4. Surface currents in February, according to Wyrski (1961).
Saadon and Camerlengo (1995) give the dynamic background for the better understanding of a secondary jet flowing northward along the eastern coast of Peninsular Malaysia. In accordance with Wyrtki (1961), this jet is well resolved in our simulation in February.

In agreement with Pohlmann (1987), a gyre, flowing in a counterclockwise rotation, located approximately 300 km off the Vietnamese coast, is well resolved in our simulations.

The numerical simulation of July, a typical month of the SW monsoon season, is analysed (Fig. 5). A primary jet, flowing in a northeast direction parallel to the Vietnamese coast, is detected. A secondary jet, parallel to the east coast of the Malay Peninsula, makes the water mass flow in a northward direction. Two gyres flowing in a clockwise rotation are well resolved by the model. One is located in the Gulf of Thailand; the other is located approximately 300 km southeast of the Vietnamese coast.

These two jets, as well as the two gyres, were observed by Wyrtki (1961) for the month of June (Fig. 6). For a dynamic interpretation of the circulation during the SW monsoon season, the reader is referred to Saadon and Camerlengo (1995).
Alejandro Camerlengo and Monica Ines Demmler

In view of our results, it can be stated that no contamination of the interior solution due to the implementation of the radiative open boundary conditions employed is detected.

A numerical model solving the external mode has been developed. The model equations are the classic hydrodynamic equations of mass and momentum, vertically integrated. The model resolves reasonably well the circulation of the South China Sea, driven by the NE and SW monsoons. Our numerical simulations for the months of February and July are in agreement with Wyrtki's (1961) observations.

ACKNOWLEDGEMENTS

Comments made by Dr Nasir Saadon are appreciated. This research was financially supported by UPM in its entirety. The authors gratefully acknowledge this support.

REFERENCES


SAADON, M.N. and A.L. CAMERLENGO. 1995. Response of the ocean mixed layer, off Kuala Terengganu, during typical NE and SW monsoons. Submitted for publication to *GEOACTA (Argentina)*.