

# **UNIVERSITI PUTRA MALAYSIA**

# FINITE ELEMENT ANALYSIS OF HYDRAULIC BULGING OF METAL TUBES

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FK 2006 94

### FINITE ELEMENT ANALYSIS OF HYDRAULIC BULGING OF METAL TUBES

By

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Thesis Submitted to the School of Graduate Studies, Universiti Putra Malaysia, in Fulfilment of the Requirement for the Degree of Master of Science

November 2006



### TO THE MEMORY OF MY FIRST TEACHERS,

**MY MOTHER AND FATHER** 



Abstract of thesis presented to the Senate of Universiti Putra Malaysia in fulfilment of the requirement for the degree of Master of Science

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#### November 2006

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Faculty: Engineering

The use of finite element simulation in the development of bulge forming procedures is becoming more important as it provides a cheap and efficient way to determine important process parameters. Further improvements to the bulge forming method will be realized with the use of simulation and the design of advanced tooling. One major area where tube hydroforming is applied is in automotive structures.

In this current research, numerical analysis was conducted using the explicit finite element code ANSYS 2D. One-fourth model of the whole geometry consisting of the tube and the dies was adopted in consideration for symmetric property of the tube deformation. The model of metal tube is assumed as a bilinear isotropic model approximating the characteristics of annealed mild steel was adopted as the material for the tube. The final model contains 630 nodes and 560 elements included 19 contact elements between die and tube. The interface between the die and the tube was modeled using an automatic node to surface contact.



The effects of friction, geometric parameters; tube thickness, tube length, die corner radius and diameter of bulge width and varying internal pressures only and with axial load were evaluated in bulge hydroforming. Furthermore, two types of metal were tested, namely, mild steel tube and copper.

Numerical results were verified with available experimental values obtained from the literature were carried out and the percentage error is about 4.5%.

Finite element analysis showed that for a particular amount of wall thinning there is an increase of around 5.23% in bulge height for combined internal pressure with axial force. Results of this study indicate that tube hydroforming with combined internal pressure with axial force can increase expansion with less von Mises stress (8.32%) i.e. more difficult parts can be designed and manufactured. Furthermore, the minimum (optimum) friction coefficient displayed the highest value of bulging with the lowest value of decreasing of wall thickness was recorded for friction coefficient ( $\mu$ ) 0.15. Also the tube bulging increases with increasing die corner radius and bulge width. It also decreases with increasing initial tube length and initial thickness of the tube material. All these parameters are crucial to the success of the hydroforming operation.



Abstrak tesis yang dikemukakan kepada Senat Universiti Putra Malaysia sebagai memenuhi keperluan untuk ijazah Master Sains

### ANALISIS UNSUR TERHINGGA UNTUK PEMBONJOLAN HIDRAULIK BAGI TIUB LOGAM

Oleh

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#### November 2006

#### Pengerusi: Profesor Abdel Magid S. Hamouda, PhD

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Penggunaan simulasi unsur terhingga dalam pembangunan prosedur-prosedur pembentukan bonjol telah menjadi semakin penting kerana simulasi ini memberikan satu cara yang murah lagi cekap untuk menentukan parameter-parameter proses yang penting. Peningkatan selanjutnya dalam kaedah pembentukan bonjol akan direalisasikan dengan penggunaan simulasi yang cekap dan reka bentuk alat yang lebih maju. Satu bidang utama di mana pembentukan tiub secara hidro digunakan adalah dalam pembuatan struktur-struktur automotif.

Dalam kajian terkini ini, analisis kaedah berangka telah dijalankan dengan menggunakan kod tak tersirat elemen unsur terhingga iaitu ANSYS 2D. Satu per empat model daripada keseluruhan geometri mengandungi tiub dan acuannya telah diubah dengan mengambil kira sifat simetri bagi pembentukan tiub. Model tiub keluli ini dianggap sebagai satu model isotropi bilinear yang menyerupai sifat keluli lembut sepuh lindap yang telah dipilih sebagai bahan bagi tiub ini. Model terakhir mengandungi 630 nod and 560 unsur termasuk 19 unsur yang bersentuhan di antara



acuan dan tiub. Permukaan di antara acuan dan tiub telah dimodelkan dengan menggunakan nod automatik kepada sentuhan permukaan.

Kesan daripada geseran, parameter-parameter geometri, ketebalan tiub, panjang tiub, jejari bucu acuan dan diameter bagi lebar bonjol serta tekanan dalaman yang berlainan dan dengan paksi beban telah diuji dalam pembonjolan hidraulik. Selain itu, kajian perbandingan antara sifat-sifat bahan bagi tiub keluli lembut dan kuprum juga telah dilaksanakan.

Keputusan berangka yang diperolehi telah dibandingkan dengan hasil keputusan eksperimen dari kajian ilmiah yang lain. Keputusan menunjukkan peratusan ralat adalah sebanyak 4.5%.

Analisis unsur terhingga menunjukkan peningkatan ketinggian bonjolan sebanyak 8% bagi amaun penipisan dinding tiub yang tertentu untuk kombinasi di antara tekanan dalam tiub bersama daya paksi. Keputusan kajian ini menunjukkan pembentukan tiub secara hidro dengan kombinasi di antara tekanan dalam tiub bersama daya paksi akan meningkatkan amaun pengembangan dengan tekanan yang lebih rendah pada tiub tersebut. Oleh itu bahagian produk yang lebih kompleks dapat direka dan dihasilkan. Tambahan lagi, koefisien geseran minimum (optimum) yang menunjukkan ganjakan yang tertinggi dengan nilai terendah bagi pengurangan ketebalan dinding telah tercatat pada koefisien geseran (µ) 0.15. Ganjakan tiub juga bertambah dengan pertambahan jejari penjuru acuan dan lebar ganjak. Ia juga berkurangan dengan pertambahan panjang tiub awal dan ketebalan awal bahan tiub. Kesemua parameter berkenaan adalah amat genting dalam menjayakan operasi hidro digunakan



#### ACKNOWLEDGEMENTS

All praise to supreme almighty Allah s.w.t. the only creator, cherisher, sustainer and efficient assembler of the world and galaxies whose blessings and kindness have enabled me to accomplish this project successfully.

Gratefully acknowledge the guidance, advice, support and encouragement received from my supervisor, Professor Dr. Abdel Magid S. Hamouda, who keeps advising and commenting throughout this project until it turns to real success.

I am also grateful to my supervisory committee, Associate Professor Ir. Dr. Mohd Sapuan Salit, for their advice and helpful discussion during this period of study.

I am also grateful to Professor Dr. A. kostanjevec Senior Researcher, University of Ljubljana, Slovenia and Associate Professor Dr. I. Mupende, Technical University Clausthal, Germany, I wish to express my sincere thanks for their valuable remarks, assistance and advice me towards a successful completion of this research.

Appreciation also to all the staff in Department of Mechanical and Manufacturing Engineering, Universiti Putra Malaysia for providing the facilities and the components required for undertaking this project.



# **TABLE OF CONTENTS**

DEDICATION	2
ABSTRACT	3
ABSTRAK	5
ACKNOWLEDGEMENTS	7
APPROVAL	8
DECLARATION	10
LIST OF TABLES	14
LIST OF FIGURES	15
LIST OF ABBREVIATIONS	19

### CHAPTER

Ι	INTRODUCTION	21
	Introduction	21
	Methods	22
	Benefit and Limits	24
	Problem statement	26
	Aims	27
	Thesis Layout	28

II	LITERATURE REVIEW	29
	Introduction	29
	Mathematical descriptions of Plasticity	30
	Plasticity	31
	Plastic Deformation in Uniaxial Stress State	32
	Principles of plastic flow theory	35
	Strain Hardening Laws	36
	The Mechanics of Hydroforming Process	39
	Yield Criteria and the Yield Criterion of Tube Hydroforming	42
	Springback	43
	Hydroforming	44
	Sheet hydroforming	45
	Tube hydroforming	47
	Classification of tube hydroformed part	51
	Failure cases of hydraulic bulging	52
	Buckling	53
	Wrinkling	55
	Bursting (Fracture)	56
	Estimation of the pressure loading path for hydraulic bulge form	ning 57
	Internal pressure limits	58
	Experimental analysis	62



Experimental Setup	
Monitoring of the during hydroforming processes	
Theoretical analysis	
Analytical model	67
FEA of tube hydroforming	74
FEA modeling	74
Design of process parameters	78
Incremental approach for the estimate of plastic strain	79
Summary	

### III METHODOLOGY

Resource framework	82
Procedures for modeling and analyzing the model	85
Determination of the Process Parameters	87
Design parameters	88
Influence of tube and die geometric parameters on the	90
Hydroforming	
Effect of tube thickness	90
Effect of variation tube length	91
Effect of variation of bulge width	91
Effect of variation of die corner radius	91
Influence of Process parameters on hydroforming	92
Effect of variation of internal pressure only	92
Effect of variation of combined of internal pressure with axial force	92
Influence of process limits on hydroforming	93
Effect of variation of coefficient of friction on	93
hydroforming	
Influence of material type	93
Summary	94

### IV FINITE ELEMENT MODELING OF TUBE HYDROFORMING PROCESS

CESS	
FEM model for the free bulge THF	95
Material properties and element characteristic	97
Boundary conditions and FEA of the free bulging THF	99
Element optimization	100
Element shape optimization	100
Element size optimization	104
Solution	105
Incremental method	105
Iterative methods	106
Verification of the finite element model	107
Boundary Condition	109
Summary	113



82

V	RESULTS AND DISCUSSIONS	114
	Influence of process limits on the hydroformability	114
	Effect of friction	114
	Effect of coefficient of friction on the bulge height	115
	Influence of process parameters on the hydroformability	121
	Effect of internal pressure on the hydroformability	121
	Effect of internal pressure load only on tube forming	121
	Effect of combined internal pressure with axial load	124
	Effect of ratio of axial force to pressure $(K_R)$	129
	Influence of tube parameters on the hydroformability	130
	Effect of tube length	130
	Effect tube length on the bulge height	131
	Effect of tube thickness	133
	Effect of tube thickness on tube hydroformability	133
	Effect of die corner radius	136
Effect of variation die corner radius Effect of material type Effect of material types on bulge height and von Mises stress	136	
	138	
	139	
	Effect of variation of bulge width diameter on bulge Height	142
	Discussion	143
VI	CONCLUSIONS AND RECOMMENDATIONS	146
	Conclusions	146
	Recommendations for future works	150
REFE	RENCES	152
APPENDICES		158
<b>BIODATA OF THE AUTHOR</b>		188

LIST OF PUBLICATIONS

# LIST OF TABLES

Table		Page
2.1	The stress stat of tube hydroforming	41
3.1	Tube geometrical parameters, process parameters and limit parameters	90
3.2	The mechanical properties of materials used in this comparison	93
4.1	Material properties for copper	108
5.1	Sizes, boundary conditions and mechanical properties of the specimens	115
5.2	Bulge tube with thickness 2 mm with different $K_R$ ratios	129
5.3	Sizes, boundary conditions and mechanical properties of the annealed mild steel and copper specimens	139



# LIST OF FIGURES

Figure	P	age
2.1	Parts formed by using tube hydroforming	30
2.2	Brittle vs. ductile fracture	31
2.3	Uniaxial elasto-plastic stress strain curve	34
2.4	Deformation of a principal element	36
2.1	Schematic of the isotropic hardening rule	37
2.2	Different Strain Harding laws	38
2.3	Schematic of the kinematic hardening rule	39
2.4	Schematic diagram of tube hydroforming	40
2.5	Stress state of tube hydroforming	41
2.6	Springback	43
2.11	Various hydroforming processes	44
2.12	Classification of the sheet hydroforming	45
2.13	Sheet hydroforming process	46
2.14	Tube Hydroforming process	48
2.15	The Tube Hydroforming System	50
2.16	Tube hydroformed part features (a) bent feature, (b) crushed feature (c) bulge feature and (d) protrusion feature (referred as Y-shape)	52
2.17	Common failure modes that limit THF process, winkling, buckling and Bursting	53
2.18	Buckling stress $\sigma_z$ , tangent modulus $T_p$ and section modulus $J_z$ in relation to the expansion of the tube	n 54
2.19	The tube dimensions	55
2.20	The limits and the working range in tube hydroforming	57
2.21	Bulge forming of cross branch components (a and b)	60



2.22	Tube hydroforming consists of free forming and calibration	61
2.7	A schematic diagram of the basic tooling for the hydraulic bulging of tubes	62
2.8	The tube bulging machine at Dublin City University	63
2.9	Schematic of experimental apparatus for tube bulge tests	64
2.10	Workpiece before and after test	65
2.11	Hydraulic bulge test to determine tube quality and properties	67
2.28	Thin-walled tube in cylindrical coordinates	68
2.29	Schematic diagram of the die-punch-blank system showing geometric parameters	69
2.30	Radial and axial stress systems	70
2.31	Tube with internal and external pressure	72
2.32	Alternative view of the fully deformed tube	75
2.33	Finite element model of X-branch (1/8th symmetric model)	76
2.34	Finite element model of T-branch (2D symmetric model)	76
2.35	Tube hydroforming process	78
2.12	loading path beyond the yield point	79
3.1	Method of Approach	84
3.2	Applied load steps: a) Stepped load and b) Ramped load	85
3.3	Basic steps to carry out the simulation	86
3.4	Geometric parameters of tube bulging	87
3.5	Sectional and plan view of the formed component	89
3.6	Finite element method of one quarter of the problem	89
4.1	Schematic view of the geometric of tube and die	96
4.2	One quarter tube and die mesh with finite element model	97
4.3	Bi-linear stress-strain curve of the material	98
4.4	Contact pairs between the tube and die	99



4.5	Finite element mesh with boundary conditions	100
4.6	Quadrilateral shape element	101
4.7	Triangular shape element	101
4.8	Model meshed with quadrilateral element shape	102
4.9	Model meshed with triangular element shape	102
4.10	Comparative between quadrilateral and triangular elements shape	103
4.11	Comparative between quadrilateral elements size	104
4.12	Modified Newton-Raphson iteration method	107
4.13	Bi-linear stress-strain curve of copper material	109
4.14	Comparison of simulation results with experimental work of Hutchinson	111
4.15	Comparison of bulge heights obtained for various simulations with Experimental results	112
5.1	The effect of changing friction between the die and the tube	116
5.14	Schematic of the various forces that give rise to friction during a hydroforming process	117
5.15	Stress distribution in the thickness direction at $\mu = 0.0$	118
5.16	Stress distribution in the thickness direction at $\mu = 0.15$	118
5.17	Stress distribution in the thickness direction at $\mu = 0.3$	119
5.6	The Effect of coefficient on Bulge	120
5.18	Bulge height – Von mises stress for internal pressure only	122
5.19	Von mises stress vs Time for combined load at 60 MPa	122
5.9	The Effect of using internal pressure only	123
5.10	The Effect of using combined internal pressure with axial force	124
5.11	The effect of using internal pressure only & with axial force on tube forming	125
5.12	The effect of using different loading pressures	126
5.13	Distribution of plastic strain in the thickness direction for pressure only	127



5.14	Distribution of plastic strain in the thickness direction for combined load	127
5.20	Distribution of plastic strain in the thickness direction for pressure only	128
5.21	Distribution of plastic strain in the thickness direction for combined load	128
5.17	The effect of $K_R$ on bulge height and von mises stress	130
5.18	Effect of tube length on the bulge height	131
5.19	Bulge height with different tubes length	132
5.20	Bulge height with different tube thicknesses	134
5.21	The effect of changing the tube thickness	135
5.22	The boundary condition of die and tube	136
5.23	Effect of die corner radius on von mises stress and bulge height	137
5.23	The tube and the die with free tube length $(l_f)$	138
5.25	The Effect of using different material	140
5.24	Von Mises stress for both metals vs. simulation time	141
5.27	Effect of increasing in width diameter on tube hydroforming	142
Al	Basic element shapes	161
A2	Two-dimensional continuum domain	162
C1	Load displacement curve	180
C2	Newton-Raphson iteration method applied to a strain-softening system	180
C3	Flow chart of a nonlinear analysis program	181
C4	Flow chart of a nonlinear analysis with a load increment	182



# LIST OF ABBREVIATIONS

$\mathbf{D}_{0}, \mathbf{d}_{0}, \mathbf{D}$	Outer tube diameter
di	Inner tube diameter
D <sub>p</sub>	Protrusion diameter
E	Young modulus
F, F <sub>a,</sub> F <sub>r</sub>	Axial force (Load)
Ft	Total axial force
Ff	Axial friction force
k	Shear strength
K <sub>R</sub>	Ratio of the axial force to the internal pressure
K	Strength coefficient
l <sub>f</sub>	The free tube length
L, <i>x</i>	Length of tube
μ	Coefficient of friction
m	Friction factor
n	Strain hardening exponent
Pi	Internal pressure
Po	Outside pressure
(Pi) <sub>max</sub>	Calibrating pressure
( <b>P</b> <sub>i</sub> ) <sub>b</sub>	Bursting pressure
( <b>P</b> i),	Yielding pressure
Poc	Pressure under constrained area
$\mathbf{R}_{\mathbf{b}}, \mathbf{r}_{\mathbf{b}}$	Smallest die corner radius



t <sub>i</sub>	Finial tube wall thickness
t <sub>o</sub> , t	Initial tube wall thickness
Tp	Tangent modulus
$W_b$	Bulge width diameter
ν	Poisson's ratio
<i>x</i> <sub>0</sub>	Punches enter a length
σ <sub>k</sub>	Buckling stress
σ <sub>f</sub>	Flow stress of the material
σu	Ultimate tensile strength of the material
$\sigma_y$ , S	Yield strength of the material
α <sub>θ</sub>	Axial stress
σ	Von Mises Stress
ε <sub>t</sub>	Plane strain
ρ	Density



#### **CHAPTER I**

#### **INTRODUCTION**

### 1.1 Introduction

Hydroforming is one kind of plasticity working or metal forming process, which can be used to increase the diameter, to change the geometry, or to expand the outer walls of a cylindrical shell or tube. This process is very important, especially for industrial products of light weight and high strength.

In the past several years tube hydroforming technology has proved itself as a vital metal forming process for manufacturing variety tubular parts, e.g. household piping components, fittings, complex automotive parts such as exhaust pipes and structural components.

The rapid growth of this technology has been due to the advantages Tube hydroforming (THF) offers compared to conventional manufacturing via stamping and welding, namely (a) part consolidation; (b) weight reduction through more efficient section design and tailoring of the wall thickness in structural components;(c) improved structural strength and stiffiness via optimized section geometry; (d) lower tooling costs due to fewer parts; (e)fewer secondary operations (less welding and punching of holes during hydroforming); (f) tighter tolerances and reduced spring-back that facilitates assembly



and (g) reduced scrap since trimming of excess material is far less in THF than in stamping. The development of this process for automotive industries is relative new and many process variables have been studied, like: friction, material properties, pressures and displacement path during the process. The simulation is a very important method to help to develop this process. Using finite element method many researches have been studying the influence of these variables in the process and they are applying forming limit expressions to define whether the material will resist to the deformation or not. Successful tube hydroforming process requires proper combination of part design, material selection, and application of internal pressure and axial feeding. By using Finite Element Analysis methods, process parameters can be determined before manufacturing the dies and starting die try-out and process development.

The development of hydroformed parts for series production necessitate efficient methods to meet the requirements of short development times, high part quality with an optimized process chain. An important factor in achieving these short development lead times is process simulation exploiting the potential of finite element analysis (FEA).

#### 1.2 Methods

The bulge forming of tubular components is accomplished by the application of hydrostatic pressure to tube blanks either in free expansion mode or using a die bearing the shape of the component to be formed. The pressure is transmitted via a medium such as a liquid (e.g. hydraulic fluid or water), an elastomer (e.g. rubber or polyurethane), or a



soft metal (e.g. lead or a lead alloy). Bulge forming using pure internal pressure has a major limitation for producing excessive thinning of the tube wall which lead to the rupture of the tube for only moderate expansions. However, if a compressive axial load is applied to the ends of the tube simultaneously with the internal pressure, metal can be fed into the deformation zone during forming enabling more expansion and less thinning.

In tube hydroforming THF, compressive stresses occur in regions where the tube material is axially fed, and tensile stresses occur in expansion regions. The main failure modes are buckling, wrinkling (excessively high compressive stress) and bursting (excessively high tensile stress). It is clear that only an appropriate relationship between internal pressure and axial load, guarantees a successful THF process without any of the failures. Hence, it is imperative to establish a systematic way for determining loading paths and using finite element analysis (FEA) is one possible way. Internal pressure and axial load are then applied simultaneously to form the tube to fill the die cavity. To obtain a successful part, coordination of the pressurization and axial feeding is required. High internal pressure without end feeding will result in bursting of tube blank. On the other hand, large end feeding with insufficient internal pressure will lead to the development of wrinkles on the tube wall.

Effective classifications of hydroformed tubular parts are necessary for development of THF part design and process systematically. Finite element analysis (FEA) simulations can be used as a tool to extensively analyze THF. Design of the process parameters are normally selected through time-consuming, trial-and-error iterative FEA simulations.



FEA simulation enhanced with optimization schemes can greatly reduce the lead-time spent in the process development.

#### 1.3 Benefit and Limitations

Tube hydroforming has been identified as a new technology to manufacture parts. Tube hydroforming has many advantages in comparison with conventional manufacturing via stamping and welding. It can reduce the weight of the component, retain and even improve the strength and stiffness, reduce tooling cost due to fewer parts and tube hydroforming requires fewer secondary operations.

With the aid of FEA simulation, the part quality control, and the design of the tube hydroforming process can be easily implemented and monitored. FEA simulations provide insights on the necessary process parameters internal pressure and axial load, part geometry, and part formability by analyzing the thinning, thickening, and strain distribution in the deformed tube.

In all metal forming processes, part and process design is an essential step in successful manufacturing of any products. Tube hydroforming (THF) process demands a lot of engineering knowledge starting from the part design which is constrained by part functionality and geometry, to the process design where appropriate combination of internal pressure and axial feed need to be determined. It has always been of a primary concern in the industry to reduce the lead time in part and process design developments

