



UNIVERSITI PUTRA MALAYSIA

**EXPERIMENTAL AND COMPUTATIONAL CRUSHING BEHAVIOUR
OF LAMINATED COMPOSITE SHELLS**

ELSADIG MAHDI AHMED SAAD

FK 2000 52

**EXPERIMENTAL AND COMPUTATIONAL CRUSHING BEHAVIOUR OF
LAMINATED COMPOSITE SHELLS**

By

ELSADIG MAHDI AHMED SAAD

**Thesis Submitted in Fulfilment of the Requirement for the Degree of Doctor of
Philosophy in the Faculty of Engineering
Universiti Putra Malaysia**

December 2000



To My Exemplary Parents, Sisters and Brothers

**To My Wonderful Brother's and Sister's Sons and Daughters, Especially Shahinaz
and Selma, to Whom I am Very Proud.**



Abstract of thesis presented to the Senate of Universiti Putra Malaysia in fulfilment of the requirement for the degree of Doctor of Philosophy.

**EXPERIMENTAL AND COMPUTATIONAL CRUSHING BEHAVIOUR OF
LAMINATED COMPOSITE SHELLS**

By

ELSADIG MAHDI AHMED SAAD

December 2000

Chairman: Associate Professor Barkawi Bin Sahari, Ir. Ph.D.

Faculty: Engineering

This thesis presents the effect of structural geometry, reinforcement type and hybridisation on the crushing behaviour, energy absorption, failure mechanism and failure mode of cylindrical, conical and compound composite shell. The static crushing behaviour of cylindrical, conical and compound composite shell under uniform axial load has been investigated, experimentally, analytically and numerically. Four types of composites were tested, namely, carbon fibre/epoxy, glass fibre/epoxy, oil palm frond fibre/epoxy and the carbon-glass hybrid. This work also examines the effect of the residual stresses built on the crushing behaviour; energy absorption, failure mechanism and mode of failure of the filament wound laminated circular conical composite shell.

For the circular cylindrical and conical shells, the cones vertex angles tested were 0, 6, 12, and 18⁰. Results for the glass/epoxy circular cylindrical shell show that

the stress distribution is constant along the shell generator. On the other hand results for the glass/epoxy circular conical shells with vertex angles of 6, 12 and 18 degrees show that the stress distribution is sensitive along the shell generator. As the vertex angle increases, the average crushing load increases, while the initial failure load decreases.

The compound shells used in this investigation were the cone-cone and cone-cylinder-cone intersection composite shells. For the cone-cone intersection shells, the cone vertex angles were 10° , 15° , 20° and 25° . While for the cone-cylinder-cone, the cone vertex angles are 10° and 15° and the cylindrical part lengths were varied between 0 and 50 mm.

The results showed that the initial failure was dominated by interfacial and shear failure, while the delamination and eventually fibre fracture dominated the failure mechanism after the initial first failure. For the circular cylindrical and conical shells, the proposed analytical solution well predicts the initial failure load for the circular cylindrical and conical laminated composite shells. The failure criteria used to predict the initial failure show an excellent agreement. For the cone-cone intersection composite shell, the results showed that the structures with vertex angles 20° and 25° exhibited good energy absorption capability. For the cone-cylinder-cone, numerical results show that high-localised stress has been concentrated at the junctions between the cylinder and cones. Experimental results showed that structures of cylindrical part

length varies between 10 and 20 mm exhibited good energy absorption capability and stands a very high crushing load.

Abstrak tesis yang dikemukakan kepada Senat Universiti Putra Malaysia
sebagai memenuhi keperluan untuk ijazah Doktor Falsafah

**EKSPERIMEN DAN KOMPUTATION PERTEMBUNGAN TINGKAHLAKU
BERLAMINA KOMPOSIT RANGKA LUAR**

Oleh

ELSADIG MAHDI AHMED SAAD

Oktober 2000

Pengerusi: Profesor Madya Barkawi Bin Sahari, Ph.D.

Fakulti: Kejuruteraan

Tesis ini memberi penjelasan tentang kesan geometri struktur, jenis perykukah dan hibridisasi lerada kelakuan hentakan dalam, penyerapan tenaga, mekanisma kegagalan dan mod kegagalan kon selinder dan rangka luar sebatian komposit. Kelakuan hentakan statik selinder, kon dan campuran komposit rangka luar dalam bebanan selanjar juga dikaji secara analisis, pengiraan, dan secara percubaan. Terdapat empat jenis komposit yang diuji iaiyu gentian karbon /epoksi, gentian kaca /epoksi, gentian tandan kelapa sawit /epoksi dan karbon gentian kaca /epoksi. Tesis ini juga mengkaji kesan tegasan baki dalam keadaan hentakan, penyerapan tenaga dan mekanisma kegagalan dan mod filamen berlamina rangka luar kon komposit.

Untuk kon dan silinder, sudut puncak kon diuji pada 0, 6, 12, 18 darjah. Kajian dan perkiraan secara pengiraan menunjukkan tegasan baki tertumpu pada hujung kecil kon. Jika tegasan baki merupakan permasalahan utama maka struktur yang terbaik

adalah rangka luar selinder yang mempunyai sudut 0. Bila sudut puncak meningkat, bebanan tekanan hentakan meningkat manakala kadar bebanan permulaan gagal menurun.

Sebatian rangka luar yang digunakan untuk kajian adalah kon-kon dan kon-kon dan kon-selinder-kon yang terpotong pada komposit rangka luar. Bahagian konikal dalam sebatian terpotong adalah simetri. Untuk rangka luar kon-kon terpotong, sudut puncak adalah 10, 15, 20 dan 25. Bagi kon-silinder-kon, sudutnya adalah 10 dan 15 darjah. Jarak antara silinder adalah diubah diantara 0 dan 50mm.

Mod kegagalan telah dikaji dengan gambar diambil semasa hentakan spesimen dilakukan. Hasilnya kegagalan awal di dominasi oleh antaramuka dan kegagalan tegasan, manakala delaminasi dan kegagalan gentian mendominasi mekanisma kegagalan selepas kegagalan awal. Untuk selinder dan kon rangka luar, seperti yang ditunjukkan oleh kajian analitik mentafsirkan kegagalan awal untuk selinder dan kon berlamina rangka luar komposit. Dengan ini kriteria kegagalan yang digunakan menunjukkan korelasi yang tinggi.

Dari pandangan geometri dan bahan, yang telah dianalisis secara analitik, eksperimen dan pengiraan menunjukkan rangka luar selinder diperbuat daripada karbon/epoksi meramalkan beban berpusat sebagai sebab utama kegagalan awal. Boleh ditunjukkan juga bahawa bila sudut puncak meningkat kadar kegagalan awal menurun. Untuk potongan kon-kon komposit rangka luar, hasil menunjukkan bahawa

dengan sudut puncak 20 dan 25 mempamerkan sifat penyerap tenaga yang tinggi. Hasil pengiraan menunjukkan tegasan tetempat banyak ditemui pada pertemuan antara dua kon. Untuk kon-selinder-kon, hasil pengiraan menunjukkan bahawa tegasan tetempat tertumpu pada tempat pertemuan antara selinder dan kon. Hasil Eksperimen juga menunjukkan panjang bahagian selinder adalah diantara 10 hingga 20mm mempamerkan suatu keadaan yang boleh menyerap tenaga yang optimum dan dapat menahan bebanan hentakan yang tinggi.

ACKNOWLEDGEMENTS

First I would like to thank my supervisor Associate Prof. Dr. Barkawi Bin Sahari. Many ideas originate in our frequent discussion and his constant support and patience over the years have been of invaluable help.

My deep thanks to my co-supervisors Dr. Yousif A. Khalid and Dr A. M. S. Hamouda for their always helpful advise and for many discussions. .

I am very grateful to Hj Md Sharaani for helping out in designing and setting up of the experiments. I also, acknowledge the help from Mr. Ahmed Shaifuldeen.

The period from October 1998 to May 1999 was spent at the Institute of Solid Mechanics, Denmark Technical University at Lyngby. I am indebted to Professor Pauli Pedersen for making this visit possible, and thus giving me a great opportunity to spend some productive and quality time in his institute and also letting me communicate with great scientists.

Special thanks go to my family and colleagues, Hisham and Rasha, who have helped and supported me beyond description.



TABLE OF CONTENTS

		Page
DEDICATION		ii
ABSTRACT		iii
ABSRTAK		vi
ACKNOWLEDGEMENTS		ix
ABROVAL SHEETS		x
DECLARATION FORM		xii
LIST OF TABLES		xviii
LIST OF FIGURES		xix
NOTATION AND ABBREVIATIONS		xxv
 CHAPTER		
1	INTRODUCTION	1
2	LITERATURE REVIEW	8
	2.1 Background Review	8
	2.1.1 Constituent Materials of Composite	8
	2.1.2 Reinforcement	8
	2.1.3 Matrix	9
	2.1.4 Epoxy Resin	9
	2.2 Types of Fibres	10
	2.2.1 Oil Palm Frond Fibre	10
	2.2.2 Carbon Fibre	15
	2.2.3 Glass Fibre	19
	2.3 Micromechanics of Composite Materials	22
	2.4 Engineering Properties in Global Coordinate Systems	27
	2.5 Failure Criteria	32
	2.6 Composite Shells	34
	2.6.1 Fabrication Process of Composite	34
	2.6.1.1 Background Review	34
	2.6.1.2 Hand Lay-up	35
	2.6.1.3 Filament Wound	35
	2.6.2 Work On Composite Shells	38
	2.6.2.1 Development Of Shell Theory	38
	2.6.2.2 Circular Cylindrical Composite Shells	39
	2.6.2.3 Circular Conical Composite Shells	47
	2.6.2.4 Compound Shells	49
	2.7 Finite Element Analysis Work	50
	2.8 Conclusion	53



3	METHODOLOGY	54
	3.1 Analytical Work	57
	3.2 Finite Element Simulation Work	58
	3.3 Experimental Work	59
	3.4 Discussion	61
4	ANALYTICAL WORK	62
	4.1 Introduction	62
	4.2 Assumptions	62
	4.3 Shell Coordinates and Infinitesimal Distance in Shell Layers	63
	4.4 Basic Equation	65
	4.5 Equilibrium	66
	4.5.1 Stress Resultants and Couples	66
	4.5.2 Strain-Displacement Relationship	67
	4.5.3 Transformation Relations	71
	4.6 Failure Criteria	72
	4.7 Numerical Examples	75
	4.7.1 Circular Cylindrical Shell	75
	4.7.2 Circular Conical Shell	76
	4.8 Results	78
	4.9 Discussion	79
	4.10 Conclusion	80
5	FINITE ELEMENT WORK	82
	5.1 Element Description	83
	5.2 Nodal Systems	84
	5.3 Composite Models	85
	5.3.1 Local Coordinate System	85
	5.3.2 Composite Constitutive Model	86
	5.3.3 Integration of Element Matrices	88
	5.4 Effect of Fabrication Residual Stresses on FWL Composite Shells	91
	5.5 FWL Cylindrical and Conical Composite Shells Under Axial Compression	95
	5.6 FWL Hybrid Cylindrical Composite Shells Under Axial Compression	95
	5.7 FWL Cone-Cone Composite Shells Under Axial Compression	98
	5.8 FWL Cone-Cylinder-Cone Composite Shells Under Axial Compression	101
	5.9 Numerical Example	104
	5.9.1 Residual Stresses in FWL Circular Shells	104
	5.9.2 Crushing Behaviour of FWL Cylindrical and Conical Composite Shells	114

	5.9.3	FWL Cone-Cone Intersection (C-C) Composite Shell	118
	5.9.4	FWL Cone-Cylinder-Cone Intersection (C-T-C) Composite Shell	125
	5.10	Summary and Conclusion	127
6		EXPERIMENTAL WORK	
	6.1	Fabrication Method	128
	6.1.1	Fabrication Process of FWL Composite Shells	128
	6.1.2	Fabrication Process of OPFFRP Cylinder and Cones	128
	6.2	Geometry and Material	133
	6.3	Test procedure	134
	6.4	Results	139
	6.4.1	Circular Conical Shells	
	6.4.1.1	Crushing Behaviour	139
	6.4.1.2	Crushing Energy Absorption	143
	6.4.1.3	Structural Volume Reduction	145
	6.4.1.4	Discussion	164
	6.4.2	FWL G/C Hybrid Circular Cylindrical Shells	164
	6.4.2.1	Crushing Behaviour	164
	6.4.2.2	Crushing Energy Absorption	167
	6.4.2.3	Structural Volume Reduction	167
	6.4.2.4	Discussion	174
	6.4.3	FWL Cone-Cone Intersection (C-C) Composite Shells	175
	6.4.3.1	Crushing Behaviour	175
	6.4.3.2	Crushing Energy Absorption	177
	6.4.3.3	Structural Volume Reduction	178
	6.4.3.4	Discussion	178
	6.4.4	FWL Cone-Cylinder-Cone Intersection (C-T-C) Composite Shells	189
	6.4.4.1	Crushing Behaviour	189
	6.4.4.2	Crushing Energy Absorption	191
	6.4.4.3	Structural Volume Reduction	192
	6.4.4.4	Effect of T Length on the Initial Failure of C-T-C Intersection Shell	193
	6.4.4.5	Cylindrical Part length Consideration	193
	6.4.4.6	Discussion	206
	6.4.5	Effect of Material and Geometry	206
	6.4.5.1	Energy Absorption	207
	6.4.5.2	Initial Failure Load	207
	6.4.6	Comparison between Experimental and Theoretical Results	214
	6.4.6.1	FWL Circular Cylindrical and Conical Composite Shells	214

	6.4.6.2 FWL Compound Composite Shells	216
6.5	Discussion	218
6.6	Conclusion	219
7	OVERALL DISCUSSION	221
8	CONCLUSIONS AND RECOMMENDATIONS	228
	REFERENCES	236
	APPENDICES	245
	VITA	254



LIST OF TABLES

Table		Page
2.1	Typical mechanical properties of some of epoxy resins.	10
2.2	Yield of fresh fruit bunches crude palm oil and palm.	13
2.3	Oil palm planted area: 1975 - 1999 (Hectares).	14
2.4	Typical composition of glass fibre (in weight percent).	21
4.1	Typical engineering properties of CFRP and GFRP.	77
4.2	Maximum stresses (MPa) in principal material system stress space CFRP and GFRP.	78
4.3	Axial load (kN) cause initial failure in filament wound laminated circular cylindrical and conical shells.	79
5.1	Finite element predicted axial load (kN) causes failure in filament wound laminated circular cylindrical and conical shells.	115
5.2	Finite element predicted axial load (kN) causes failure in filament wound laminated cone-cone intersection composite shells.	119
6.1	Typical engineering properties of constituent materials.	137
6.2	Description of FWL carbon, glass and oil palm frond fibre cylindrical and conical composite shell.	138
6.3	Description of FWL carbon/glass/epoxy hybrid cylinder.	138
6.4	Description of filament wound cone-cone intersection composite shell.	138
6.5	Description of filament wound cone-cylinder-cone intersection composite shell.	139
6.6	Crush loads specific energy absorption and structural volume reduction of FWL glass fibre/epoxy, carbon fibre/epoxy and HLU oil palm frond fibre/epoxy circular cylindrical and conical shells.	163
6.7	Crush loads specific energy absorption and structural volume reduction of FWL glass/Carbon hybrid composite circular cylindrical shells.	174
6.8	Crush loads specific energy absorption and structural volume reduction of FWL GFRP and CFRP C-C intersection shell.	188
6.9	Crush loads specific energy absorption and structural volume reduction of FWL GFRP and CFRP C-T-C intersection shell.	205
6.10	Comparison between the experiment, theoretical results.	214
6.11	Comparison between the experiment and the finite element prediction of axial load (kN) causes initial failure in filament wound laminated cone-cone intersection GFRP composite shells.	216
6.12	Comparison between the experiment and the finite element prediction of axial load (kN) causes initial failure in filament wound laminated cone-cylinder-cone intersection GFRP composite shells.	216

LIST OF FIGURES

Figure	Page
2.1 Weight Loss and Shrinkage vs. Temperature during Stabilisation process	16
2.2 Unidirectional fibre square packing geometry	22
2.3 Variation of engineering properties with fibre orientation angle for carbon fibre/epoxy	30
2.4 Variation of engineering properties with fibre orientation angle for E-glass fibre/epoxy	31
2.5 Shells of Revolution of constant meridional curvature	38
2.6 Compound shells composed of cone-cone and cone-cylinder-cone in different arrangements	39
3.1 Flow chart describes the plan to carry out the work.	56
3.2 Flow chart describes analytical work	57
3.3 Flow chart describes the finite element simulation work	58
3.4 Flow chart describes the fabrication process of the specimens	59
3.5 Flow chart describes the specimen preparation and the testing criteria	60
4.1 Position vector to a point on the middle surface	64
4.2 Conical shell	65
4.3 Force equilibrium on shell element	66
4.4 Maximum stresses in principal material system stress space	73
4.5 Circular cylindrical shell model for axial compression	75
4.6 Circular conical shell model for axial compression	77
5.1 Quadratic thick shell elements (QTS8)	84
5.2 Definition of an orthotropic material in 2-D using an angle of orthotropy	87
5.3 Definition of an orthotropic material in 3-D using a Cartesian set	87
5.4 Typical tow-step cure cycle	92
5.5 Circular conical shell with vertex angle of 0 degree subjected to a uniform temperature	93
5.6 Circular conical shell with vertex angle of 6 degree subjected to a uniform temperature	93
5.7 Circular conical shell with vertex angle of 12 degree subjected to a uniform temperature	94
5.8 Circular conical shell with vertex angle of 18 degree subjected to a uniform temperature	94
5.9 Model of circular conical shell with vertex angle of 0 degree for axial compression	96
5.10 Model of circular conical shell with vertex angle of 6 degree for axial compression	96
5.11 Model of circular conical shell with vertex angle of 12 degree for axial compression	97

5.12	Model of circular conical shell with vertex angle of 18 degree for axial compression	97
5.13	Circular cone-cone intersection shell model with vertex angle of 10 degrees for axial compression	99
5.14	Circular cone-cone intersection shell model with vertex angle of 15 degrees for axial compression	99
5.15	Circular cone-cone intersection shell model with vertex angle of 20 degrees for axial compression	100
5.16	Circular cone-cone intersection shell model with vertex angle of 25 degrees for axial compression	100
5.17	Circular cone-cylinder-cone intersection shell model with vertex angle of 10 degrees and cylindrical part length of 10 mm for axial compression	102
5.18	Circular cone-cylinder-cone intersection shell model with vertex angle of 10 degrees and cylindrical part length of 20 mm for axial compression	102
5.19	Circular cone-cylinder-cone intersection shell model with vertex angle of 10 degrees and cylindrical part length of 30 mm for axial compression	103
5.20	Circular cone-cylinder-cone intersection shell model with vertex angle of 10 degrees and cylindrical part length of 40 mm for axial compression	103
5.21	Circular cone-cylinder-cone intersection shell model with vertex angle of 10 degrees and cylindrical part length of 50 mm for axial compression	104
5.22	Axial residual stresses at the top surface of cured FWL circular conical shells	106
5.23	Axial residual stresses at the middle surface of cured FWL circular conical shells	107
5.24	Axial residual stresses at the bottom surface of cured FWL circular conical shells	108
5.25	Hoop residual stresses at the top surface of cured FWL circular conical shells	110
5.26	Hoop residual stresses at the top surface of cured FWL circular conical shells	111
5.27	Hoop residual stresses at the bottom surface of cured FWL circular conical shells	112
5.28	Deformed structure of circular cone with vertex angle of 0° at initial failure	116
5.29	Deformed structure of circular cone with vertex angle of 6° at initial failure	117
5.30	Deformed structure of circular cone with vertex angle of 12° at initial failure	117
5.31	Deformed structure of circular cone with vertex angle of 18° at initial failure	118

5.32	Deformed mesh of FWL cone-cone composite shell intersected at vertex angle of 10° .	120
5.33	Deformed mesh of FWL cone-cone composite shell intersected at vertex angle of 15° .	120
5.34	Deformed mesh of FWL cone-cone composite shell intersected at vertex angle of 20° .	121
5.35	Deformed mesh of FWL cone-cone composite shell intersected at vertex angle of 25° .	121
5.36	Axial stress distribution at portion along shell generator for the FWL cone-cone intersection glass/epoxy composite shells	122
5.37	Hoop stress distribution at portion along shell generator for the FWL cone-cone intersection glass/epoxy composite shells	123
5.38	In-plane Shear stress distribution at portion along shell generator for the FWL cone-cone intersection glass/epoxy composite shells.	124
5.39	Stress Distribution of FWL GFRP C-T-C with vertex angle of 10°	126
6.1	Stages of fabrication process of FWL composite shell specimen	130
6.2	Curing assembly Diagram of FWL composite shell	130
6.3	Typical FWL cylinder and cone under investigation	131
6.4	Material sequence of carbon/glass hybrid cylinder	131
6.5	Typical sketch of FWL cone-cone composite shell specimen.	132
6.6	Typical sketch of FWL cone-cylinder-cone composite shell specimen	132
6.7	Curing assembly Diagram of OPFFRP composite shell.	133
6.8	Load-displacement curve for the FWL glass/epoxy circular conical shells.	146
6.9	Load-displacement curve for the FWL carbon/epoxy circular conical shells.	147
6.10	Load-displacement curve for the hand laid up oil palm frond fibre reinforced epoxy composite circular conical shells.	148
6.11	Macroscopic view of the various failure modes for the circular cylindrical composite shells under axial compressive load	149
6.12	Crushing history of FWL glass/epoxy circular cylindrical shell under axial compressive load	150
6.13	Crushing history of FWL carbon/epoxy circular cylindrical shell under axial compressive load	151
6.14	Crushing history of hand laid up oil palm fibre/epoxy circular cylinder shell under axial compressive load	152
6.15	Crushing history of FWL glass/epoxy circular conical shell with vertex angle of 18 degrees under axial compressive load	153
6.16	Crushing history of FWL carbon/epoxy circular conical shell with vertex angle of 18 degrees under axial compressive load	154
6.17	Crushing history of hand laid up oil palm fibre/epoxy circular conical shell with vertex angle of 18 degrees under axial compressive load	155

6.18	Optical micrograph of a FWL glass/epoxy section through the crush zone at initial crushing failure	156
6.19	Optical micrograph of a FWL glass/epoxy section through the crush zone at complete crushing failure	156
6.20	Optical micrograph of a FWL carbon/epoxy section through the crush zone at initial crushing failure	157
6.21	Optical micrograph of a FWL carbon/epoxy section through the crush zone at complete crushing failure.	157
6.22	Optical micrograph of a HLU oil palm frond fibre section through the crush zone at initial crushing failure.	158
6.23	Optical micrograph of a HLU oil palm frond fibre section through the crush zone at complete crushing failure.	158
6.24	Load-Displacement curve and average load of composite circular cylindrical shell specimens.	159
6.25	Initial, average failure load, specific crushing energy and structural volume reduction of the FWL glass/epoxy circular conical shells with different vertex angles	160
6.26	Initial, average failure load, specific crushing energy and structural volume reduction of the FWL carbon/epoxy circular conical shells with different vertex angles	161
6.27	Initial, average failure load, specific crushing energy and structural volume reduction of the hand laid up oil palm frond fibre reinforced epoxy composite circular conical shells with different vertex angles.	162
6.28	Filament wound glass/carbon hybrid Circular cylindrical shells with different material sequence	168
6.29	Load-displacement curve for the hand laid up oil palm frond fibre reinforced epoxy composite circular conical shells	169
6.30	Total crushing failure history of FWL CGG hybrid cylinder under uniaxial compressive load	170
6.31	Total crushing failure history of FWL GGC hybrid cylinder under uniaxial compressive load	170
6.32	Total crushing failure history of FWL GCG hybrid cylinder under uniaxial compressive load	170
6.33	Optical micrograph of a FWL CGG hybrid section through the crush zone at initial crushing failure.	171
6.34	Optical micrograph of a FWL GCG section through the crush zone at initial crushing failure.	171
6.35	Optical micrograph of a FWL GGC section through the crush zone at complete crushing failure	172
6.36	Initial, average failure load, specific crushing energy and structural volume reduction of the FWL C/G hybrid composite circular cylinder.	173
6.37	Load-displacement curve for the FWL GFRP C-C intersection shells.	179

6.38	Load-displacement curve for the FWL CFRP C-C intersection shells.	180
6.39	Optical micrograph of a FWL GFRP section through the crush zone at initial crushing failure	181
6.40	Optical micrograph of a FWL GFRP section through the crush zone at total crushing failure.	181
6.41	Optical micrograph of a FWL CFRP section through the crush zone at initial crushing failure.	182
6.42	Optical micrograph of a FWL CFRP section through the crush zone at total crushing failure	182
6.43	Crushing history of FWL GFRP C-C15 under axial compressive load	183
6.44	Crushing history of FWL CFRP C-C15 ⁰ under axial compressive load	184
6.45	Load-displacement curves for the FWL GFRP and CFRP C-C15 intersection shells.	185
6.46	Initial, average failure load, specific crushing energy and structural volume reduction of the FWL GFRP C-C intersection shells with different vertex angles.	186
6.47	Initial, average failure load, specific crushing energy and structural volume reduction of the FWL CFRP C-C intersection shells with different vertex angles.	187
6.48	Load-displacement curve for the FWL GFRP C-T-C intersection shells with vertex angle of 10 degrees.	194
6.49	Load-displacement curve for the FWL GFRP C-T-C intersection shells with vertex angle of 15 degrees.	195
6.50	Crushing history of FWL GFRP T10 with vertex angle of 10 ⁰ under axial compressive load	196
6.51	Crushing history of FWL CFRP T10 with vertex angle of 10 ⁰ under axial compressive load	197
6.52	Crushing history of FWL GFRP T20 with vertex angle of 15 ⁰ under axial compressive load	198
6.53	Crushing history of FWL CFRP T20 with vertex angle of 15 ⁰ under axial compressive load	199
6.54	Load-displacement curves for the FWL GFRP C-T-C intersection shells with vertex angle of 10 and 15 degrees and cylindrical part length of 10mm.	200
6.55	Load-displacement curves for the FWL CFRP C-T-C intersection shells with vertex angle of 10 and 15 degrees and cylindrical part length of 10mm	201
6.56	Initial, average failure load, specific crushing energy and structural volume reduction of the FWL GFRP C-T-C intersection shells with vertex angle of 10 degrees and different cylindrical part lengths.	202



6.57	Initial, average failure load, specific crushing energy and structural volume reduction of the FWL GFRP C-T-C intersection shells with vertex angle of 15 degrees and different cylindrical part lengths	203
6.58	Effect of reinforcement on energy absorption characteristics of circular conical and cylindrical composite shells.	208
6.59	Effect of reinforcement on energy absorption characteristics of cone-cone intersection composite shells	209
6.60	Effect of reinforcement on energy absorption characteristics of cone-cylinder-cone intersection composite shells	210
6.61	Effect of reinforcement type on the load-displacement curves of circular cylindrical shells	211
6.62	Non-dimensional plot of the average crush loads relative to the instantaneous failure crush loads.	212
6.63	Initial failure load of the filament wound laminated circular cylindrical and conical composite shells	214
6.64	Initial failure load of the filament wound laminated cone-cone intersection composite shells	216
6.65	Initial failure load of the filament wound laminated cone-cone intersection composite shells	217

NOTATIONS AND ABBREVIATIONS

ρ	is the mass density of the structure
A	is the average cross-section area of the structure
M	is the mass of the structure
V_i, V_f	is the initial and final space volume occupied by the structure respectively.
E_s	is the specific crushing energy
H_{z1}	is the length of cone
H_{z2}	is the length of cylinder
H_z	is the total length of the structure.
E_m	is the matrix modulus
E_f	is the fibre modulus
G_m	is the matrix shear modulus
ν_m	is the matrix poison's ratio
ν_f	is the fibre poison's ratio
ξ	is the fibre packing geometry factor
E_{11}	is the longitudinal modulus
E_{22}	is the transverse modulus
G_{12}	is the in-plane shear modulus
G_{13}	is the transverse shear modulus in 1-3 plane
ν_{12}	is the major poison's ratio
ν_{21}	is the minor poison's ratio
β	is the semi vertex angle of the cone.